

NAVIGATION,

OR, THE

ART of Sailing upon the Sea.

CONTAINING

A Demonstration of the fundamental Principles of this Art.

Together with

All the Practical Rules of computing a Ship's Way,

BOTH BY

Plain Sailing, Mercator, and Middle Latitude,
Founded upon the foregoing Principles.

With many other useful Things hereto belonging.

To which are added,

Several necessary TABLES.

Vela damus, vastúmque cava trabe currimus æquor.
Postquam altum tenuere rates; nec jam amplius ullæ
Apparent terræ; cælum undique & undique pontus:

et cæcis erramus in undis.
VIRG.

Printed for W. INNYS and J. RICHARDSON, in Pater-noster Row.

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PREFACE

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PREFACE.

HE art of Navigation is of fuch consequence to this nation, that it is hard to fay whether or no we could tell how to live without it. And yet fuch is the ill luck it has met with, that it has never been treated of with that perspicuity. as fo useful an art deserves, nor rendered so easy as to be of general use to the world. For all the books that have fallen into my hands, are either too voluminous for being of any real use; or else they are defective in fome points or other; which yet 'tis necessary for a Mariner to be inform'd of. And which is worse, authors are not agreed about the truth of their own principles. Some crying down Plain Sailing as erroneous and not to be trusted at all; and others denying even Mercators Sailing to be true.

I thought therefore I should do some service to the young Navigator, by laying down, and demonstrating the sundamental principles of this art; and at the same time A 2 deducing,

deducing, from these principles, all the necessary rules for calculating a ship's place; and by making them so short and easy, and disposing them in such order, that the Mariner may not be at all puzzled with them. So that he may have at once all the rules that are necessary for him to know, as far as mathematical computations have any thing to do in the matter.

To this end, I have, in the first part, given several Problems in Astronomy, of frequent use at sea, and such Tables as are necessary to their solution. Likewise easy Rules for taking an observation, for sinding the variation of the Compass, the Lee-way of a Ship, the Motion of a Current, with an account of the Trade-Winds, the way of placing the Sails to the best advantage, which, though it may be hard to do exactly, yet it will be proper to come as near as one can; with some other things of like kind; all which are some way or other relating to the art of Navigation.

In the fecond part you have the demonfiration of the principles of what is properly call'd Navigation, with all the practical Rules

PREFACE.

Rules drawn from these principles, and applied to the solution of the several cases of Sailing. Then you have the method of keeping and correcting a reckoning. And then the method of keeping a journal of a whole voyage, to which end all the rest that goes before is directed.

Then follow several Tables, of which the Tables of Sines, Tangents, and Logarithms go but to five places of figures, which is abundantly sufficient for any degree of exactness that Navigation can admit of; and to go further would be needless.

In the Table of the Latitude and Longitude of places, the Longitude is reckon'd from the Canaries, as antiently. That whimfical humor of many modern Geographers of counting the Longitude from the metropolis of their own country, has brought all into confusion. And the same confusion must attend the practice of some persons, who, pretending to draw Maps and Charts, put the east or west end uppermost, according as their fancy directs them, tho' contrary to the establish'd Rules of Geography, by which the upper part ought always to be the north. To this I

A 3

may

may also add the giving old names to new places, as New-England, New-Spain, New-York, &c. which betrays a barrenness of invention in those that impose them, as well as induces a fort of obscurity and confusion in the use of them.

The Table of Meridional Parts here given is calculated for the Sphere; for I look upon it as an idle refinement to deduce them from the Spheroid; for this would require all the Parallels of Latitude, and Arches of the Meridian to be alter'd accordingly; which would create an endless deal of trouble for no real advantage. For if we consider that no Ship can steer true to a degree, or hardly to a quarter point of the Compass; nor can measure her distance sail'd, by the Log, to any fuch degree of exactness; but that there will always be a confiderable variation from the precise truth, in regard to the place of a Ship: And for this reason she is obliged, as oft as possible, to correct her Latitude and Longitude by observation. Therefore it would be quite trifling to descend to such minute differences as can have no fenfible effect in practice; and fuch is the difference between the Sphere and Spheroid. And therefore.

therefore, fince we must needs wander a little from the truth, we had better do it in a plain and easy way, than in a rigid and difficult one.

All the Rules here laid down for practice, I have made as short and plain as possible; for the Seaman ought not to be incumber'd with long tedious Rules. And I am in hopes that what is deliver'd in this little book will answer his end, and give him as much Satisfaction as any he will ever meet with, and I think too, as much as he can ever wish for.

W.E.



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EXPLANATION.

RAD. Radius.

Cos. Cosine.

T. or Tan. Tangent.

Cot. Cotangent.

Sec. Secant.

Dif. Lat. Difference of Latitude.

Dif. Long. Difference of Longitude.

Asc. Ascension.

Dec. Declination.

Perp. Perpendicular.

Log. Logarithm.

D. H. M. S. Days, Hours, Minutes, Seconds.

D. M. Degrees, Minutes.

E. W. N. S. East, West, North, South.

M. P. Meridional Parts.

NAVIGATION.

DEFINITIONS.

1. AVIGATION is the art of guiding or directing a ship; and computing her way through the sea, from one place to another.

2. Latitude of a place, is an arch of the meridian, contain'd between the equinoctial line and that place. This is reckon'd in degrees; and the greatest latitude never exceeds 90 degrees; for the poles are 90 degrees from the equinoctial.

3. Difference of Latitude of two places, is an arch of a meridian, contain'd between the parallels of lati ude passing through these places; this is also measured by degrees, and miles or minutes, of

which 60 make a degree.

4. Longitude of a place, is an arch of the equinoctial, contain'd between the first meridian (wherever it is) and the meridian of the place. This is measured by degrees, whereof 360 reach round the globe.

5. Difference of Longitude, is an arch of the equator, or the degrees contain'd between the me-

ridians of any two places.

6 Meridional Distance, is the distance in miles of any given place, from the meridian of another place. This is counted in the parallel of latitude of the given place.

7. Departure, is the whole easting or westing a ship continually makes during any single course, in passing from one meridian to another.

8. Course, is the angle which the ship's way

makes with the meridian.

9. Rumb, is the path or line that a fhip describes during any one course. A rumb line cuts all meridians in the same angle; and therefore it is a spiral line upon the globe, continually approaching the pole: except in an east and west course where it coincides with the parallel; and in a north and south with the meridian.

10. Plain Sailing, is the computing a ship's way by plain trigonometry, with regard to her easting,

westing, northing, or fouthing.

11. Middle Latitude Sailing, is a method of computing the way or place of a ship, with respect to her longitude, by rules depending on the latitude lying in the middle between two places of the ship.

12. Mercators Sailing, is computing a ship's way, or her place, in regard to her longitude, by help of a table of meridional parts, calculated on

purpose, for all latitudes.

13. Charts, are maps of the fea and the fea coasts. If the latitude and longitude be made every where equal, it is call'd a Plain Chart: If the meridians are drawn parallel, and besides, the degrees continually increase in proportion to the co-sines of the latitude; it is call'd a Mercator's Chart. There are other forts of charts, but not so common. But mercators is the truest, best known, and the most useful for navigation. In all charts, the upper end is the north, and the lower the south.

14. Variation of the Compass is an arch of the FIG. horizon, contain'd between the meridian of the place, which is a north and south line; and the magnetical meridian, or direction of the needle, or slower-de-luce. It is call'd, east variation, when it lies easterly of the north part of the true meridian; and west variation, if westerly.

Instruments belonging to Navigation; and their Use.

1: The Compass.

I. HIS is a circle divided into 32 equal parts; every point of division is a rumb, or point of the compass. These points are all named according to their polition, and number'd clear round the compass, thus, viz. North, north by east, north north east, &c. but only the first letter of every word is put. The use of this is to direct the ship in its proper course. For there being no tracts or high roads upon the fea, to direct her motion, there is no other way but for the perfon at the helm, so to steer the ship, that the flower-de-luce may always stand at the point of the compass the ship is to fail upon. The needle and compass-chard are so suspended, that they always lie horizontally; if it do not, drop a piece of fealing-wax upon the lightest side, under it; nothing of iron must be suffer'd to come near the com-

The

The mariners compass is so constructed, that the FIG. needle lies directly under the meridian, or north I. and fouth points of the card; by which means if there is any variation, the north point of the compass does not point to the true north. But it would be much easier for the practice of navigation at Sea, if the needle was not fixt to the compals card, but so contriv'd as either to be movab e under it, or fixt to another card under it that is movable, about the same (in nature of a rectifier), going a little stiff with a fpring; and to have a small index at the north end of the needle, by which to fet it to any degree of variation from the north point. If this was done, and the Index always fet to the proper variation at fea, the flower-de-luce would always point to true north; and there would be no ariation to be allow'd for in the reckoning; which would fave a great deal of trouble to the mariner, and prevent fuch miltakes as often happen in allowing for variation.

The azimuth compass, besides the card with the points of the compass, has an index and a thread, which index is movable about the center, and has two sights; the use of this is to take the azimuth of

the fun or a star.

The Log-Lie.

This is a cord divided into several parts call'd knots, each knot or part containing 46 feet:
This line is fasten'd to a board call'd the log, which board is about seven inches long. To one end of it the log-line is fastened, and to the other as much lead as will make it swim upright, just with the head above water. At the lower end is a hole where a pin goes in, which is fasten'd to a

part of the line; and this pin may be pluck'd out, FIG. when the line is run off.

In dividing the log-line there must be allow'd next the log 12, 15, or 18 sathom of stray line, according to the bigness of the ship. At the end of this is put in a red or white rag; and at that place the divisions of the line begin. The reason of this stray line is to veer the log pretty well out of the ship's wake, lest the eddy should suck the log after

the ship, and deceive you in the distance.

The use of the log and log-line is to measure the ship's way, or her distance run, by help of a half minute glass. For after the log is thrown in, and the red rag comes to hand, the half minute glass must be immediately turn'd; and that moment the glass is out, the line must be stopt; then observing the line, as many knots as are run off, so many miles the ship sails in an hour. If a line and plumes 30 times long, (reckoning from the center of the ball to the point of suspension) be hung up, it will vibrate 30 times in one glass, if it be t uc. In strictness each knot should be about 50 feet; but it is better to be only 45 or 46, and this agrees best with experience, for the log will drag a little after the ship, and make the measur'd distance less than it is; and it is better the reckoning be a-head of the ship, than the ship a-head of the reckoning.

A ship's way is commonly measured by degrees, and minutes or miles, 60 to a degree; or by leagues, 20 to a degree. But to avoid several tedious reductions, it were better to keep this account of the ship's way, as also of the difference of latitude and longitude, in degrees, and 100 parts of a degree. Ordinary a ship goes about a degree in a day. If the ship's way was kept in cents or hundred parts of a degree, then the knots of the log-line would be 27 feet.

The way the ship makes may be nearly estimated by an old experienced seaman; or it may be known by the distance of two marks on the ship's side; and the time she makes this way, may be measured by a watch, or by a glass, or by the pulse, or by repeating a certain number of words, or by hanging up a pendulum 30; inches long, to vibrate seconds.

3. The Sea Quadrant, or Davis's Quadrant.

The sca quadrant is an instrument to take the sun's altitude. It consists of three vanes, A, B, C; and two arches ed, GF. A is the horizon vane, B the shadow vane, C the fight vane, de is the 60 arch, containing 60 (or 65) degrees. FG the 30 arch, containing 30 (or 25) degrees. In using this instrument the vane B must be put to an even degree, less by 15° or 20° than the zenith distance, or complement of the altitude. Then turning the back to the fun, and looking through the vanes C and A, raise or settle the Initrument till the shadow of the upper edge of the vane B fall on the flit in A; then raise or settle the vane C, till you fee the horizon appear through C and A. thus you have the fun's altitude; and adding the degrees on the arch ed to the degrees on the arch FG, gives the zenith distance.

To obtain the meridian altitude, continue obferving; and as the fun rifes higher, the fea will appear through the vanes C, A; then the vane Cis flill to be mov'd lower, till the fun be at the highest; and when the fun begins to fall, the sky will appear through the vanes A, C; and then it is

time to give over observing for that day.

But note, the refraction makes the fun or a star FIG. appear higher than he is, when near the horizon, 3. and therefore the zenith distance must be increased (or the altitude diminish'd) according to the following table.

Altit.	Refraction.	Zenith. dist. deg.	Altit.	Refrac- tion. min.	Zenith. dist. deg.
0	33	90	7	7	83
1	23	89	8	6	82
2	17	88	10	5	80
3	13	87	12	4	78
4	9 8	86	16	3	74
5		85	24	2	66
6		84	42	1	48

There is a late invented instrument call'd Hadley's Quadrant, for taking altitudes more exactly. But I shall not describe it here, because there is a little book which goes along with the Instrument; and that gives the description of it at large, and the use of the instrument in taking an observation.

4. The Cross Staff, or Fore-staff.

This instrument is used to take the altitude 4. of a star. It consists of a staff AD, and three or four crosses BC, to suit different altitudes. The staff AD being graduated on each side, in a different manner for the different crosses.

In using it, put on the proper cross CB, then placing the end A as near the eye as possible, and turning the face to the star, move the cross CBB A

USE OF INSTUMENTS.

end C, and the horizon at the lower end B; then you have the altitude number'd on the inner edge of the cross, and on that side of the staff belonging to the cross you observe with.

For the meridian altitude; continue observing till the sea begin to appear, instead of the horizon;

and then your observation is finish'd,

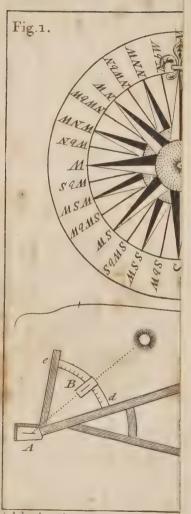
8

5. The Lead.

This is a heavy piece of lead, with a line fasten'd to it, divided into fathoms, to found the depth of the fea, in shoals and places near the shoar.







Navioation.

NAVIGATION.

PART I.

The Solution of astronomical Problems, also concerning Lee Way, Variation of the Compass, taking Observation, and several other Things useful in the Art of Navigation.

PROB. I.

To find the Moon's Age.

RULE.

1. DIVIDE the year of Christ (which begins with March) by 19. and keep the remainder. Note, if o remain take 19.

2. Multiply that remainder by 11, and divide

by 30, and note this remainder.

3. To the last remainder add the number of the month, beginning at March, and the sum taken from 30 (or 60) gives the day of the change Or that sum added to the day of the month, gives her age; rejecting 30 if it exceed: according to the new stile.

Note, the last remainder is the epact, and a added to the first remainder is the golden number. This rule seldom misses above a day.

B 5

Other-

Otherwise: The moon's age is easiest and truest known by an almanack, or else by a mariners calender; one or both of which a navigator should never want.

Example. Aug. 27th 1754. N. S.

19)1754(92	6	6 Rem.	12
1.71	11	6 Month.	27 day.
-			-
44	30)66(2	12 Sum.	39.
38	60	30	30.
-		broom	derina de la composição
6 Rem.	6Rem.	18 Change.	9 Age.

PROB. II.

To find the Time of the Moon's Southing.

RULE.

Take 8 tenths of the moon's age for her fouthing.

Or thus, by the Nocturnal.

In the middle piece against the moon's age, in its proper circle, stands her southing in the circle of Hours.

Otherwise, by seeing the Moon.

The time of the moon's fouthing may be nearly conjectured by observing the quantity of her enlightned side. For so many 12th parts of her whole hemisphere as is contain'd in her illuminated arch

arch (on the right hand), fo many hours fhe fouths after 12 o'clock: If on the left hand, it is before 12.

Example.

On Aug. 27th 1754, the moon is 9 days old; then,

So she souths about a quarter past 7 o'clock.

PROB. III.

To find the Time of High Water at a given Place.

RULE.

By the following tide table, find the time of full fea, on the full or change day, for the place proposed; add this to the time of the moon's southing.

Otherwise, by the Nocturnal.

Set 12 o'clock on the middle piece, to the time of high water at the new or full moon, on the great piece; then bring the long index to the moon's fouthing, or age on the middle piece; this cuts the inner circle, (the circle of hours) of the great piece, as required.

Example.

At the Lizard, Aug. 27th 1754. it is full sea at 7:30. at the full, by the table. And the moon B 6 fouths

fouths at $7\frac{1}{4}$, the fum is $14\frac{3}{4}$: that is 3 quarters past 2, the time of high water.

SCHOLIUM.

Some general observations relating to the tides, are as follow:

1. About the quarters of the moon the tides happen something sooner, but in some places something later. Thus, at London these tides happen an hour sooner; and at Dublin half an hour later.

2. The nearer the moon comes to the zenith or nadir of any place, the greater is the tide. And therefore in north latitude, when the moon has north declination, she makes greater tides when above the horizon, and past the meridian, than when she is under the horizon. And consequently in north latitudes the evening tides are higher than the morning tides in summer; and the morning tides higher than the evening tides in winter. And the contrary in south latitudes.

3. The highest tides make the lowest ebbs.

4. The highest spring tides in the year, are always about the beginning of March, and end of September; but the neap tides (or quarter tides) are least at that time, and greatest in June and December. Therefore the greatest tide at the new and full moon is always succeeded by the least at the quarters.

5. The highest monthly tides are always about

the 3d day after the full or change.

6. The tides, ceteris paribus, are greatest under the equinoctial; and greater in lesser latitudes than in greater latitudes.

7. Tides are greater in greater seas than in lesser seas; and greater at the shores than in the middle of the sea, or in islands far from the continent.

8. Within

8. Within the mouths of rivers the tide ebbs longer than it flows.

9. The motion of the water is greatest about half flood or half ebb; and at high or low water is

little or nothing.

10. Great winds fetting the fame way as the tides, will bring them fooner, and make them run higher: But if they be contrary, will retard them.

A Tide Table, shewing at what Hour it is High-Water on the full and change of the Moon.

· A			
`		h. '	m.
A BERDEEN	100	12	45
Abermorith		. 6	0
Aberwark		2	15
Abroth -	-	. 5	15
Africa W. Coast -	3 4 3	3	Õ
Aldborough	100	9	45
Amazon's R. Mouth	-	6	0
Ambletense - =	35	II	0
America W. Coast		3	. 0
E. Coast	~ -	4.	30.
Amsterdam	12	/ 3	- 0
Antwerp	- 69	6	0
Apenars -	· · - · ·	12	45
Apenmark -		2	15
Archangel -	- 1	6~	0
Armentiers	. in / '	3	, 0
Army :	- 4	4.4	30
Audiern -	*** ·**	2.	15
Auray -	- /	12	45
В			
Bajador	m 1	12	0
		Raltan	ore

	h.	m.
Baltamore	4	30
Barfleur	8	0
Barneville -	7	0
Bafs, without	3	45
Bayonne +	'3	30-
Beachy	12	0
Beauvoir -	3	45
Bell I.	· I '	30
Bermudas -	. 7	. 0
Berwick -	· 2	15
Biscay Bay	3	0
Blackness	I	30
Blackney -	6	0
Blacktail Beacon -	12	15
Blanquet Race	12	O
Blavet	· 3	0
Bloy	. 4	30
Bluet, without	, 2	15
Bologne	11	0
Bourdeaux	. 6	0
Brafile Coast	- 4	30
Bree Sound	4	30
Bremen	. 6	. 0
Brest	3	. 30
Bridgewater	7	30
Bridlington	4	0
Briftol	- 6	0
Key	: 6	45
Brovage, without -	3	45
Buchaness -	3	0
Bulloign	IQ	. 30

C

Caen To O Caldy

	h.	m.
Caldy -	5	.15
Calice	11	·- 0
Calfhot -	EX	15
Camfere -	I I	30
Canary If.	3.	0
Cancale	6	, .0
Cape Blanco	9	45
Cantin	12	0
Clear	4	30
— De Four -	2	45
- Of Good Hope	3	0
Sierre Lion	8	15
Carmarthen Bay -	5	15
Carnarven Bay	5	15
Cafkets -	9	45
Caskets without -	8	15
Chamberness > =	9	45
Cherburg -	9	0
Chily Coast	3	9
Concarnean	3	0
Condado	12	0
Conquet	3	10
Cork	4	30
Corpus Christi Point -	I.	30
Cows	10	30
Creyl	II	15
Cromer	. 7	0
D		
Dartmouth	5	15
Derby	.2	15
Defire Port	12	0
Dieppe.	10	Q
Dort	3.1	, 0
2	Do	ver

	9	
	h.	m.
Dover	10	30
Dover Port	12	0
Downs	I	15
Dublin Bar	10	O
Custom-house -	II	9
Dunbar	2	0
Dundee	2	15
Dungarven -	4	30
Dungeness	9	45
Dunkirk	12	0
Dunnose	9	45
Dunwich	9	45
E		
•		
Edam	I	30
Edinburgh	4	30
Egmon -	.4	30
Eider 2	12	0
Elve. "	12	O
Emden	12	0
Emes	9	0
Emes Entrance -	7	30
Enchuyfen -	12	0
Engomonts	9	-0
Estaple	ΙÍ	Ø
Exwater	7	30
	•	
F		
Fair I.	12	0
Fair I. Roads	11	15
Falmouth	4	30
Fen .	1	30
Fefcan -	: 0	45
3	Finn	

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F: 1 0 1		h. m
Finmark Coast	-	1 30
Flamborough Head		4 0
Flanders Banks	-	1 0
Florida -	-	7 30
Flushing -	-	0 45
The Fly -	-	7 30
Foreland, N. and S.	-	9 45
Forn -	-	5 15
Foulness -	-	6 45
Fountenay Race	_	2 15
Foy -		5 15
France W. Coast		3 0
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Friesland Coast	_	7 30
a Holland Coale		1 30
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Galicia -	-	3. 0
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Garande Garonne Mouth Gafcoin Gibralter Road Goree Gorend Granville Gravelling Gravfend Groyn		12 • 1 30 11 15 7 0 12 0 1 30 3 •
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Garande Garonne Mouth Gafcoin Gibralter Road Goree Gorend Granville Gravelling Gravfend Groyn Guernfey H Hague Hamborough		12
Garande Garonne Mouth Gafcoin Gibralter Road Goree Gorend Granville Gravelling Gravfend Groyn Guernfey H Hague		12

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Harlem	1 #0	9	0
Hartlepool		3	0
Harwich -	2 4 7	II	0
Haver-de-grace	* #0	9	0
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Hever -	, m	12	
Holms -	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		0
Holy-Head		I	30
Home Head	-7	9	. 0
Honfleur		9	- 0
Horn 7	-	1	30
Hull	general Control	6	0
Humber Mouth	-	5	15
Hunclif Foot	-	3	45
1			
-			
John de Luce		10	. 30
Ireland S. Coast	-	5	15
Ireland W. Coast	-	3	ð
Jutland Is	622 00 00 2.12	12	. 0
K	1311 37 %	45.0	
Kentish Knock -	-	12	2 0
Kildive -	, + ,,	9	0
Kilduyn -		7	30
Killiars -	.	3	0
Kingfale -		4	30
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Y1		. 0	P ===
Lambay -		0	15
Landfend		: 7	30
Lanion		. 0	45
Lawreness -		4	30
			Leith

	7.	
Table	h.	m.
Leith	4	. 0
Lenow	9.	45
Leystaf	9	45
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Lifbon	2	15
Lizard -	7	30
London	- : 3	, 0
Longfand Head	10	30
Loyr Mouth	3.	. 0
Lundey -	5	15
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Mackwell's Caftle -	8	15
Maes 7	38	45
Magnes Sound -	8	15
Malden -	12	45
Man I.	. 9	0
Marget Road -	11	15
Memissan -	3	30
Milford	:5	13
— Haven	7	30
Moonless	5	15
Morbihan	3	0
Mounts Bay	4	30
Mousehole	4	30
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N		
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Nantz River	3	0
Naze	11	15
Needles	9	-0
Newcastle -	5	15
Newcame	Newp	
7 ' '	S.temb.	

	23,	
	h.	m.
Newport (I. Wight) -	12	O
Nore -	12	0
Normandy Coaft -		
Normandy Coalt	10	30
O		
Ollonne	3	15
Orfordness	10	0
Orkneys -	6	0
Orwell -	9	0
Oftend -	12	0
Onema	12.	
D		
P		
_		
Pens	3	0
Peru Coast	3	. 0
Peterport	8	15
Picardy Coast	10	30
Plymouth.	6	0
Podesemsk (Russia) -	6	45
Poictou S. Coast		
Port Blank	3	. 0
	4	30
Porthus -	38	0
Portland	8	15
Portugal Coast	3	45
Portsmouth	12	. 0
·· O ·· ·		
. ~	-	*
Quebeck (Canada) -	6	0
Quinborough	_	
Quinbolough	12	0
7. A.		
R		
Ramkins	I	30
	Ra	mley
		- 4

	h.	m.
Ramsey	. 5	15
Rebdan	12	45
Rhee L	3:	0
Rhodes -	II	15
Robin Hood's Bay -	3	0
Rochel	3	45
Rochester	12.	45
Rohan -	: 3	45
Rotterdam -	3	0
Roven	10	30
Rumney	I	30
Rye	11	15
S		
C . Andrews		12.20
Saint Andrews	:2	15
Augustine (Florida) David's Head	7.	30
Helen's		
John de Luz	10	30
Lucas -	3	15
- Malo's		30
- Mark	· 5	15
- Matthew's Point -		45
— Nicholas (Ruffia)	3	45
- Paul de Leon	4	. 0
— Powis	6	0
Valleri J		45
Salconrb	. 9	. 0
Scarbrough	3	45
Scilly Islands	3.	45
Sedmouth	6	45
Senegal S	IO	130
Seven Clifts	0	. O
Seven Isles	4	30
	Şe	vern

A LIDE LAD.	L E.	/
28 · ·	h.	m.
Severn Isles	4	30
Severn Mouth	. 5	15
Seyn Mouth -	9	0
Sheerness -	12	0
Shelbergh -	9	0
Shetland -	3.	. 0
Shoe	12	0
Shoram -	9	45
Sleeve 6	12	0
Somme Mouth	11	0
Sound	3	45
Southampton -	12	0
Spain W. Coast	3	0
Spits	12	0
Spurn	5	15
Staples -	3	45
Start	. 6	45
Stockton -	5	15
Swin -	12	0.
T		
Tees Mouth		
Tenerif -	3	
Tenet -	3	0
Terveer, within	I	30
Terveer without	12	45
Tergon -	I	30
Texel -	9.	45
Texel Cliffs	7	. 0
Thames Mouth	5	
Tinmouth		30
Torbay -	3	0
Treport	5	15
- report	10	30

U	
Vannes Voard Urek Ufe Ufhant within	h. m. 12 45 4 30 12 0 3 0 4 30
W	
Wales Wafh, (Lincolnf.) Waterford Weilands Wells Weymouth Weymouth Wieringham Whitby Wieringham Whight I. Winchelfea Winterton	5 15 6 30 6 0 1 30 6 0 6 0 6 45 3 0 7 0 12 0 12 45 8 0
Yarm Yarmouth Roads Younghall, (Ireland)	6 45 10 0 10 30 4 30
Z	
Zeland Coast Zerick Sea	3 0
4	PROB.

PROB. IV.

The Latitude of the Place, and the Sun's Declination given; to find his Amplitude.

RULE.

As cofine lat.
Radius.
Sine of the declination.

Sine of the amplitude.

The amplitude is fouth if the declination be fouth; and north, if north.

Note, The declination is had by the Table, after

Prop. 13.

PROB. V.

The Declination, Altitude, and Azimuth of the Sunbeing given; to find the Hour.

RULE.

As cof. declination.

Cos. altitude. Sine azimuth.

Sine of the hour angle.

This turn'd into time, allowing 15 deg. to an hour, gives the distance of time from noon or midnight, for it is doubtful sometimes whether it is.

PROB. VI.

Given the Latitude and Sun's Declination; to find the Time of Sun-Rising.

RULE.

RULE.

As radius,
Tan. latitude,
Tan. declination,
Sine afcentional difference.

This turn'd into time, allowing 15 deg. to an hour, will show how long the fun rifes before 6, when his declination is towards the elevated pole; but after 6, when his declination is the contrary way.

PROB. VII.

Given the Sun's Declination and Amplitude; to find the Latitude.

RULE.

As fine amplitude, Radius, Sine declination, Cof. Latitude.

PROB. VIII.

Given the Sun's rising and Declination; to find the Latitude.

Find how long the fun rifes before or after 6; and turn this time into degrees, allowing for every hour 15 deg. and four minutes of time for one degree; call this the ascensional difference; then,

RULE.

As radius,
Co-tan. declination,
Sine afcentional difference,
Tan. latitude.

5

wards the elevated pole: If after 6, the declination is tois towards the depress'd pole.

PROB. IX.

Given the Declination and Meridian Altitude of the Sun or a known Star; to find the Latitude. Or to work an Observation.

RULE.

Take the altitude of the fun or star with the quadrant, and subtract it from 90; and the re-

mainder is the zenith distance.

Describe the semicircle SZN for the meridian, SN the horizon, S the south point, N the north. Biffect SZN in Z for the zenith. Then if the observed altitude be south, set the zenith distance from Z towards S; (but if north, towards N), let it be at *.

Then if the declination be north, fet it from * towards S, (but if fouth towards N), suppose to E. Then is E Z the latitude, which is north, when Z is between E and N; but south, if Z is between E and S; and EC will be the equinoctial.

And thus a figure may be drawn by hand, to fhew when you are to add the declination and zenith distance together, or when to subtract the one from the other; for finding the latitude.

PROB. X.

Given the Altitude, Declination, and Azimuth of the Sun, or a known fixt Star; to find the Lasitude.

The

The azimuth is reckon'd from the north. FLOR Subtract the altitude from 90, the remainder is the zenith distance: then.

RULE.

As radius. Cof. azimuth, Tan. zenith distance. Tan. an arch A.

Then fine altitude, Sine declination. Cof. arch A. Cof. arch B.

Then the difference of the arches A and B fub-

tracted from 90 gives the latitude.

Note, If the observation be made between 6 and 6 in the day; and at the same time the azimuth is less than 90; then you must subtract the sum of the arches A and B from 90.

PROB. XI.

The Latitude of two Places, and their Difference of Longitude being given; to find the Angles of Position; or the bearing of one Place from another, in the Arch of a great Circle.

RULE.

Let A, D be the two places; find the distances 6. of the two places from one and the fame pole, as the north pole P, and add these two polar distances together, and subtract them from one another to find their fum and difference, then fay,

As Cofine of ½ fum,
6. Cof. ½ difference,
Cotan ½ difference

Cotan. ½ difference of longitude,

Tan. of an arch B.

Where note, if ! sum be greater than 90°, B is greater than 90, otherwise less. Again,

As fine of ½ fum,

Sine of ½ difference,

Cotan. ½ difference of longitude,

Tan. of an arch G.

There the sum of the arches B and C is the angle of position at the place of greater latitude, or nearest the pole. And the difference of B and C is the angle at the place of lesser latitude, or furthest from the pole.

SCHOL.

Upon this prop. great circle failing depends. If the places be far diftant from one another, there will be a confiderable difference between the angle of position, and the course or bearing upon the rumb; and likewise in the distance: a great circle being the nearest distance between any two places. But it is very difficult for a ship to fail exactly upon the arch of a great circle; because she must be continually altering her courfe. And to know exactly the course every moment, it must be computed for all points of the arch, which will give more trouble than advantage. Yet if any have a mind to keep near a great circle in failing from one place to another, as from A to D; he must procoed thus, first let him compute the angle of position . t 1, which is the course he must steer at first. Then after failing some distance upon this course,

as 60 or 70 leagues, let him compute the place of FIG. the ship, as at e. Then there will be given the 6. lat. and diff. longitude of the two places e, D (as before of A, D): Then compute again the angle of position at e, by this prop. as before; and this is the course to steer from e. And so on from one place to another.

PROB. XII.

To find the Time of the Southing of a given Star, on a given Day.

RULE.

In the following tables, find the right ascension of the sun for the time given, and likewise the right ascension of the star; and subtract the right atcention of the fun from the ftar's right afcention, adding 24 hours if the stars be less; then the remainder is the time of the star's fouthing, from noone

Or, subtract the star's right ascension from the fun's, gives the distance of time before noon.

2 Example.

To find when Syrius or the great Dog fouths, Feb. 20th 1756. London. N. S.

Right ascension of Syrius Add	h. 6 24	m. 33 0
Sun's right ascension Feb. 19th (leap year).	30 22	33
The Hour.	8	18
C 3	RC	B.

PROB. XIII.

To find what Star fouths at a given Hour of a given Day.

RULE.

Find the sun's right ascension for the day, in the following table of the sun's right ascension; to this add the given hour, counted forward from noon. Look for the sum, or the nearest to it, in the following table of the star's right ascension; and against it you will find the star sought.

Note, If the sum exceed 24, reject 24.

Example.

What star souths at 3 o'clock in the morning on OA. 13th, 1755. London.

Time given, Oct. 12th. Sun's right afcension,	h. m.	
Sum.	13: 12 28: 14 24	
or,	4: 12	

h. m. h. m.
The nearest to 4:12 is 4:20. So Aldebaran is the star required.

Of the Sun's right Ascension in Time, and his Declination, every Day at Noon; to the Meridian of London.

To find the Sun's right Ascension or Declination to a given Time.

RULE.

1. Find the month on the top of the page, and the day on the fide; then over against the day, in the proper column of the month, is the right afcension or declination. But note,

2. In leap year, reckon for a day less in January

and February.

3. For the 1st, 2d, or 3d year after leap year, reckon for $\frac{1}{4}$, $\frac{1}{2}$, or $\frac{3}{4}$ of a day sooner.

4. Also for every 15 deg. E. longitude from London, reckon for an hour fooner: and later for W. longitude. Also make allowance for any time after noon.

N. B. Leap year is known by dividing the year of our Lord by 4; the remainder shews the num-

ber of the year.

Examples.

1. According to these directions, the sun's right ascension, May 14th 1756 (being leap year), at noon is 3 h. 26 m. And at 6 o'clock at night is 3 h. 27 m.

And for Aug. 10, 1754 (the 2d after leap year) his right ascension at noon is 9 h. 21 m. and at 6

in the morn. is 9 h. 20 m.

2. The fun's declination Jan. 27, 1752 (or leap year), at noon is 18 d. 36' S. And Oct. 22, 1753 (the 1 after leap year), at noon it is 11° 12' S. and at midnight it is 11° 22'.

SUN's

Day	1	Janu	ary	.] .	Febru	iary			Mar	ch.	
19.	R. H.	Afc. M.		Dec. M.	R. H.	Afc M.	0.	Dec. M.	K. H.	Aic M	OI D.	
1 2 3 4 5	18 18 19	49 54 58 2		S r 55 49 43 36	2 I 2 I 2 I 2 I 2 I	3 7 11 15	16 16 16 16	S 59 42 24 6 48		52 55 59 3	7 6 6 6 5 5	\$ 21 58 35 12 49
67890	19	12 16 20 25 29		29 22 14 5	2 I 2 I 2 I 2 I 2 I	23 27 31 35 39	-	29 10 51 32 12	2 3 2 3 2 3	10 14 18 21 25	5 5 4 4 3	25 2 39 15 51
13	19	33 39 43 48 52	21	47 35 25 14 3	2 I 2 I 2 I 2 I 2 I	47 51 55	13 13 13 12	5 ² 31 11 50 29	2 3 2 3 2 3	29 32 36 39 43	5	27 4 40 16 53
17 18	19 20 20 20 20	56 0 4 8 13	20	52 40 28 15	22 22 22 22 22	3 7 11 15	11	8 47 25 4 42	23	51 54 57	0	29 5 42 18 N.6
21 22 23 24 25	20	17 21 26 30 34	19	49 35 21 6 51	2 2 2 2 2 2 2 2 2 2 2 2	21 25 29 33 37	9	20 59 36 14 51	000	12	I	30 53 17 40 4
26 27 28 29 30 31	20	47 51 55	18 18 18 17 17	36 20 5 49 33		1 1	. 8	2 9	0	27 30 34 37	3 3 4	28 51 14 37 0

April.					1	M	ay.			Jui	ne.	
ys.	R H.	Afc M.	0 D.	Dec. M.	R. H.	Afc. M	0 l D.	Dec. M.	R. D.	Afc.	0. D.	Dec. M.
1 2 3 4 5	0 0 0 0	45 48 52 56 59	4 5 5 5 6	N.46 9 32 55 18	2 2 2 2	36 39 43 47 51	151 15 15 16 16	33 50 8 25	4 4 4 4	39 43 47 51 55	22 22 22	N. 8 16 24 31 37
6 7 8 9	I I I I	3 6. 10 14 18	6 7 7 7 8	41 3 25 48 10	2 3 3 3	55 59 2 6	16 16 17 17	42 58 15 31 46	4 5 5 5 5	59 3 7 11 16	22	44 50 55 0
11213	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	21 24 28 32 36	8 8 9 9	32 .54 16 37 59	3 3 3 3 3	14 18 22 26 30	18 18 19	2 17 32 46	5 5 5 5	20 24 28 32 36	23 23 23	9 13 16 19
16 17 18 19 20	I	40 43 47 51 54	10	20 41 2 23 43	3 3 3 3	34 38 42 46 50	19	14 28 41 54 7	5 5 5 5	40 45 49 53 57	23 23 23	24 26 27 28 29
21 22 23 24 25	1 2 2 2 2 2	5 9	1 2 1 2 1 2 1 3	4 24 44 3 22	3 3 4 4 4	- 1	20 20 20 20 20	19 30 41 52 3	6 6 6	10	23 23 23 23 23	29 29 28 27 25
26 27 28 29 30 31	2 2 2 2 2	20 21 28	13	42 1 20 38 57	4 4 4 4 4	18 22 26 31	21 21 21 21 21 22	14 24 33 43 52 0	6 6 6	27 31 35	23 23 23 23 23 23	23 21 18 15

Days.		July. August.						Se	epter	mber	-
ys.			Dec. M.	R. H.	Afc M	O D.	Dec. M.	R. H.	Afc M	Э I).	Dec M
1 2 3 4 5	6 6	43 23 47 23 51 22 55 22 59 22	58 53	8 8 8 8	48 52 56 59 3	17	V.57 42 26 10 54	10	4. 4. 51 5- 58	8 I 7 7 7 6	45 23 0 38
6 7 8 9	7 1	4 22 8 22 1 2 22 1 6 22 2 C 22	36 29 22	9 9 9 9	7 11 15 19 22	16 16 16 15	37 21 4 4(20	11	2 5 9 13	6 5 5 4	16 53 30 8 45
11 12 13 14 15	7 2 7 3 7 3	24 22 28 21 32 21 36 21	6 57 48 39 30	9 9 9 9	26 30 34 38 41	14	52 34 15 5(11	19 25 25 30 34	4 3 3 3 2	59 36 13 50
16 17 18 19 20	7 4 7 5	5 21 9 21 2 20 6 20 0 20	48	9 9 9 10	45 49 53 57	13 13 12 12	36 17 58 38 18	II	38 41 45 48 5 ²	2 2 1 1 0	26 3 40 16 53
21 22 23 24 25	8 1	4 20 8 20 2 20 6 19	26 14 2 49 36	10 10 10 10	4 8 11 15	II II IO IO	58 38 18 57 36	11 11 12 12	56 59 3 7	0 0 0 0 0	29 6 .17 41
26 27 28 29 30 31	8 2 8 3 8 3 8 4	4 19 8 19 2 18 6 18 0 18	23 9 55 41 27 13	10 10 10 10	22 26 30 33 37 40	10 9 9 9 8 8	15 54 33 12 50 28	1 2 1 2 1 2 1 2 1 2	14 18 21 25 28	1 1 2 2 3	28 51 15 38 1

R. Afc O Dec R A(c O Dec. H. M D. M. H. M. D. M. M. H. M. D. M. M. H. M. D. M. H. M. D. M.	ec· M.
H. M D. M H. M D. M H. M. D. M H. M D. M H.	M. 56
1 12 32 3 S.25 14 29 14 S.38 16 33 21 S. 2 12 35 3 48 14 33 14 57 16 37 22 3 12 36 4 11 14 37 15 16 16 42 22 4 12 42 4 35 14 41 15 35 16 46 22	56 5 13
2 12 35 3 48 14 33 14 57 16 37 22 3 12 35 4 11 14 37 15 16 16 42 22 4 12 42 4 35 14 41 15 35 16 46 22	5
2 12 35 3 48 14 33 14 57 16 37 22 3 12 35 4 11 14 37 15 16 16 42 22 4 12 42 4 35 14 41 15 35 16 46 22	5
3 12 35 4 11 14 37 15 16 16 42 22 4 12 43 4 35 14 4 15 35 16 46 22	13
412 43 4 35 14 41 15 35 16 46 22	
	die 1
5 12 46 4 58 14 45 15 53 16 50 22	29
6 12 50 5 21 14 49 16 11 16 54 22	36
7 12 54 5 44 14 53 16 29 16 58 22 8 12 57 6 7 14 57 16 46 17 322	43
	49 55
9 13 1 5 30 15 117 4 17 7 22 10 13 5 6 53 15 5 7 21 17 12 23	0
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11 13 9 7 15 15 9 17 37 17 16 23	5
12 13 13 7 38 15 13 17 53 17 21 23	10
13 13 17 8 0 15 17 18 9 17 25 23 1413 20 8 22 15 21 18 25 17 29 23	14
	17
15 13 24 8 45 15 25 18 40 17 34 23	
16 13 28 9 7 15 29 18 55 17 38 23	23
17 13 31 9 29 15 33 19 10 17 43 23	25
18 13 35 9 51 15 37 19 24 17 47 23	27
19 13 39 10 12 15 41 19 38 17 52 23	28
20 13 43 10 34 15 46 19 52 17 56 23	29
21 13 46 10 56 15 50 20 5 18 1 23	29
22 13 50 11 17 15 54 20 17 18 5 23	29
23 13 54 11 38 15 58 20 30 18 9 23	28
24 13 58 11 59 16 3 20 42 18 14 23	27
25 14 2 12 20 16 7 20 54 18 19 23	25
2614 512 40 16 1121 5 18 2323	22
	23
27 14	18
29 14 17 13 40 16 24 21 37 18 36 23	14
20 14 21 14 0 16 28 21 47 18 41 23	10
31 14 25 14 191 118 45 23	6

C 6

A TABLE of the right Ascension in Time, and of the Declination and Magnitude of the principal fixt Stars, to the Year 1752; and 30 Years after, without any sensible Error.

Stars.	Af	ight cen. M.	n	Decli- ation. M.	Magn.
Whales fouthern tail.	0	21	-	22 S.	2
Pole star.	0		87	59N.	21
Caffiopeia's hip.	0		59	23N.	2
Last in Eridanus, Acarnar.	I		5 8	44 S.	
Bright star of Aries.	I		22	7N.	2
Whales jaw, Cetus.	2	47		58N.	2
Brightest of the 7 stars.	3		23	18N.	3
Bull's Eye, Aldeharon.	4		16	oN.	1
The Goat, Capella.	4	57	45	44N.	1
Orion's foot, Rigel.	5	2.		33 S.	1
Middle of Orion's belt.	5	23	1	23 S.	2
Orion's right shoulder.	5 5 6	41		20N.	1
Ships rudder, Canopus.		18	52	33 S.	1
Great dog, Sirius.	6	3 3	6	22 S.	1
Northern twin, Castor.	7	18		30N.	2
Little dog, Procyon.	7	26	5	52N.	1
Southern twin, Pollux.	7	28	8	42N.	2
Hydra's heart Alphard.	9	14	7	26 S.	2
Lions heart, Regulus.	9	55	13	12N.	1
Lower pointer.	IO	45	57	42N.	2
Upper pointer.	10	47		6N.	2
Lions tail.	ΙI		16	ION.	1
Foot of the crossers.	12	12		24 S.	2
Great bears rump, Allioth.	12	431	57	21N.	2
Virgin's spike, Azimech.	13	10	9	50 S.	1
Last in great bear's tail.	13	38	50	50N.	2
Arcturus.	14	3	20	30N.	1
Centaurs right foot.	41	23		46 S.I	1
				Lit	tle

Stars.	Ri Af H,	ght cen. M.	D na D.	eclina- ation. M.	Magn.
Little bear.	14	50	75	20N.	2
Northern crown, Ariadne.	15		27	35N.	2
Scorpions heart, Antares.	16	13	25.		
The harp, Lyra.	18	28	38	30N.	1
Eagle or vultur's heart, Aquila.	19	37	8	14N.	I
Swan's tail, Deneb.	20		44	23N.	2
Southern fish, Fomelhaut.	22	41	30	55 S.	1
Pegasus's wing, Marcab.	22	51	13	50N.	
Andromeda's head, Alpheratz.	23	53	2.7	44N.	2

PROB. XIV.

To calculate the Eclipses of the first Satellite of Jupiter; for the Meridian of London.

r. Out of Tab. I. take the time for the year, month and day &c. next less than the day proposed; and also the correspondent numbers A and B, and add them all up in separate columns. Thus you have the mean time of the iniddle of the eclipse.

2. Out of Tab. II. with number A, take the equation of number B, to be added to B. Take also another small equation for B out of Tab. III. for the day of the month, to be added to B likewise.

then call this numb. C. Also,

3. From Tab. II. with number A, take out the 1st equation, and with number C, the 2d equation; and then add these equations and the mean time together; and you have the true equated time of

the middle of the eclipse.

4. From Tab. II. with numb. A, take out the femiduration; and if number C, be less than 500, subtract the semiduration, and you will have the mean time of the beginning or Immersion: But is more than 500, add it; and you have the mean time of Emersion, or end of the eclipse. 5. Lastly,

5. Lastly, out of Tab. III. take the equation of time, for the day, and add or subtract as the table directs; and you have the apparent time reckon'd from noon.

N.B. In leap year after February, one day is to be deducted from the day of the month. Also if the eclipse happens in the day time, add one Revolution 1 d. 18 h. 28 m. 36', gives the time of the next eclipse. When the numbers A or B exceed 1000, reject 1000. When the numbers cannot be found exactly in the tables, you must take a proportional part of the difference, as is usual.

This fatellite never goes fo far as 21 of Jupiter's

diameters, from his Body.

Example I.

To find the Time of the Eclipse, Jan. 29th 1754.

So the beginning of the eclipse happens 29th Jan. at 15 h. 43 m. after noon, or 3 h. 43 m. after midnight.

Example

Example II.

To find the Time of the Eclipse of Jupiter's first Satellite, July 15th, 1752. N. S.

	D	. H.	M.	S. A	B
1752.	1	9	20	57 65	0 5841
July.	I	7	5	44 4	2 450
Day.	14	3	48	48	3 37
Mean time	16	20	15	2969	5 71
-				Á	0
	15	20	15	29	3
1 Equa.		Ί	17	50	
2 Equa.			13	21	74
	15	21	46	40	Ci
Sub.	13	I	6	40 20 S	emidur.
					cialidui.
	15	20	40	20 I	mmerf.
Sub.	,		5		q. time.
	15	20	35	4	

So the eclipse begins on July 16th, at 8 o'clock, and 35 m. in the morning. But because this happens in the day time, add one revolution, viz.

1 18 28 36

Then 17 15 3 40 is the time of immersion.

So the eclipse begins 15 h. 4 m. after the noon of July the 17th, or which is the same thing, on July 18, at 3 m. 40 s. past 3 in the morning.

But by the old style it happens on July 7th in the morning.

T A B. I.

			4 -	,			779990 V 1000
1 Y	cars		The	Time		Numb.	Numb.
	rent.	D.	. H.	M.	S	A	P
	-	-		.*	-	10.1	-
	1750	0	10	29	`26	481	752
	1700	O'.	. 0	40	53	566	665
	1751			20	57	650.	584
	52	7.	13	I) / I	735	502
	53	I	8	12			416
	34	1	2.2		29	019	
	55	-	L. L.	23	56	903	330
	1;56	0	12	35	24	987	241
1	57	0	21	15	28	72	163
1	58	0	11	25	55	-157	75
	59	0		38	: 22	241	990
1	6c		10	18	26	325	909
1	-			1 ()	20	3-)	
A.Francis	1761	0	0	29	5 3	410	823
1	(:2)	1	9	9	57	494	741
1	6;	0	23	21	24	578	655
	6.4	0	13	32	52	601	570
		2	22	12	55	746	488
	ACR-HAMMANA	-			-	- Automotive	
1	1,60	0	12	24	23	830	403
aver 18	67		2	35	50	914	317
Ī	68		1 1	15	54	999	2.35
	69		I	27	21	83	149
1	70	1	10	7	2.5	167	68
	1771	I	O	18	52	252	982
1	172	C	14	30	20	336	896
1	-73	C	. 23	01	24	420	814
	740	С	13	21	52	504	728
	7.5	3	3	33	101	589	641
	-						-
	1776	I	12	13	23	673	560
1	- gate	0	2	24	50	757	474
	.784		- 11-0	4.	. 53	842	392
	70		- 1	16	20	926	306
	1780		15	27.	481	. 10	220
				, ,	7		
	1781	Ť	. 0	7	52	95	130
1	1			/	2 ~1	7)	1 66.

TAB. I.

Months.	D	The '.	Time.	s.	Numb. A	Numb. B
January. February. March. April.	0 0	0 20 4 6	0 34 12 18	47 23 34	0 7 14 21	82 152 226
May. June. July. August.	0 1	8 4 7 9	24 59 5	4-5: 3-2: 4-4: 5-5:	28 35 42 49	300 377 450 524
September. October. Novem. December	I I O O	5 7 9	46 52 59 5	42 54 5 16	56 63 70 77	603 679 758 836
Days, Hours, &c.	0 1 3 5 7 8	0 18 12 7 1	0 28 57 25 54 23	0 36 12 48 24	0 0 1 1 2 2	0 5 9 14 18 23
	10:	14 9 3 22 16	51 20 48 17 46	36 12 48 24	2 3 3 4 4	27 32 37 41 46
,	21 23 24 25	5 0 13	14 43 11 40 8	3(12 47 22 5(4 5 5 6	51 55 60 64 69
	1,	7 2 20	37 6 34	35	7 7 7	73 78 82

TAB. II.

N	ımb.	Eq.	ı E	qua.	2 E	jua.	Se	mid	ur.
A	or C	of B.	M.	S.	M.	S.	H.	M.	S.
-	0	15	42	38	14	0	I	5	9
	20 40 60 80	17 19 21 22 24	37 33 28 24 20	24 55 34	13 13 13 13	57 49 36 16 52	I l I	4 4 4 4	44 23 7 1
	120 140 160 180 200	25 27 28 29 30	16 13 9 7 5	5 56	12 11 11 10 9	23 49 13 31 45	I	4 4 4 5 5	6 2 I 42 9 38
	220 240 260 280 300	30 30 31 31 30	3 2 1 1 2	20 15 44 49 34	8 7 6	58 7 16 22 30	I	6 6 7 7 8	11 43 15 45
	320 340 360 380 400	30 29 28 26 25	3 8 11 15	56 56 31 40 21	3 2 2	38 48 59 15	I	8 8 8 8 7	22 28 27 17 58
	420 440 460 480 500	23 21 19 17 15	19 24 28 33 39	57	0	35	I	7 6 6 5 5	31 58 20 45

PARTI. ASTRONOMICAL TABLES. 43

TAB II.

-	Numb. A or C.	Equ.	I	Equ	ia.	2 E M.	qua. S.	Se	mid M.	ur.
-	A OI C.	OI D.	11.	IVI.	٥.	IVI.		11.	IVI.	٥.
-	500	15	0	39	8	0	0	I	5	9
	520	13	0	44	23	0	4	I	4	39
l	540	II	0	49	32	0	16	I	4	15
I	560 580	9	0	54	31	0	35	I	4	3
I	600	6	0	59	15	I	3	I	4	0
ı			-	3	39		37		4	7
١	620	4	I	7	38	2	15	I	4	23
۱	640	3	I	II	7	2	59	I	4	49
1	660	2	I	14	6	3	48	I	5	19
I	680	I	I	16	30	4	38	I	5	54
I	700	0	I	18	16	5	30	I	6	28
١	720	0	I	19	27	6	22	I	7	2
ł	740	0	I	20	. 0	5	16	r	7	33
I	760	0	I	.19	55	7 8	7	I-		57
I	780	0	I	19	16		58	I	78	15
I	800	I	I	17	58	9	45	1	8	26
1	0	-	-	- 6				-	0	
	820	2	I	16	9	10	31	I	8	30 26
	840 860	3	I	13		II	13	I	8	16
i	880	5	I	7		12	23	I	8	0
i	900	7	I	4		12	52	I	7	37
ı	900	-	_	т,	- 7					
	920	8	I	0	20	13	16	I	7	8
	940	10	0	56		13	36	I	6	40
	960	12	0	51		13	49	I	6	8
	980	13	0	47	15	13	57	I	5	37
	1000	15	0	42	38	14	0	I	5	9

TAB. III.

0	January. 1	hes. 12	Mirco.	Aprille 1	, May.	june.
Days.	M. S.	1		M. S. B	M. S. B	M. S. B
2 4	4 5. 35		12 2 3	; S, 4° 4	3 A. 24 4 4 3 38 4	2 A. 40 5 2 24 5
468	6 31 7 2: 8 14	4	12 8 3 11 22 3 10 51 3	2 2 4 1 4 4 1 13 3	3 5 4 3 58 3 4 6 3	2 4 4 I 42 4 I 19 4
14	9 30	14 49 14 48 14 43		o 10 3	4 9 3 4 12 2	5 3 3 5 30 3 6 0 2
3	10 43	14 33	\$ 53 2 8 15 1 7 41 1	0 50 2	4 5 1	o S. 26 2 o 53 I
2:	1 12 3	13 50	7 2:1 6 25 1 5 47 0	1 43 : 2 7 1 2 3 1	3 40 I 3 40 I	1 19 I 1 4 I
3	8 3 28	13 9	5. 100	2 51 6	3. 25	2 300

Days.	July. August.			11	Sept.			October. 1			Nov.		Decem.					
ys.	M.	S.	В	M	I. S	. []	3 N	f. ;	S.	B	M.	1	5. 7	B	M.	S	M	. S.
-	1 S.	20		-	S. 3		1	A	40		10	A,	38	2	16	A.2	-	A.53
2	,	42	4.4	5		4 3	P	220)		3	10	24	-	2 .	16	0	12	221
6	3	3	4	5		4 3	1 R		58	3	II	1	14,	2	15		9	5
8	4	21	4	15			2		37	3.	12		22	2	15	47	7	23
30		38	3	4		5 2	13		18	2	12		50	2	15	35	6	29
-				-			1-				-	-			-			
12	1	54	3	4	3	0 2	4		00	2	13		23	1	15	22	15	32
14	15	7	3	4		6 2	4		40	2	13		48	I	15	8	4	30
16		18	2	13		3 2	5		20	2	14		13	I	14		3	30
18	,	27	2	13		9, 1			0		14		35	I	4		2	30
20	5	3 5	1	2	5	2 1	16		41	1	14		56	1	13	45	Į.	35
22	5	41	I	2		5 1			22	1	15		14	0	13	1.4		40
24	8.	41	1	ī		5 3 6	170		2	I	15		29		12		0	S. 20
2,4		46		1		23			4.2	0	15		40		12		I	S. 20
2		45		10			lig		·2 I	0	15		50	0	II		4.3	20
13				3			5.			1 .	15		-	1	Io			18
. 5	12:15 4310 > 14:0 10 0 0 15 5510 10 381 3 18																	

PROB. XV.

To determine very nearly the Longitude of any Place upon the Earth.

Several ways have been attempted to perform this, but none of them so proper, so easy and certain, as that by the eclipses of Jupiter's satellites. And those of the first or nearest satellite happening so frequently, afford the best means for this end, by observing the precise time when any of them happens. But then it is necessary that the observer know before hand, within a little, when these opportunities offer; less the either let them slip, or grow weary by too long attendance. The method is thus,

1. He must know within a small matter the Difference of longitude of London, and the place proposed, either by the common maps, or by the dead reckoning at sea. Turn this difference of longitude into time, allowing 15 degrees to an hour.

2. By the last prop. compute the time of the eclipse for London, and to this time add the time answering to the diff. longitude, if the place is east from London; or subtract it, if west: and you have the time when to look for the eclipse at that place. Therefore begin to observe a quarter or half an hour before, with a telescope: And note the precise time in that place, when you see the beginning or end of the eclipse. Then the difference of this time, and the time for London, turn'd into degrees, will give the difference of longitude from London; which will be east if the time observed be after the time at London; but west if before.

Note, In observing you must look on the right or west side of Jupiter for the Immersion; and on the lest or east, for his Emersion. And you need never look further from his body for either of them, than half, or at most, $\frac{2}{3}$ his diameter.

Example.

If on August the 20th N. S. 1752, I be in one of the Ladrone flands; whose diff. lon. by estimation is about 140° E. from London: And I observe the beginning of the cclipse at 39 m. past 3 o'clock next morning; and I find by computation that the same cclipse happen'd Aug. 20, at 7: 44" past 6 at night; that is 9 h. 31 \frac{1}{4} m. later in the island than at London; therefore its diff. longitude from London east will be 142" 49.

SCHOLIUM.

This method is fo easy that one would wonder it is not more practifed by feamen, when they go to remote countries; there being nothing more required than a common telescope of three feet long, or a reflecting telescope of one foot; and a clock or watch fet to the true hour of the night in that place, by which to know the moment of the cclipfe. And these eclipses happen very often; there being about four of them every week. It is true, many of them happen in the day, or when Jupiter is below the horizon; and fometimes clouds may interpose and prevent the observation. But there are frequent opportunities when none of these things happen; and when they do, one may fave the la-bour of waiting upon them. I don't know whether this could conveniently be practifed at fea; but on shore nothing is more easy. And one would expect that failors above others, should be more

than ordinary folicitous for making proper observa-FIG. tions, in distant countries, in order to settle the longitude of places; without which, this their

art must for ever remain impersect.

To rectify your clock or watch in any place, observe when the star Allioth, or Cassiopeia's hip is in a plumb line with the pole star, (which is easily known by hanging up a line and plummet); and at that time the said star is upon the meridian below the pole, and therefore the time of night will be known by prob. 12, beforegoing.

PROB. XVI:

To find the Variation of the Compass.

RULE. I.

By the Sun's true Amplitude.

Take the sun's amplitude, by the compass, which is call'd the magnetical amplitude, just when his lower limb touches the horizon, or rather is half

a diameter above it.

Describe the circle SWNE for the horizon; N the north, E the east point. Set the sun's true amplitude at rising, (found by prop. IV.) from E towards N, as to \odot , if it be north; if south, towards S. Then set the magnetic amplitude from \odot towards S, as to A, if it be north; but towards N, if south. Then make AB equal to EN, 90 d. then AE or NB is the variation; which will be east, if B be between N and E; and west, when between N and W.

And a like method may be used when the am-

plitude is taken at fun set.

And.

フ

8

fig. And a figure may be drawn by hand, which will shew how to add or subtract the true and magnetic amplitude, to find the variation.

RULE. 2.

By two equal Altitudes of the Sun.

Take two azimuths of the fun (by the azimuth compass) when he is at the same altitude twice in one day. Set them upon the horizon NBSN, in their proper places, suppose at A and B. Then bissect AB in S, and SCN will be the true meridian. Then let the azimuth of the first observation be reckon'd from the south, and set it from S the south point to D, towards A, if it lye eastward; or towards B, if westward. Then AD is the variation, which is west when D salls between A and S; and east when between A and N.

And the fame thing may be done by drawing the meridian NS by the pole star, just when it is in a plumb line with the star Alioth, or with Cassio-

peia's hip.

SCHOL.

The variation of the compass is continually altering. At London in the year 1580 it was 111 deg. east. In 1657 it was north. In 1723 it was 12 deg. west. And now it is at least 15 deg. west; and proceeds westward by a flow motion of one degree in about seven years. However it does not move westward in all places, but in some places eastward, and in others is nearly at a stand. Likewise the increase or decrease of the variation is greater or less in different places.

A short TABLE of the variation of the compass, as has been observed in different places, which may be some guide to the mariner, when other helps fail bim.

A TABLE of the Variation of the COMPASS.

	D.
Ascension I.	ı W.
Azore If.	8 W.
Baffins Bay.	57 W.
Baltic	10 W.
Barbary, N. W. Coast.	7 W.
N. E. Coaft.	TTT
Bombay.	5 W.
Brasil Coast, Lat. 10 S.	6 E.
Lat. 20 S.	
British Channel.	12 E.
Canary Isles.	15 W.
Cape Comerin	7 W.
Frio.	5 W.
	12 E.
	16 W.
Chili W. Coast.	8 E.
England, West at Sea.	12 W.
France, W. Coaft. West at sea 10 deg.	II W.
West at sea 10 deg.	8 W.
German Ocean.	14 W.
Guinea S. Coast.	5 W.
Gulf of Bothnia.	6 W.
Hudson's Bay.	30 W.
Straits.	40 W.
Tava Coast	2 W.
Indian Sea.	14 W.
London	16 W.
Madagascar W. Coast.	19 W.
South from, in Lat. 40.	
Majorca Isl.	
7.11. 170	
Malacco	10 W.
New England Cook	2 E.
New England Coast.	10 W.
D	New-

	D.
Newfoundland C.	21 W.
New Guinea C.	6 E.
New Holland S. and W. Coast.	4 W.
New Zeland	9 E.
Portugal Coast. 9	9 W.
West 8 deg	6 W.
River Grand, before.	14 E.
Plate, before	19 E.
Saint Helena	2 W.
Sardinia.	13 W.
Sicily	12 W.
Straits of Gibraltar.	6 W.
Magellan E. Entrance.	15 E.
W. Entrance.	13 E.
Terra Magellanica, E. Coast.	19 E.
Tristian de Cunha J.	0
Van Dements Land.	ı E.
Virginia: - ' -	5 W.

But the mariner is not to depend much upon this table, the variation in most places being very uncertain, and in many places quite unknown. And besides, the variation is continually altering. Therefore he must omit no opportunities to take the variation at sea by observation, as in this Problem is directed.

PROB. XVII.

To find the Lee-way of a Ship by Observation.

RULE.

1. If you are within fight of land, take the angle between the ship's keel, and that point of land which

which always bears on the fame point of the com-

pass; and this is her quantity of lee-way.

2. Or fet the ship's wake with the compass: the angle between this and the keel is her lee-way. And here the ship's course is to be reckon'd so much further from the wind, as is her quantity of lee-way.

SCHOL.

All ships do not make the same quantity of leeway, but some a great deal more than others; and that difference proceeds from the different forms of their hulls, which may be infinitely varied. A person used to a particular ship will know better what lee-way she makes, than a stranger; and in this, experience is the best director. The general practice to allow for lee-way, is as follows.

1. The ship upon a wind, and all sails set, allow one point.

2. Topsail reefs in, 11 point.

3. Hard gale, and one topfail taken in; 2 points.

4. Hard wind, high fea, both topfails in; 3 points.

5. Only main-fail and mizen out; 4 points.

6. Only main-fail out; 5 points.

- 7. Only mizen out; 6 points. 8. All fails furl'd; 7 or 8 points.

D 2

In all these cases, a higher sea, and harder wind, increases the lee-way. Likewise respect must be had to the fetting of the Water, when it runs high, which will increase or decrease the lee-way, according as it opposes or conspires with the motion of the ship: and must often be allow'd for according to Judgment.

Ships

Ships that draw most water make least lee-way; and a ship out of her trim, makes most lee-way. However, the way most to be depended on, is to set the wake of the ship with the compass, as directed in this problem.

PROB. XVIII.

To find the setting of a Current and its Velocity.

When there is a smooth sea and little wind, heave out the boat with three or sour hands in her, together with a compass, log-line, and half-minute glass; and also a triangular board, the bigger the better: To one side of this board fasten as much lead as will sink it; and to the three angles, tye three equal pieces of line; and knot the other three ends together, and to this tye another line 100 sathoms long, or more. Some use a kettle ty'd by the bow, instead of this board.

When you are off from the ship, cast over your board, letting it sink 60, 80, 100, or 120 sathom, if your line will allow. Then sattening the line to the stern of the boat, it will bring her up, and make her ride as if she were at an anchor. Then cast over your log, turn up the glass, and as you veer out the log-line, set the drift of the log with the compass; and this shews you how the current sets; and the length of the log-line run out will give the quantity of its motion. But you must add to the drift, or \(\frac{1}{4} \) part, according to the length of the line she rides at; for both the board and the board will drive; but the bigger the board is, the less she will drive.

If this board be heav'd out of the ship, into the wake, and suffer'd to fink far enough, it will

fhew the direction of the current, and the line run off compared with the ship's way will help to

determine its velocity.

The direction of a current or great fea raifed by the wind may be nearly conjectured from the position of the waves, that is of the ridges and furrows of the sea. For the direction of the current's motion is always perpendicular, or across these waves.

A current's motion may be discover'd by keeping an exact account of the ship's way, both outward and homeward, according to the dead reckoning. For the difference of the reckoning outward and homeward, will shew the motion of the current, if it be continual.

SCHOL.

tinual current; as in the straits of Gibraltar, where the Atlantic sea runs continually into the Mediterranean, and in this place there is an under current setting the contrary way. In the Baltic sound there is a current, and sour or sive sathom deep an under current. There is a current from the Euxine sea, through the straits of Constantinople, and Propontis, and in many other places. And in all such places, it is probable there are under currents setting the contrary way.

If a ship be at rest, or have no motion in the sea, and at the same time the sea has a current towards any point: It is the same thing, as if there was no current, and that the ship sail'd toward the same point, and with the same motion, the current

was supposed to have.

Hence, if a ship sails upon any course in a cur-

rent; inflead of confidering the current's motion, one may confider the fhip as having a new course, the same as the current's motion is.

PROB. XIX.

To describe the Times, Periods, and Directions of the Trade-Winds, and Monsoons.

It is certain from experience, that in the temperate zones, the winds are fo variable and uncertain, that they blow from all points of the compass at all times of the year, without any distinction; but between the tropics and fomething beyond, they keep a certain regular course, either constantly the same, or variable by certain rules, according to the time of the year. And these winds, that blow constantly thus from some certain point of the compassion periodical times of the year, they are called monsons. Concerning which, the following observations have been made.

1. Between the tropics, and as far as 30 deg. N. and S. lattitude, there is conftantly an easterly wind, all the year, which would doubtless be the same quite round the globe, if it was not for the interposition of high mountains and continents, that interrupt its motion in particular places, as in the Indian and Chinese seas, as will be explained afterwards. The limits of these trade winds, are confin'd to a very little compass, for in passing these limits, the wind is found to change almost instantaneously. Likewise it is said, that a little without these limits, from 30 to 35 deg. lat. there are generally westerly winds.

2. In places near the tropic of Cancer the wind is N. easterly; but near the tropic of Capricorn, S. Easterly: Likewise, when the sun is near the tropic of Cancer, or all fummer, these winds are a point or two more foutherly; and in the winter more northerly. The motion of the fea likewife follows the course of these winds. All this is to be understood in open seas, where there is no interruption from the land. In the Pacific Ocean or great South Sea, the winds are very fresh, and so regular and constant, that in sailing, one scarce ever need attend the fails. Only near the land, as on the coast of Peru, and on the west of Africa in S. lat. and 100 leagues from Guinea, the wind is always foutherly. Storms and tempests are seldom known in the fouth fea. What has been faid holds in general in open feas; for at or near the shoar there is a great variety in the forces and directions of these winds, arising from the situation of mountains, vallies, woods, and the various disposition of the foil, as it is more or less capable of reflecting heat.

3. In the Atlantic and Ethiopic feas, the trade winds on the coast of Asrica reach to about 28 deg. N. and S. lat. and at the American shore near 31° lat. and in this sea the S. easterly winds reach as far as 4 deg. N. lat. and near the coast of Brasil in America, they are more easterly than in the same lat. near the African coast, where they are more southerly.

On the S. coast of Guinea from Sierra Leone to St. Thomas's Isle, the southerly and south-westerly winds are perpetual. Also on this coast there are frequent calms, and tornadoes. In lat. 10. on that coast the wind is west, and in lat. 20 or 30, N. west.

Between 4 and 10 deg. N. lat. and 100 or 150 leagues from the Guinea coast, there is a tract of sea, wherein there are perpetual calms, attended with thunder, lightning, and frequent rains; whence this place is by pavigators call'd the Rains.

Near the Caribbee islands there are often hurricanes in the month of Lugust: Near these islands the wind bears more easterly, sometimes E. sometimes E. by S. yet commonly a point or two to the northward. And the strength of these winds gradually decreases, in sailing to the westward.

On the coast of Brasil, from April, the S. W. wind blows, and from September the N. E. And S. of Brasil it inclines more westerly. But on the W.

coast of America the winds are westerly.

For the fake of these winds, all those that use the West-India trade, even those going to Virginia, count it their best course to get as soon as they can to the southwards, that so they may be certain of a fair wind.

4. In the Indian ocean, the winds are partly general, as in the Ethiopic and Atlantic; and partly periodical, between the latitudes of 10 and 30 deg. S. the S. E. by E. wind blows all the year.

From 2 to 10 deg. S. lat. the S. E. wind blows from June to November; and the N. W. wind from December till May; this extent is a degree less near Madagascar, and a degree more near Java. And this Monsoon reaches as far as the Molucco islands.

From 3 deg. S. lat. northwards, the N. E. wind blows from October till April, a clear breeze; and the S. W. or S. S. W. wind from April to October; this last is stronger, but accompanied with rainy weather. These winds are not so constant in the gulf of Bengal, as in the Indian sea.

Between

Between Madagascar and the African shore, as it as the equinoctial, the S. S. W. wind blows om April to October, which is more westerly near ne line. The rest of the year, it is easterly.

To the east of Sumatra, and in the coast of Lambaia and China, as far as the Philippine islands nd Japan; the N. wind blows from November till May; and the S. wind from May to October or Iovember; but these Winds will vary a point or wo sometimes. And between New Guinea and umatra S. of the equinoctial you have the same vinds; but the N. wind is N. westerly, and the is S. easterly, but vary sometimes 5 or 6 points. Besides, the time of the changing of these winds is month or six weeks later.

Between the S. end of Madagafcar and the shore, he S. E. wind blows from October till May; And rom May a west wind. Beyond St. Laurence in-

o the sea a S. wind.

These contrary winds do not shift all at once, but are in some places attended with calms, in others with variable winds. The end of the westerly monsoon on the coast of Coromandel, and he two last months of the southerly monsoon in he Chinese sea, are very subject to be tempestures, which renders the navigation of these seas unafe at that time. These tempests are by our seanen called the breaking up of the monsoons.

nen called the breaking up of the monstons.

By reason of the shifting of these winds, all hose that sail in those seas, are obliged to observe the seasons proper for their voyages; and so doing they fail not of a fair wind and speedy passage. But if they chance to out stay their times till the contrary monston sets in, as it sometimes happens; they are forced to give over the hopes of accomplishing their intended voyages, and either return-

D 5

to

to the port from whence they came, or else put into some other harbour, there to spend the time till the winds shall come favourable.

PROB. XX.

To determine the Position of the Sails of a ship, in respect to the Wind; the Position of the Rudder; and Way of working a Ship.

The fails of a ship have more or less force to move the ship, according to the different position they have in respect of the ship's keel, as well as in respect to the wind; concerning which, observe these general

RULES.

- to make her ware. Main fails tend only to move the center of gravity of the ship. Mizen fails keep a ship from sheering backwards and forwards; and serve to force a ship's stern to leeward. Sails have more force the taughter they are hoisted; and a sail that bags has less power. The higher a sail is placed the more wind it will receive to move the ship.
- 2. Any one fail gives the greatest motion to the ship, when it stands at right angles to the keel, and the ship goes directly before the wind. But in all the sails together, because one sail keeps the wind from another; if the wind come at an angle of about 60 degrees, they will have the most power to move the ship. Likewise the nearer a right angle any sail makes with the keel, or ship's way, the less lee-way she makes; and the further from a right angle, the more lee-way.

 Again, The nearer the way of the wind is with the

way of the ship, the less lee way; and the more distant or a-cross, the more lee-way she makes.

- 3. As to the most advantageous placing of the FIG. sails: If S be a ship, SD her way, SA the sail, 9. WS the direction of the wind, or the point it blows from. Then if the ship lie near the wind, the angle WSA must be almost twice the angle ASD, that is, the angle between the wind and the sail, should be nearly double the angle between the sail and the keel. If the wind come near at right angles to the way of the ship; the angle WSA must be once and a half the angle ASD. And if she go almost before the wind, the sail must almost bissect the angle, between the point of the wind and the keel. And such positions will give the greatest motion to the ship. And to cause her to gain the most to windward, the angle WSD must be 55, and WSA 35, ASD 20, or thereabouts; if any ship can lye so nigh the wind.
- 4. If the wind come almost across the way of the ship, then the sharper the head sails are set, the more power they have to turn the ship's head about. Again, if the way of the wind be nearly the same as the way of the ship; the sail ought to make an angle with the keel of 54 degrees. If the wind make an angle of 40 or 50 deg with the ship's way, the angle between the sail and the keel may be about 30 deg. And these positions will turn her sastest about.
 - 5. The most advantageous position of the rudder, so as to have the greatest force possible in turning the ship about, is, when it makes an angle with the keel of $54^{\frac{1}{2}}$ degrees. The faster a ship sails, the better she will answer her helm; if she sail very

D 6

o. flow, fhe will scarce steer at all. If she heel much

PROB. XXI.

· To find the Place of turning to Wind-ward.

Suppose WA be the direction of the Wind, and the angle WAD or WAF the nearest a ship can lie to the wind. And if a ship sail from A to B; to find the point C, where she must turn to windward.

Having made the angles WAD and WAF the nearest the ship can lie to the wind; through B draw BC parallel to FA intersecting AD in C; then C is the place required.

Trigonometrically.

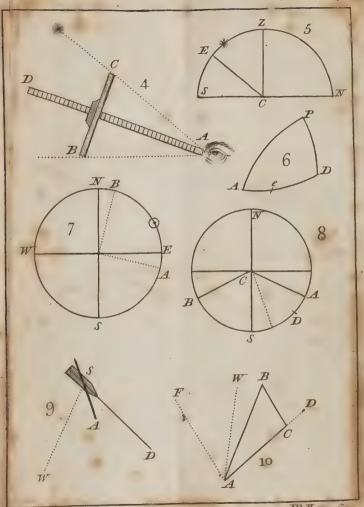
AB is given, and the angle WAB and WAF or WAC, then you have BAC, and FAB or its equal ABC; and from thence ACB. Therefore as S.ACB: AB:: S.ABC: AC.

P. R. O. B. XXII.

To find the Place of turning to Windward in a Current.

Suppose a ship sails from A to B in a current that fets in the direction AI, from A to I; and if WA be the point of the wind; to find the place C where to turn to windward.

Make the angle WAE and WAF the nearest the ship can lie towards the wind. And make AE to EH, and AF to FG, as the motion of the ship



Pl.II.pa.bo.



to the motion of the current, and draw FG, EH_{FIG} , parallel to AI; then through I, H, draw the lines AG, II. AHC. From B draw BC parallel to AG, and from C draw CD parallel to AF, and from B draw BD parallel to AI.

Then C is the point of turning to windward; and the ship is to steer the course and distance Ae, and by the motion of the current she will be brought to C. Then she must steer the course and distance CD, and she will then by the motion of the cur-

rent arrive at B, as required.

Here note, If the direction of the current be from I to A, the points G, H must be taken on the other side of the lines AF, AE: but the rest of the work is the same.

SCHOL.

It is scarce worth while to solve this trigonometrically. But they that have a mind, may find enough given in the triangles AHE, AFG, CDB. Many more questions might be proposed, of little use in the art of navigation; which if any one would know how to resolve, he must make himself well acquainted with plain trigonometry.

PROB XXIII.

To find the Distance of a Cape or Head Land at Sea.

RULE.

Suppose you are failing on some known course at A towards B, and you see the cape C. Take the bearing of the cape C by the compass, from A.

FIG. Then after you have failed a known diffance AB. the fame course, take the bearing of the cape again 12. at B. Then there is given the distance BA, the angles A and B, subtract the sum of A and B from 180, the remainder is the angle C at the cape.

> Then say, As sine of angle C. Distance A B. Sine angle B. Distance A C at the first observation.

PROB. XXIV.

To direct a Ship through the Sands, to a Harbour, or the Mouth of a River.

RULE.

13. To do this there must be sea marks, or light houses set up on purpose; so that every two of them may fland in a right line passing through the road between two fands; and a ship is to fail along fome of these right lines, till she come into some others of the right lines, and then change her

course, according to the position of these sands. Thus, T, H, R, G, P, W are sea marks. And suppose a ship at sea is to fail into the river F; the must come either into the line PW as to E, or into the line TH as to D. Then the must fail in a right line with TH, or elfe with PW till she come into a right line with RG. Then she must fail along the right line RG, till the is within the river. And thus she avoids the fands A, B, C.

There are often buoys placed in the road between one fand and another, which answers the fame end in the day time, where the passage is not FIG. very difficult; or where there are not convenient 13. places for light houses.

PROB. XXV.

To compute the Power or Force of a Tackle.

RULE.

Put I for the force at the hand, also mark every 14. part of the same running rope with 1. And when one rope acts against several, mark it with the sum of all these it acts against. And every part of the fame running rope must likewise be mark'd the fame. Proceed thus till you come to the weight.

Call the force at Ab, 1; also mark AC, 1; and CD, 1. then mark AB, 2; because it acts against Ab, AC. likewise mark BC, 2. And BE (acting against AB, BC) must be mark'd 4. Laftly, CW (acting against AC, BC, DC) will be 4. Therefore the force of the hand is to the weight, as I to 4.

PROB. XXVI.

To gauge a Ship's Hold.

There being fuch great diverfity in the shapes and forms of ships, that it is not to be expected there can be any one rule which can answer exactly for all ships. The practical rules laid down by feveral authors are as follows.

RULE 1.

Multiply her breadth, half breadth, and length in: in feet, together; and divide by 94, gives the tuns.

RULE 2.

Multiply the length by the breadth, and the product by the depth, in feet; then divide by 100 for war ships, or 95 for merchants that allow nothing for guns, gives the tuns.

RULE 3.

Take her length from the stern-post to the upper part of the stem, subtract \(^2_3\) her breadth from that length; multiply the remainder by the whole breadth, and that product by half the breadth, in feet; and then divide by 100 or 94, gives the king's or merchant's tunage.

RULE 4.

The weight of a ship's burthen is half the weight of water she can hold.

PROB. XXVII.

The Diameter of an Iron Ball being given, to find its Weight; and the contrary.

RULE.

As 100 to the cube of the diameter in inches, fo is 14 to the weight in pounds.

Extrem Breath-17.8 11 1,3

Pl.M.pa. 64.



Example.

- If the diameter be 4 inches, its cube is 64,

Then 100:64::14:

256 64

100)896(8.96 or 9 lb. the weight.

If the weight be 63 lb.

14:63 ::100

14)6300(450 cube of the diameter.

70 Its Log. 2.65321
70 Third part 0.88440
— Its numb. 7.66. the diameter.

NAVIGATION.

PART II.

The Theory or fundamental Principles of NAVIGATION.

FIG.

PLAIN SAILING.

PROP. I.

As Radius:
Distance run::
Sine of the course:
Departure.

DEMONSTRATION.

17. Let ABFQ be the rumb line described by the ship; P the Pole. Divide the rumb or distance AF into an infinite number of equal parts, AB, BC, CD &c. through A, B, C &c. draw the meridians PA, PB, PC &c. and the parallels of latitude AL, Ek, Cp, Dg &c. These will form an infinite number of small triangles ABk, BCp, CDg &c. all equal and similar: for all the hypothenuses AB, BC, CD &c. are equal by construction. And the angles kAB, pbC, gCD &c. are equal by desc. are equal by desc. are equal by desc. are equal; And also the sides kB, pC, gD

gD &c. Now in any one of the triangles, as FIG. ABk; it will be, by plain trigonometry, As radius: 17. S.kAB :: AB : kB :: BC : pC :: CD : gD&c. And by composition, rad: S.kAB:: AB+ BC+CD &c. : kB+pC+gD &c. But AB+BC+CD &c. or AF is the distance run, and kB+pC+gD &c. is the departure, by def. 7. Therefore it is, as rad : S.kAB :: distance run : departure; or alternately rad : distance :: S.course (kAB): departure. Q. E. D.

Cor. I. As Radius : Distance run :: Cosine of the course: Diff. latitude.

For by trigonometry, rad : S.kBA :: AB: Ak :: BC : Bp :: CD : Co &c Bp + Cg &c. but $\overrightarrow{AB} + \overrightarrow{BC} + \overrightarrow{CD}$ &c. = distance run = \overrightarrow{AF} , and Ak + Bp + Cg &c. = AR the difference of latitude. Therefore, Rad: S.kBA or cof. course: : distance AF: diff. lat. AR. or alternately rad: distance AF:: cof. course: diff. lat. AR.

Cor. 2. As Radius : Diff. latitude :: Tan. course: Departure.

For by this prop. radius : distance : : S. course : departure :: (by cor. 1.) cos. course : diff. latitude. And alternately, cos. course : S. course : : diff. latitude: departure. But by the nature of fines and tangents, cofine: fine:: radius: tangent. Whence rad: tan. course: : diff. lat.: departure.

Cor. 3. Hence if the distance run, the difference

FIG. of latitude, and the departure, be laid out in right 17. lines, they will form a true right angled plain triangle. And confequently the fquare of the distance run is equal to the sum of the squares of the departure and diff. latitude.

SCHOL.

This prop. and its corollaries will refolve all the cases of plain failing, or those where no longitude is concern'd.

Hence may be discover'd a manifest difference between the departure and meridional distance. For in sailing from A to F, or from F to A, the departure is the same, being the sum of the lines kB, pC, gD &c. which is greater than the meridional distance AL, if she sails towards the equinoctial at A. For all the parts Bk, Cp, Dg &c. of the departure, are greater than the correspondent parts Rm, mn, no, &c. in the parallel RF; and lesser

than At, ts, sr, &c. in the parallel AL.

And the departure is of a middle quantity between them. The diff. of longitude is also different from both the departure and meridional diftance. For as the meridional distance at F is RF; and at A is AL; and the departure between A^t and B is the sum of the lines Bk, Cp, Dg, &c. to Fi; so the diff. of longitude is the arch of the equinoctial contain'd between PA and PL, and therefore is greater than any of the others. I here therefore, the meridional distance, departure, and difference of longitude, are effentially different from one another. The diff. longitude is fixt and immutable when the places A, F are

PART II. PARALLEL SAILING. 69

re fixt; and so is the departure for a single course, FIG. whether backward or forward. But the meridi-17. In all distance differs from itself in the places A, F. Indicate this is of no manner of use in navigation, all omputations whatever depending upon the other wo

But though the departure is of a certain quantiy, for any one given course, yet if there be seveal courses between any two places A, F, the whole eparture may be different. Thus, if one ship ails from A to L, and from L to F, she makes he departure AL. But if another ship sails from A to R, and thence to F, she makes the departure RF, less than the former. And one of these is greater, the other less than the departure in the lirect course AF.

PROP. II.

As Cof. latitude:
Radius::
Distance of two places in one parallel:
Diff. longitude.

DEMONSTRATION.

The cofine of latitude is the radius of the paallel of the two places; and the radii of all circles re as the circumferences, or any correspondent parts thereof; therefore the radius of the parallel, is to the distance in that parallel: : as radius of the phere, is to their distance in the equinoctial, or lift. longitude by def. 5. that is cos. latitude: adius:: distance of the places: diff. longitude. 2. E. D.

Cor. The length of a degree of longitude in any pacallel of latitude, is as the cosine of its latitude.

For

MID. LATITUDE SAILING.

FIG. For the diff. longitude being given; the cosine 17. of the lat. to the distance in the parallel, will always be in a given ratio.

70

Schol. This prop. will refolve all cases of parallel failing, that is of failing directly east or west.

PROP. III.

As Cosine of middle latitude:
Radius::
Departure:
Difference of longitude, nearly.

DEMONSTRATION.

Suppose A, F, be two places, then it was shewn in prop. I. that the departure is the sum of the lines kB, pC, gD, &c. which sum is greater than RF and less than AL; and if the distance AF be not great, it is nearly a mean between RF and AL. Let x be in the middle between A and A, then the parallel xw is nearly a mean between RF and AL, therefore xw may be taken for the departure, nearly. But by prop. II. it is as coslat. of x: radius:: xw: diff. longitude; that is cosl. middle latitude: radius:: departure: diff. longitude, nearly. 2. E. D.

Cor. 1. Cof. middle latitude:
Sine course:
Distance run:
Difference of longitude.

For by this Prop. cof. mid.lat: rad:: dep:dif.long. and by Prop. I. rad: diftance:: f. courfe: dep.

Therefore

PART II. MERCATORS SAILING. 71

Therefore ex equo, cof. mid. lat. : dift. :: FIG. S.course : dif. long.

Cor. 2. Cosine mid. latitude:

Tan. course:

Difference of latitude:

Difference of longitude.

For by this prop. cos. mid. lat: radius:: dep. dif. long, and by cor. 2. prop. I. rad: dif. lat.:: tan. course: dep. and ex equo, cos. mid. lat: dif. lat.:: tan. course: dif. long.

SCHOLIUM.

This prop. and its corollaries will resolve all cases of sailing where the longitude is concern'd. And if you take half the sum of the natural cosines of the two latitudes, and (finding its logarithm) use it instead of the cosine of middle latitude, these proportions will be something more exact.

PROP. IV.

As proper difference of latitude:
Meridional difference of latitude::
Departure:
Diff. longitude.

DEMONSTRATION.

Let A, F be two places, then, it has been proved in Prop. I. that the infinitely small triangles upon the globe, ABk, BCp, &c. are all similar and equal. And by the nature of Mercators chart, these triangles are each of them projected into others upon the chart, likewise similar to these, and to one another; the angle of the course

FIG. course remaining the same in both. Now in any small triangle as ABk, since its departure kB, by the construction of the chart, is so far enlarged as to be represented by its corresponding diff. longitude; therefore the distillatitude Ak will be increased in the same proportion, that is, as kB: diff. longitude of kB, or of A and B: so proper distillatitude Ak: to its representation in the chart, call'd its meridional diff. latitude, or meridional parts of Ak. Therefore from the similitude of all these triangles, it will be as

Meridional parts of Ak: dif. long. A, B:: Ak: kB:: Bp: pC:: Cg: gD &c.:: (by composition) Ak + Bp + Cg &c. or AR: kB + pC +

gD &c. or the departure.

And again, as AR: departure:: merid. p. Ak: dif. long. A, B:: mer. p. Bp: dif. long. B, C:: mer. p. Cg: diff. long. C, D &c.:: (by composition) sum of the meridional parts of Ak, Bk, Cg, &c. that is of AR: sum of all the dif. long. of AB, BC, CD, &c. or the dif. long. A, F. And alternately, as AR proper dif. lat.: Meridional parts of AR:: departure: dif. longitude of A and F. A. A. A. A. A.

Cor. As Radius:
Tan. course:
Meridional diff. latitude:
Diff. longitude.

For by cor. 2. pr. 1. rad.: Tan. course :: dif. lat. : departure :: (by this prop.) meridional dif. lat. : dif. longitude.

SCHOL.

This prop. and corollary will resolve all the cases of Mercators failing, or where the longitude is concern'd

concern'd, by help of a table of meridional parts, Fig. by which the meridional diff. latitude is had.

The foundation of this prop. depends on the construction of Mercators chart; which construction

is this:

All meridians in this chart are parallel to one another, and at the same distance as at the equator. In consequence of which, all parallels of latitude, and every part of them will be represented in this chart, bigger than they really are upon the globe; and that in proportion of the cofine of la. titude to radius. From the parallelism of the meridians it likewise follows, that every rumb line will be a right line in this chart, fince any rumb cuts all the meridians at equal angles. Now to have the angle of the rumb, the fame on the chart as it is on the globe; the contiguous parts of the meridian must alto be increased in the same proportion as the parallel was increased, that is, as cos. latitude to radius, or which is the fame, as radius to the fecant of latitude. And hence it follows that the degrees of the meridian in approaching the pole. continually increase, as the secant of latitude increases. The lengths of the meridian line in this chart, from the equinoctial to all the degrees of latitude, being express'd by numbers, and put into a table, are what they commonly call meridional parts. And the difference of these numbers answering to the difference of lat. of two places, is call'd the meridional difference of latitude. And as upon the globe; the rumb, the diff. latitude, and departure put in streight lines will form a right angle triangle; fo their representatives in the chart, that is, the rumb, the meridional diff. latitude, and diff. longitude, will also form a right angled triangle, fimilar to the former.

E

PROP. V.

From the table of fines and tangents, find the difference of the log. tangents of half the complements of the latitudes of two places; multiply it by 10000, and keep the product: Then,

As the tan. of the constant angle 51 38, or, }. As constant number, whose leg. is 10.1015093 }:

That product::: Tan. course: Diff. longitude.

DEMONSTRATION.

It is demonstrable (by the method of fluxions, and must here be taken for granted) that the length of the part of the meridian line in mercators chart, which represents the difference of latitude of two places upon the globe, is equal to the difference of the log. tangents of half the complements of the two latitudes, multiply'd into the number 2.30258 509, and that product into the radius of the sphere.

Now, fince the table of meridional parts are express'd in minutes; express the radius of the earth in minutes, and it contains 3437.7469, and this multiply'd by 2.30258509 gives 7915.705; which last number multiply'd into the difference of the said log. tangents, gives the meridional parts, or meridional diff. latitude. Put D for the difference of the log. tangents, then 7915.705 D is the meridional parts. Whence by cor. pr. 4. As the radius of the tables: mer. dif. lat. :: tan. course: dif. longitude. That is 10000000000: 7915.705 D: tan. course: dif. longitude. And dividing the two first terms by 7915.705, and multiplying by

10000,

13.

10000, you'll have, 12633100000: 10000 D:: FIG. tan. course: diff. longitude. And the log. of 12633100000 is 10.1015093, and is the log. tangent of the constant angle 51 38. Q. E. D.

SCHOL.

This prop. with the help of prop. 1. will refolve

all cases of failing whatever.

In the few foregoing propolitions I have demonstrated the truth of the chief methods of failing now in use; and deduced them from their genuine principles, and fixt them upon their proper foundations. By which the reader will be enabled to fee that this theory is not founded upon false principles; but upon fuch as are folid and true; And confequently that all calculations built hereon may be depended on as exact. What remains is to give the particular folution of all the cases of failing, with some other things of use in this art of navigation.

PROP. VI. PROB

To refolve all the Cases of sailing, geometrically by Scale and compass.

Make two right angled triangles ABC, ADE.

AB is the difference of latitude.

BC the departure.

AC the distance sail'd.

AD the meridional diff. latitude. (from the,table).

DE the difference of longitude.

BAC the course.

Any two of these being given, the rest may be found, if the triangles be constructed. All lines FIG. are to be taken from, and measured upon, the 18. same scale of equal parts. And the angle laid down by the help of a line of chords.

Or thus,

Here must be constructed two right angled triangles ABC, BCD.

AB is the diff. latitude.

BC the departure.

AC the distance sail'd.

BAC the course.

CD the diff. longitude.

BGD the middle latitude.

Any two of these given will find out the rest, by constructing the triangles.

PROP. VII. PROB.

To refolve all the Cases of failing by the Traverse Table.

1. Cases of Plain Sailing.

In this table you have the difference of latitude, and departure standing together, in the proper column of the course; over against which, on the side, is the distance run. Any two of which being given finds the rest.

If any of the given terms be greater than the table contains, it must be taken out at twice or oftener; or take out the tenth part only, and then

multiply by 10.

2. Cases of Mercator.

Seek the meridional difference of latitude in the

column Lat. under the proper course; and adjoining thereto, in the column Dep. is the diff. longitude; and any two, being given, finds the third.

3. Cases of middle Latitude.

Seek the complement of middle lat. in the column of Degrees or Points, then in the column Dep. you have the departure; over against which on the side, in the column Dift. you'll have the diff longitude. And any two being given finds the third.

PROP. VII. PROB.

To resolve all the Cases of sailing by Gunter's Scale.

This scale is very expeditious for resolving any proportion, when the first, and one of the middle terms, are of one denomination; and the other middle term and the last likewise of one. The numbers are to be taken off the line of numbers; the fines off the line of sines; and the tangents off the line of tangents, &c. The proportions wrought here, are drawn from the foregoing propositions.

General Rule.

- 1. Set one foot of the compasses in the first term of the proportion; and extend from the first term to one of the middle terms, on its proper line: This extent will reach from the other middle term to the 4th term required, on its proper line. Reckon backward from 90 for cosines.
- 2. Both extents must be made from lesser to greater terms, or else both from greater to lesser;

 E 3

And each extent must be upon one single line, of the proper denomination. Observe, Radius is of any denomination, it is the sine of 90, or 8 points; and the tangent of 45 or 4 points; all at the end of the scale.

- 3. If you are extending from any given angle on the tangents, and the extent reaches beyond the line: You must set it as far back as it reaches over. Or proceed thus; set one foot at 45 (or 4 points,) and note, where the other foot falls, and keep it fixt there, and extend the other to the given angle. This extent set from 45 (or 4 points,) will fall on the 4th term, or angle required. For co-tangent take the complement, for they stand together on the scale.
- A. If the meridional diff. latitude be a term in the proportion, it is found thus: Extend from one latte to the other, on the line Merid. And fet that extent on the line E. P. and note to what number it reaches, for that is the merid. diff. latitude. Likewise on the centrary, the meridional diff. latitude taken off the line E. P. and set on the line Merid. will reach from one lat. to the other.
- 5. When in the given proportion, one term is en the fines, and its corresponding one is on the tangents; that on the fines must be reduced to the tangents; thus, Find the degrees on the fines, from which go directly over to the tangents, and you have the place you must extend to or from, instead of the fine; and this tangent term is always below 45°.

PROP. IX. PROB.

FIG. 15.

To make a Mercator's Chart, and to resolve the Cases of sailing by it.

1. By Gunter's Scale.

Draw the right line FI for the equinoclial, and FG perpendicular to it, for a meridian. Then with your compasses take 10, 20, 30 &c. from the line E. P. and fet from F to 10, 20, 30, &c. in the line FI; to be continu'd as far as you will; through which points, draw lines parallel to FG for meridians, as 10, 10: 20, 20: 30, 30, &c. then with your compasses take 10, 20, 30, 40, &c. from the line Merid. and fet these extents from F to 10, 20, 30, 40, &c. as far as you please, in the meridian FG. Through all which points draw lines parallel to the equinoctial FI, for parallels of latitude, as 10, 10; 20, 20; &c. likewise from the line Merid. set off the intermediate degrees, upon FG. Then graduate the equinoclial FI and the meridian FG, and number them as in the fig. and in one or more places put the mariners compass, with the rumbs. So your chart is finish'd.

2. By a Table of meridional Parts.

Let a chart be made from lat. 49 to lat. 58. 16. Draw FI for the parallel of 49, and FG perpendicular thereto for the meridian; and make F 1, 12, 23, 34, &c. each equal to 60, taken off any scale of equal parts; and through the points 1, 2, 3, 4, &c. draw lines parallel to FG for meridians. Then from the table take the meridional parts of 49, 50, E 4

rig. 51, 52, &c. and substract that of 49 from each of 16. the rest, and you'll have the remainders 93, 187, 283, 382, &c. take these off the same scale of equal parts, and set them from F upon the meridian FG to 50, 51, 52, &c. through which draw right lines parallel to FI, for the parallels of latitude; and number the degrees as in the figure. Also divide the degrees 12, 23, &c. as also 49, 50; 50, 51, &c. into minutes if there is occasion. Lastly, draw the mariners compass and rumbs, and you have sinish'd your chart.

A plain chart is easier made; for all the divisions of the meridian FG are only to be made equal to these in FI, and therefore it needs no further

explication.

The Use of the chart-in resolving the Cases of sailing.

1. The latitude and longitude of a place being given; its place will be found at the intersection of the meridian of the place, and its parallel of latitude, with a pair of compasses. And if any place upon the chart be given, its latitude is had on the side, and the longitude on the soot of it.

2. The course is easily laid down or measured by a line of chords; or by laying a ruler parallel to the proper rumb.

3. The difference of longitude is always meafured on the foot of the chart, but the departure and distance are both measured on the side: always observing to set one foot of the compasses as much above one latitude, as the other foot is below the other latitude: Or if both places lie in one parallel;

one

one foot must be as far above, as the other is be-FIG. low it. And thus any two being given, finds the third.

Example.

Let A, C be two places in the chart: Draw AC, and BC parallel to FI; then AB measured on the meridian (from 20 towards 40) gives the difference of latitude. And BC, measured on the foot of the chart, is the diff. longitude. BAC is the course; BC measured on the fide of the chart, gives the departure. And AC, measured on the fide, gives the distance.

Or thus, for the Distance.

Having the diff. latitude, take it from the foot of the chart, and fet one foot of the compasses in some point d, so that the other foot (turn'd about) may just touch some parallel, as at e; which parallel intersects AC (the line of distance) in f; then df measured on the foot of the chart is the distance.

Or thus,

Take the diff. lat. from the foot of the chart, and fet it from A to g, and draw gh parallel to FI, then Ah, apply'd to the foot of the chart, gives the distance; and gh apply'd the same way, gives the departure.

And by having the distance given, by a reverse

operation, the other latitude may be found.

The Solution of all the Cases of sailing in particular.

Having shewn the method of resolving all cases of failing in general, I come now, for the sake of the less experienc'd, to give all their solutions in particular: And that by feveral methods. So that in practice every body may take which he likesbett.

In working any of these proportions with the pen; you must take the logarithms of the several numbers, and fet them down in order; and then add the logarithms of the fecond and third terms together, and from the fum subtract the logarithm of the first term, so have you the logarithm of the fourth term; which being found in its proper table will shew what the fourth term is.

The middle latitude is had, by taking half the fum of the two latitudes. Likewise, if you subtract one lat. from double the middle latitude, you have the other latitude. In finding the middle latitude, take it rather too big than too little.

The meridional diff. latitude is found, by fubtracting the meridional parts of the leffer lat. from those of the greater, taken from the table of meridional parts: Or by adding them if the two places be on different fides of the equinoctial.

And if you have one latitude, and the meridional diff. of latitude, add or subtract (as the case requires) this merid, diff. lat. to or from the meridional parts of the known lat. And the table of meridional parts will flow the other latitude.

Being thus furnish d with all the necessary data, you may purfue your computation, in calculating the place of a ship, for a single course as follows.

Note, You must mark what is given with a dash (1), and what's fought with a cypher (0).

77:e

The feveral Cases of Plain Sailing, or where no FIG.

Longitude is concern'd.

PROP. X. Case I.

Course and Distance run being given, to find the diff. Latitude and Departure.

Example.

Suppose a ship to sail 300 miles N. E. by N. 3° 7′ 20. easterly.

I. Geometrically.

Draw CA for the meridian; make the angle ACB 3 points and 3° 7'. and make CB 300; on CA let fall the perpendicular BA; then CA meafured on the scale is 240, the difference of latitude; And AB 180 the departure.

II. By the Traverse Table.

Look for the course 37, or $3\frac{1}{4}$ points in the table, and over against the distance 30, you have 24.0 the diff. lat: and 18.0 the departure. Therefore for the distance 300, you'll have 240 the diff. latitude, and 180 the departure.

III. By Logarithms.

As Radius — 10.00000 Distance 300 — 2.47712 Cos. course (36 52) 9.90310 Diff. lat. 240 — 2.38022

And Radius — 10.00000

Distance (300) 2.47712

Sine course (36 52) 9 77811

Departure (180) 2.25523

So the diff, latitude is 240, and departure 180.

FIG.

IV. By Gunter's Scale.

Extend from radius or 90, to the course (36 52) reckon'd backwards on the line of sines (or S. rumbs); the same extent will reach from the distance (300),

to the diff. latitude 240, on the numbers.

And the extent from radius, on the fines (or S.rumbs), to the fine of the course 36: 52 (or 3 ½ points); will reach (apply'd the same way) from the distance 300, to the departure 180 on the line of numbers.

Note, This is the most common case in failing.

PROP. XI. Cafe 2.

Course and diff. Latitude given; to find the Distance and Departure.

Example.

Suppose a ship sails S. E. by S. making the diff. lat. 1d. 10m. or 70m.

I. Geometrically.

Draw CA for the meridian, on which fet the diff. lat. 70 from C to A. and make the angle ACB 3 points (or 33 45) for the course. And at A, raise AB perpendicular to AC. Then CB measured is 84, the distance; and AB, 46, the departure.

II. By the Traverse Table.

Look for the course 3 points (or 33 45) in the table; and in the column Lat. under the said course, find

find the diff. lat. 7, against which (in the column dist.) is 8.4 the distance; and in the column dep. 4.6, the departure. And the diff. lat. being 70, the distance will be 84, and the departure 46.

Here as the diff. lat. cannot be found exactly in the table; you must take a proportional part of the

difference, as is common.

III. By Logarithms.

As Cof. course (33 45)	9.91984
Diff. lat. (70) -	1.84509
Radius —	10.
Distance 84	1.92525
And Rad.	10.
Diff. lat. (70) -	1.84509
Tan. course (33 45) -	9.82489
Departure 46 -	1.66998

IV. By Gunter.

The extent from the course (33 45 or 3 points) reckon'd backwards, to radius, on the sines; will reach from the diff. lat. 70, to the distance 84 on the numbers. And the extent from the complement of the course (56 15) to the course (33 45) on the sines; will reach from the diff. lat. (70) to the departure 47, on the numbers. Or the extent from rad. to tan. course, on the tangents, will do the same.

PROP. XII. Cafe 3.

Course and Departure given; to find the Distance and diff. Latitude.

Example.

Let a ship sail N. W. b. W. and her departure 84 miles. I. Gea-

FIG.

I. Geometrically.

Draw BA (84) for the departure, and AC perpendicular to it; and make the angle ABC the complement of the course, 3 points or (33 45); then BC measured, is 101 the distance; and AC 56, the diff. latitude.

II. By the Traverse Table.

Seek for the proper course (56 15 or 5 points) in the table, find the departure (8.3) the nearest; against which in column Lat. is 5, 6 the diff. latitude; and in column Dist. is 10 the distance; therefore when the departure is 84, the diff. lat. is 56 and distance 100.

III. By Logarithms.

As S Course (56 15) 9.91984

Radius — 10.

Departure (84) 1.92427

Distance 101 — 2.00443

And Tan. course (56 15) 10.17510

Radius

Departure (84)

Diff. latitude, 56

1.74917

IV. By Gunter.

Extend from the S.course (56 15 or 5 points) to radius on the sines; this apply'd to the line of numbers.

bers, will reach from the departure (84) to the FIG. distance 101.

And the extent from the course (56 15 or 5 points) to the complement of the course (33 15 or 3 points) on the sines; will reach from the departure (84), to the diff. latitude 56, on the numbers.

PROB. XIII. Case 4.

Distance and difference of Latitude given, to find the Course and Departure.

Example. .

Let a ship sail N. easterly 100 miles, making the diff. latitude 74.

I. Geometrically.

Draw CA for the meridian, on which fet 74 23. the diff. lat. from C to A; at A raise the perpendicular AB; then with extent of 100 the distance run, and one foot in C, with the other cut the line AB in B. Then AB measured is 67, the departure; and the angle ACB, measured by the line of chords is 42 15, the course.

II. By the Traverse Table.

Find the distance 10 on the fide, over against which in some of the columns Lat. find 7.4, the diff. latitude; adjoining to which is 6.7 the departure in column Dep. And at top the course 3 \(\frac{1}{4}\) point, or 42 deg. And when the distance is 100, the departure is 67.

III. By Logarithms.

As Distance (100)	2.00000
Radius	10.
Diff. latitude (74) -	1.86923
Cos. course, 42 16 -	9.85923
And as 1	0.
Sum of dist. and diff. lat. (174)	2.24054
Their difference (26) —	1.41497
Square of the dep	3.65551
Half the log. —	1.82775
gives the departure -	67.

Otherwise the departure may be sound by case 1, having the course.

IV. By Gunter.

The extent from the diffance (100) to the diffalatitude (74) on the numbers; will reach from radius to 42 16, the course, reckon'd backward on the sines.

Take the sum and difference of the distance and diff. latitude. The extent, on the numbers, from 1 to the difference, will reach from the sum to a fourth, then half of the extent from 1 to this 4th, is 67 the departure. You may find it otherwise by case the 1st, by having the course.

PROB. XIV. Cafe 5.

Distance and Departure given; to find the Course and diff. Latitude,

Example.

A ship sails S. easterly 100 miles, and makes 74 miles departure.

I. Geometrically.

Draw AB equal to 74 for the departure, on 24. which raise the perpendicular AC for the meridian; with one foot in B make the distance BC 100; then AC measured by the scale is 67, the diff. latitude; And ACB measured by the line of chords is 47 45 the course.

II. By the Traverse Table.

Find the distance 10 on the side, over against which in some of the columns Dep. sind 7.4 the departure; adjoining to which, in column Lat. is 6.7 the diff. latitude; and at bottom the course 48. since the distance is 100 the diff. lat. will be 67.

III. By Logarithms.

As Distance (100) — 2.00000 Radias — 10. Departure (74) — 1.86923 S.Course, 47 44 — 9.86923

Find the sum and difference of the distance and departure.

Then log. Jum (174) 2.24054
Add the log. diff. (26) 1.41497
Half the log. — 3.65551
is diff. lat. 67. — 1.82775

FIG. Or the diff. latitude may be found by cafe 1, having the course.

IV. By Gunter.

The extent from the distance (100) to the departure (74) on the numbers, will reach from radius to 47 45 the course, on the fines. Then,

The except from radius to the course 47 45, reckon'd backwards on the fines; will reach from the distance (100) to the diff. latitude 67, on the numbers.

The diff. lat. may also be found in the same manner as the departure was, in the last case.

PROB. XV. Cafe 6.

Difference of Latitude and Departure given; to find the Course and Distance.

Example.

There are two ports C and B, whose diff. lat. is 72, and the southermost B lies 54 miles well from the meridian of the other place C.

I. Geometrically.

25. Draw the meridian CA, and set the diff. lat. (72) from C to A; at A erect the perpendicular AB, 54 for the departure. Draw BC, which measured is 90, the distance; and the angle BCA, measured by the line of chords, is 36 50, the course from C to B.

II. By the Traverse Table.

Look through the column's lat. and dep. till you find

find the diff. latitude and departure (7.2 and 5.4) flanding together. Then you have the course 3 points at top; and over against them on the fide, is the distance 9, or rather 90, because the diff. lat. is 72.

III. By Logarithms.

As Diff. latitude (72) - 1.85733 Radius Departure (54) — 1.73239 Tan. course, 36 52 - 9.87506

· And then the course being known,

As Cof. course (36 52) - 9.90310 Diff. latitude (72) - 1.85733 Radius Distance, 90 1.95423

IV. By Gunter.

The extent from diff. latitude (72) to the departure (54), on the numbers; will reach from radius, to 36 50 the course, on the tangens. Then,

The extent from the course (36 52) reckon'd backwards to radius, on the fines; will reach from the diff. latitude (72), to the distance 90, on the numbers.

FIG.

The Cases of failing, where the Longitude is concern'd.

PROP. XVI. Cafe 1.

The Latitude and I orgitude of two Place being given; to find the Course, &c.

Example.

Let one place be N. lat. 51. longitude 1: 0. The other place N. lat. 53 45, longitude 8: 30. Then the diff. lat. is 2 45 or 165 miles.

Diff. long. 7 30 or 450 miles.

Merid. diff. lat. 270 m.

Mid. lat. 52 22.

I. Geometrically.

26. Draw the meridian AB, and fet the meridional diff. latitude (270) from A to B; at B raise the perpendicular BC equal to the diff. longitude (450), and draw AC. then the angle BAC measured by a line of chords, is 50 deg. the course.

Or thus.

27. Make the angle BCD equal to the middle latitude (52 22), and CD the diff. longitude (450); from D draw DA perpendicular to BC, and make BA the difference of latitude (165); draw AC, then BAC measured on the chords, is (59 deg.) the course: and AC the distance.

II. By the Chart.

16 Find the places A, C in the chart, and draw AC, and the meridian AB. Then the angle BAC meafured on the chords, is (59 d.) the course. And AC apply'd PART H. MERCATORS SAILING. 93 apply'd to the fide of the chart is 5 d. 20 m. or FIG. 320, the distance.

Or thus.

Lay a rule over the two places A, C; and find what rumb is parallel to the ruler's edge, and that is $5\frac{1}{4}$ points, or N. E. by E. $\frac{1}{4}$ eafterly, for the course.

III. By the Traverse Table.

Look through the column's Lat. till you find the merid. diff. lat. 27, and adjoining to it the diff. longitude 45 in column Dep. the nearest is 27.2 and 45.4; then at bottom you have the course 5 ‡ points.

IV. By Mercator.

As Meridional diff. lat. (270) 2.43136

Radius 10.

Diff. longitude (450) 2.65321

Tan. course, 59 2 10.22185

V. By Middle Latitude.

As Diff. latitude (165) — 2.21748.

Diff. longitude (450) — 2.65321

Cof. mid. lat. (52 22) — 9.78576

Tan. courfe, (59 1) — 10.22149

By the Log. Tangents,

Find half the complements of the lat. of the two places,

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FIG. places, 18 7, and 19 30; and then the difference of their log. Tangents, .03437; multiply it by 10000, and referve the product 343.7; then,

As that product (343) — 2.53529

Conjunt log. (1an. 51 38) 10.10151

Diff. longitude (450) — 2.65321

12.75472

Tan. courfe, 58 54 — 10.21943

VII. By Gunter.

Extend from one lat. (51) to the other (53 45), on the line merid. and apply that extent to the line E. P. and note the degrees $(4\frac{1}{2})$ or 270 miles. Then the extent on the numbers, from $4\frac{1}{2}$ (or 270) to the diff. longitude $7\frac{1}{2}$ (or 450); will reach from radius to tan. course, 59 d.

Or thus,

Count the mid. lat. (52 22) backwards on the fines, against which on the tangents you have 31. 25. then the extent from diff. lat. (165), to diff. long. (450), on the numbers; will reach from tan. 31 25 to tan. course 59 deg.

SCHOL.

If the distance be required, the course must first be found by this case; and from that the distance by case 2, plain failing.

But the distance may be found by the chart, Thus: Take the dist. lat. (2 45) from the foot of

the

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the chart, and set one foot in some point d, so fig. that the other foot (turn'd about) may just touch some parallel, as at e; which parallel intersects As (the distance of the places) in f; then df measured on the foot of the chart, is 5 20 the distance.

PROB. XVII. Case. 2.

The Latitude and Longitude of two Places being given; to find the Departure.

Example. . .

One place in N. lat. 51, long. 1. The other place N. lat. 53 45, long. 8 30. Then the diff. lat. is 165 miles. The diff. long. 450 m. Merid. diff. lat. 270 m. Mid. lat. 52 22.

I. Geometrically.

Draw the meridian AB, and let the proper diff. 26 latitude (165) from A to d, and the meridional diff. latitude (270) from A to B; on AB raise the perpendiculars BC, de; make BC the diff. longitude (450), and draw AC, then de measured is the departure, 275.

Or thus.

Make the angle BCD the middle latitude (52 27), and CD the diff. longitude (450); draw DB perpendicular to BC; then BC measured is the departure.

II. By the Chart.

Let A, C be the two places: Take the diff. lon- 16 gitude

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96 FIG. gitude BC, and apply it to the graduated meridian; fo that one foot may reach as far above the latitude 16. of one place, as the other reaches below the other latitude; then the degrees intercepted (4 36) turn'd into miles, is the departure, 276.

III. By the Traverse Table.

Find the complement of middle latitude (37 38) in the column of Degrees or Points at top; and on the fide, in the column Dift. the diff. longitude (450, or rather 45); against which, in column Dep. you have (27.5) the departure. Therefore the departure is 275. Here as the degrees are not to be found exactly, you must take a proportional part.

IV. By Mercator.

As Merid. diff. latitude (270) 2.43136 Diff. longitude (450) 2.6,321 Proper diff. lat. (165) 2.21748 4.87069 Departure, 275 2.43933

V. By Middle Latitude.

As Radius 10. Cof. mid. latitude (52 22) 9.78576 Diff. longitude (450) - 2.65321 2.43897 Departure, 275

VI. By the Log. Tangents.

Find the course by case 1; and then the depar ure by case 2, of plain failing.

VII. By Gunter.

Extend from one lat. (51) to the other (53 45) on the line *Merid*. and apply that extent to the line *EP*. and note the degrees $(4\frac{1}{2})$, which turn into miles (270); then the extent on the numbers, from these miles (270) to the diff. latitude (165); will reach from the diff. longitude (450), to the departure, 275.

Or thus,

Extent from 90 on the fines, to the course (52 22) counted backwards; will reach from diff. longitude (450), to the departure (275), on the numbers.

PROP. XVIII. Case 3.

The Latitude of two Places, and the course being given; to find the Difference of Longitude.

Example.

Let one place be N. lat. 20. The other place N. lat. 37. The diff. lat. 17 d. or 1020 m. The course N. N. E. 2 19 easterly. Merid. diff. lat. 1168 m. Mid. latitude 28 30.

I. Geometrically.

Draw the meridian AB, and fet the merid. diff. 28. lat. (1168) from A to B. raife BC perpendicular to AB; and make the angle BAC (2449) the course. Then BC measured is (540 or 9 deg.) the diff. longitude.

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Or thus.

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FIG. Draw AB equal to the diff. latitude (1020), and BC perpendicular to it; then make the angle BAC 20 (24 49) the course. Make the angle BCD (28 30) the mid. latitude; Then CD measured is the difference of longitude, 540.

II. By the Chart.

Lay a ruler upon the first place A, parallel to 15 its proper rumb, and note where the edge of it cuts the parallel BC of the fecond place, as in C; then take the distance CB, (between C and the meridian of the first place A;) and apply it to the equinoctial or foot of the chart, and it gives od. or 540 m. the diff. longitude.

. III. By the Traverse Table.

Under the course (24 50), in column Lat. find the meridional diff. lat. (11.68), then adjoining thereto in column Dep. is the diff. longitude 5.4; then the diff. longitude is 540.

IV. By Mercator.

Radius -	10.
Tan. course (24 49) -	9 66503
Merid diff. lat. (1168)	3.06744
Diff. long. 540	2.73247

V. By Middle Latit	ude.
Cof. mid latitude (28 30)	9.94389
Tan. course (24 49)	9.66503 3.00860
Diff. lat. (1020)	12.67363
Diff. long. 537	2.72974

VI. By

VI. By the Log. Tangents.

Take half the complements of the latitude of the two places 35, and 26 30; find the difference of their log. tangents, .14749, multiply it by 10000, and keep the product 1475. Then,

As Constant log. — 10.10151

That product (1475) — 3.16879

Tan. course (24 49) — 9.66503

12.83382

Diff. longitude, 540. — 2.73231

VII. By Gunter.

Extend from one lat. (20) to the other (37), on the line Merid. fet that extent on the line E.P. and note the degrees cut, 19 30. Then the extent from rad. to tan. course (24 49); will reach on the numbers, from these degrees (19 30) to the diff. longitude 9 degrees.

Or thus.

Count the mid. lat. (28 30) backwards from 90 on the fines; even against which on the tangents is 41 18. Then the extent from tan. 41 18, to tan. course (24 49); will reach from diff. lat. (17 deg.), to diff. longitude (9 deg.) on the numbers.

SCHOL.

If both latitudes and the distance be given; to find the diff. longitude: The course must first be found by plain failing.

PROP. XIX. Case 4.

The Latitude of two Places, and the Departure given; to find the Difference of Longitude.

Example.

Suppose the latitudes to be 20 d. and 37 d. and the departure 472 miles; the course N. easterly.

Diff. lat. 17 d. or 1020 m. Merid. diff. lat. 1168 m. Mid. lat. 28 30.

I. Geometrically.

Draw the meridian AB, and make Ad the diff. lat. (1020), and AB the merid. diff. lat. (1168); raise the perpendiculars BC, de; make de (472), the departure; and draw AeC; then BC is the diff. longitude 540 or 9 degrees.

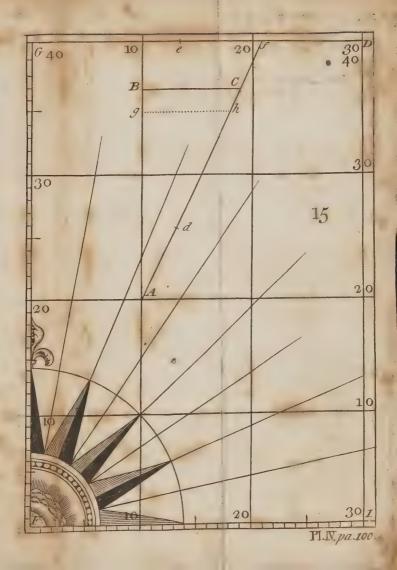
Or thus.

Draw the meridian AD, make AB (1020) the diff. latitude; and draw BC perpendicular to it, and equal to the departure (472); make the angle BCD (28 30) the middle latitude; then CD meafured is 540, the diff. longitude.

II. By the Chart.

Take the departure (472 or 7 d. 52 m.) off the fide of the chart; fetting one foot as much above one latitude A, as the other foot is below the other lat. B; apply it to the foot of the chart, and you have the diff. of longitude 9 deg.

III. By



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III. By the Traverse Table.

Find the complement of middle latitude (61 30) in the title of Degrees or Points. And in the column Dep. find the departure (47.2); over against which, in the column Dift. on the fide, is 54 the dift. longitude. Therefore the diff. longitude is 540 or q deg.

IV. By Mercator.

As Diff. latitude (1020)	3.00860
Departure (472) -	2.67394
Merid. diff. lat. (1168)	3.06744
	5.74138
Diff. longitude, 540 -	2.73278

V. By middle Latitude.

As Cosine mid. lat. (28 Radius	9.94389
Departure (472)	 2.67394
Diff. longitude 538	 2.73005

VI. By the Log. Tangents.

First find the course (24 49) by case 6th, of plain failing; and then the diff. longitude (540) by the last case of this.

VII. By Gunter.

Extend from one lat. (20) to the other (37) on the line Merid. fet that on E. P, and note the degrees 19 30, or 1170 miles. Extent on the F 4

(19 1); will reach from the departure (472), to the diff. longitude 540 miles or 9 deg.

Or thus,

Extent from the mid. lat. reckon'd backwards (28 30), to 90, on the fines; will reach from the departure (472), to the diff. longitude 540 on the numbers.

Note, This is a very usual case in mercator.

PROP. XX. Cafe 5.

One Latitude Course, and difference of Longitude being given; to find the other Latitude.

Example.

A ship fails S.W. by W. 2 47 westerly, from lat. 53 45, till her diff. of longitude be 7 d. 30 m. or 450 miles.

Mer. parts of the given lat. 3839.

I. Geometrically.

Draw AB (450) for the diff. longitude, and make the angle BAC (30 53) the complement of the course; draw CB perpendicular to AB; then CB measured is 270, the meridional diff. latitude. This taken from the meridional parts of 53 45 viz. 3839, leaves 3569 the meridional parts of the other lat. 51 deg.

II. By the Chart.

Let C be the given place; draw the meridian D, and the parallel CB equal to $(7\ 30)$ the diffigitude. Through B draw the meridian BA, d make the angle DGA $(59\ 2)$ the course, draw A intersecting BA in A; then A is the other ce.

III. By the Traversc Table.

In the column of *Points* or *Degrees*, find the course \$\frac{1}{4}\$ points) and in column *Dep*. the diff. longitude 54); then adjoining thereto in column *Lat*. is 72) the meridional diff. lat. this subtracted from e meridional parts of the known lat. leaves (3567) e meridional parts of the latitude sought 50 59.

IV. By Mercator.

As Tan. course (59 2) -	10.22179
75 11	10.
Diff. longitude (450) —	2.65321
Mer. diff. lat. 270 -	2.43142
Mer. parts of 53 45 -	3839
Subtract	270
Mer. parts	3569
Of the other lat. 51 deg.	

F 4

· V. By

V. By Middle Latitude.

Take the given lat. for the middle latitude. Then,

As Tan. course (59 2) 10.22179
Cos. mid. latitude (53 45) 9.77181
Diff. longitude (450) — 2 65321

Diff. latitude, 160 — 2.26323

By this find the mid. lat. 52 25; and repeating the operation with this mid. lat. you'll get 164 the diff. lat. and consequently the other lat. is 51 1.

VI. By the Log. Tangents.

Therefore 19 30 is half the complement of the other lat. consequently the other latitude is 51 deg.

VII. By Gunter.

The extent from the course (59 2) to radius on the tangents; will reach from the diff. longitude $(7\frac{1}{2})$ to a fourth, $(4\frac{1}{2})$ on the numbers.

Take these degrees (4 30) from the line E. P. and set it on the line Merid. from the lat. left, (53 45), and it will reach to 51 the lat. required.

I R R C M . M . J

SCHOL.

If both latitudes and distance be given; to find the diff. longitude; the course must first be found

r plain failing.

When only one latitude is given, and the differnce of longitude is required; the other latitude uft first be found by plain sailing, before the lontude can be found.

arallel failing; or failing East and West admits of three Cases, as fallows.

PROP. XXI. Cafe 1.

Given the latitude and difference of longitude of places in one parallel; to find their distance.

Example.

Suppose the latitude be 53 45, and-diff. longile 7 30, or 450 m.

I. Geometrically . .

With center A, and fine of 90, describe the DE: From a scale of equal parts take the longitude (470), and set it from D to E, and w AE. From the sines take the complement the latitude (36 15), and set from A to B and then BC measured on the scale of equal parts, es 270 the distance.

Or thus ...

Vake the angle BCD (53-45) the latitude, and (450) the diff. longitude; draw DB perpendar to BC; that BC measured is 270 the ance.

FIG.

II. By the Chart.

Let B, C, be the two places; take BC (455) and apply it to the fide of the chart, fo as one foot may be as much above the given latitude, as the other is below it; and this gives the diffance 4 30 or 270.

III. By the Traverse Table.

In the column of Degrees or Points, find the latitude (53 45), and the diff. longitude 45 on the fide, in column Dift. against which in column Lat. is the distance, 26 4; therefore the distance is 264.

IV. By the Sphere.

As Radius — 10.

Cof. latitude (53 45) 9.77181

Diff. longitude (450) 2.65321

Diftance, 266 — 2.42502

V. By Gunter.

The extent from radius to the lat. (53 45) reckon'd back from 90, on the fines; will reach from the diff. longitude (450) to the diffance, (268), on the numbers.

Or tlus.

Against the latitude $(53\ 45)$ on the line of *Chords*, you have on the line M. L. the miles contain'd in one degree of longitude (35); multiply this by the diff. longitude $(7\frac{1}{2})$, and you have the diffance 263.

Or extent from 1 to $7\frac{1}{2}$, will reach from 35 to 26%, on the numbers. PROP.

FIG.

PROP. XXII. Case 2.

The Latitude and Distance, of two Places in one Parallel, being given; to find their Difference of Longitude.

Example.

Let the latitude be 53 45, and distance 266 miles.

I. Geometrically.

With fine of 90 describe the arch DE, and 33 with fine of (36 15) the comp. latitude, the arch BC. Draw AD, and make BC (266) the distance. Draw ACE, then DE measured is (450) the diff. longitude.

Or thus.

Make the right angle DBC, make BC the diftance (266), and angle BCD (53 45) the latitude. then CD measured is (450) the diff. longitude.

II. By the Chart.

Take the distance in degrees (266 or 4 26) from the side of the chart, so as one foot of the compasses may be as many degrees above the given latitude (53 45), as the other is below it; apply it to the foot of the chart, and you have the diff. longitude 7 30.

III. By the Traverse Table.

In the column of *Degrees* or *Points*, find the latitude (53 45), and in column *Lat*. the distance (26.6), against which in column *Dist*. on the side, is 45, that is 450 the dist. longitude.

F 6 IV. By

IV. By the Sphere.

As Cof. Latitude (53 45) 9.77181.

Radius 10.

Distance (266) — 2.42488.

Diff. long. 450 — 2.65307

V. By Gunter.

The extent from the lat. (53 45) reckon'd backwards from 90, to radius on the fines; will reach from the diffance (266) to the diff. longitude (450), on the numbers.

Or thus.

Note what number in the line M. L. stands against the lat. (53 45) on the chords: Then the extent from that number (35) to 60 or 1 deg. on the numbers, will reach from the distance (266), to the diff. longitude 454, or 7 34.

P. R. O. P. XXIII. Case 3.

The Distance of two Places in one Parallel, and their Difference of Longitude given; to find the latitude.

Example.

Let the distance be 266 miles, and diff. longitude 7 30, or 450 miles.

I. Geometrically.

Draw AD_s and from A with fine of 90, describe the arch DE, set the diff. long. 450 from D to E, and

PARTIL PARALLEL SAILING.

and draw DE, AE. Set the distance (266) from FIG. D to F, and draw FC parallel to AD, then AC 33 measured on the fines is 36 15, the comp. lat. 53 45.

Or thus,

Make the right angle DBC, and BC (266) the distance, and CD (450) the diff. longitude. Then the 35 angle BCD, measured on the chords, is (53 45) the latitude.

II. By the Chart:

Take the diff. longitude (7 30) from the foot 16. of the chart, and fet that extent on the fide, in fuch latitudes, that the feet of the compasses may just intercept the distance (266 or 4 26); then in the middle between the feet of the compasses is the latitude 53 45.

III. By the Traverse Table.

Look through the columns Lat. till you find (26.6) the distance, standing against (45) the diff. longitude, on the side; Then the degrees belonging to that column Lat. is 54 the latitude.

IV. By the Sphere:

As Diff. longitude 450 - 2.65321 Distance (266) - - 2.42488 Radius Cof. latitude; 53 46 - 9.77167

V. By Gunter.

The extent from diff. longitude (450) to the distance (266) on the numbers; will reach from fine.

100

Fig. fine of 90 to the latitude 53 45, reckon'd back-wards.

Or thus,

The extent from 450 to 266 will reach from 60 to $35\frac{1}{2}$, the miles in 1 deg. of longitude; then againft $35\frac{1}{2}$ on the line M. L. is 53 45 on the chords for the lat-

PROP. XXIV.

To work a Traverse, or compound Course.

Example.

Suppose a ship fails from lat. 55. N. on the following courses.

Points or Courses.	Distances in Leag.
N. N. E.	26
N. E.	30
N.	22
E.	,24
S. E.	26

I. Geometrically.

This is done by laying down successively every course and distance one after another, till the whole be finish'd. Thus, let a be the point sail'd from, draw the meridian as, and make the angle sab equal to the first course N.N.E. and the distance ab (26). Then make the angle abc equal to that which

which the second course makes with the first, and FIG. make bc (30) the second distance. And thus make 36 every angle c, d, e equal to those which every two succeeding courses make with one another; and make cd, de, ef, their proper distances run: So is f the place of the ship at last.

Or thus,

Describe a circle about a as a center, with all the rumbs; Then draw all the courses parallel to tneir respective rumbs, and equal to the several distances sail'd.

Or thus,

Draw through all the points b, c, d, e, as you find them, fo many meridians parallel to the first as. And make the angles with these lines, at the points b, c, d, e; equal to their respective courses from the meridian: setting on each line ab, bc, cd, &c. the proper distance run: So is f the place of the ship. This is more exact than the former, but more troublesome.

Lastly, Let fall fs perpendicular to sa, then sa is the diff. latitude, and sf the departure. And the direct course saf, and distance af, may be found by case 6, of plain sailing.

II. By the Chart.

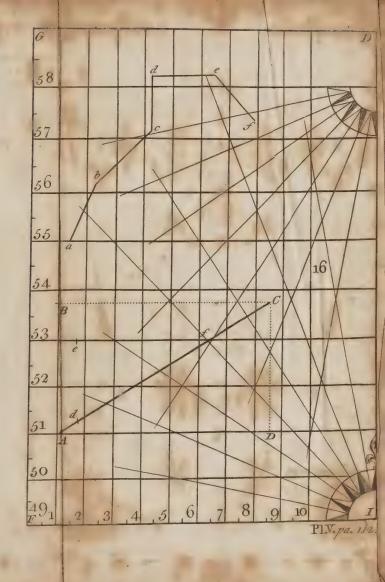
Lay a ruler upon a the first place of the ship, parallel to the N N.E rumb or first course; and draw a line, and set thereon 26 the first distance to b, which is to be taken off the side of the chart, in the same latitude the ship is in; then you have the place of the ship b, after the sirst course. Again, lay a ruler upon b the last place of the ship, and parallel to the next course N.E. and draw a line,

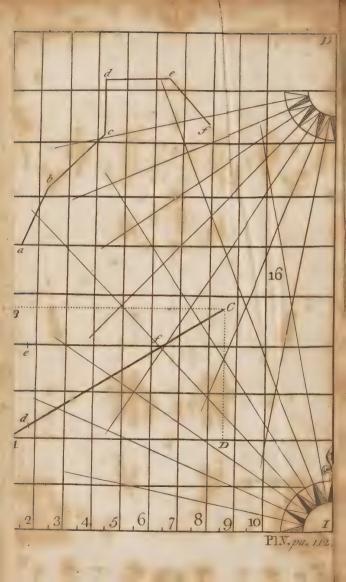
. .

rig. fetting thereon 30, from b to c, to be taken al16 ways from the fide of the chart in the fame latitude
the fails in: And thus you have the next place of
the ship, c. And thus laying a ruler successively
on each place of the ship, c, d, e, parallel to the
feveral rumbs, and drawing lines, and setting the
respective distances thereon, cd, de, ef, you will
have f the place of the ship at last: And this is
call'd, pricking the Chart.

IH. By the Traverse Table.

Find the difference of latitude and departure for every fingle course, as directed in case 1 plain sailing, either by calculation, or shorter by the traverse table. And observe whether each diff. latitude be north or south, and whether the departure be east or west. And then put all into a table, under their respective columns as sollows. Then sum up each column to find the difference between the northing and southing; and likewise between the easting and westing. And by this means get the difference of latitude and departure: And which way it lies, is known by the greater numbers.





So the difference of lat. is 48.8 north. And the departure 73.5 east. Which being had, the latitude of the ship is found to be 57.26: for 48.8 leagues is 146.4 miles, that is 2 deg. 26 m. And lastly, the difference of longitude is found by case 4 of Mercator.

PROP. XXV.

To work a Day's Reckoning.

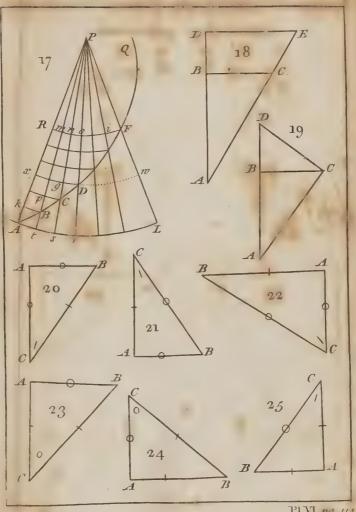
A day's reckoning is an exact account of the courses and distances that a ship sails in the space of 24 hours, that is from 12 o'clock at noon, till 12 o'clock at noon the next day. The man at the helm is to observe carefully what course he steers; or to keep close to the proper course appointed. And at the end of two hours, the log, is to be heav'd, and the knots and tenths run off in half a minute, must be exactly set down against the hour, in the log-board. And after this manner all the courses and distances for every two hours, are each to be written down on the log-board against their respective hours; as in the following sigure, which is the form of the log-board.

Here the courses must all be set down as given by the compass, and no allowance is to be made here for variation, lee-way, currents, &c. till

afterwards.

Hours.	Courfes.	7.I.	Winds.	Remarks. Variation 1	Courfes corrected.
4 6 8 10 12	S. N.W. by N. 1W.	8.0	W.N. W. W.b. N. W.N.W. S.W.		s. by E. N. W. ½ W.
2 4 6 8 10 11	S. W. S. E. S. W. E. S. E.	4.I	W. b. S. N.N.W. E.S.E. S.	I to Lee Way. A Current fetting WN W for 3hours at 2 miles an hour. I P. Lee-Way.	S. W. by E. S. W. by S.

Then after 24 hours, or the next day at noon, you must correct all the courses by proper allowances for variation and lee-way; which put into a new column. And in case of a current, consider it as a new course of the ship. With all these you must make a new table, in which you must put all these corrected courses with their distances; puting all these into one sum, that belong to the same courfe. This done, you'll have the following By this you must find the diff. latitude and departure, by Prop. XXIV. for working a traverse; as you fee. And here the traverse table is of particular service: This being its chief use. Then the diff. lat. and departure must be doubled, if the log. be only heaved every two hours, as is common.



Pl.VI. ра. 114.



-	Points. Dif	. N.	S.	E.	W.
S. S. W. S. by E.	2 14. 1 16.	144 *	13.5	3.2	5.6
$N.W.\frac{1}{2}W.$ $N.W.b.N.$	4 1/2 9.	9 6.6			7.3
S. W. b. S.	3 5.	11.	14.7		3.
S.E. by E.	5 4.	111 11	2.3	3·4 4·I	
Current	7 3.	11 /	-		3.0
W. by N.		11.7	16.7	10.7	28.7
			35.0	1	18.0
	doubled			i	36.0

Then the diff. latitude being found 70 foutherly, and the departure 26 westerly, the latitude of the ship is had, and the difference or longitude must be found by case 4th of Mercator. And then the place of the ship is known, all which must be put down in the journal; and then that day's reckoning is finish'd.

Note, If the diff. longitude be found for every particular course, it will be something more exact than finding it all at once, after 24 hours run; especially if the ship change her latitude much. But then this creates a great deal more trouble.

Note also, The several courses are easily corrected, by laying a thread over the figure of the compass (FIG. 1) to represent the true meridian.

PROP. XXVI.

To correct a Reckoning.

r. Always when opportunity offers take meridian altitude of the fun, or a star. And f thence by Prob. IX. Part. I. find the latitual And this observed latitude is always to be deper on for true. Then if the observed latitude as with your latitude by computation, then y reckoning admits of no correction.

2. If the computed and observ'd latitudes of gree: see whether you have rightly allow'd for riation or lee-way; but particularly for curre By these rectify the course and distance, as direction the last problem; and if this makes the latitudes.

agreey then your work is done.

If you have good reason to judge, that a curs is the cause of your error, as is often the canned you know the direction or course of it, not its quantity; you may correct the depart by saying, As Radius: to correction in latitude so tan. currents course: to correction in departure.

3. But if the two latitudes cannot thus be m to agree: confider your course, and if it be nesthe meridian than east and west; then it is probe the error is in the distance sail'd. Then take diff. latitude, and the departure, from the time the last observation, and say,

As diff. latitude:
To departure::
So error in latitude:
To correstion in departure.

Which is to be added or subtracted, as the case requires, according as the ship hath out-run the reckoning, or the reckoning hath out-run the ship.

4. But if your course be nearer the east or west than the north or fouth; then the error is most likely to be in the course. Then taking the diff. latitude and departure, from the time of the last observation, say,

As departure: To diff. latitude : : So error in latitude: To correction in departure.

But here if the course be very near east or west, you may fave the labour of this correction, it is fo fmall.

If you fail near 4 points from the meridian, and you be more fure of one than the other; then you must correct the other, whether course or distance. But otherwise you must divide the difference between them, and correct both.

5. For correcting the longitude, take the merid. difference between the computed and observ'd latitude: Then fay,

As error in latitude :

To correction in departure ::

So merid. diff. lat. : ...

To correction in longitude.

Which is to be added or subtracted as the case requires.

6. The error in the distance may arise from the log, or the inaccurate measuring the way of the ship by it. For generally speaking, the ship's way is greater than that given by the log; especially if a

great

PROP. XXVI.

To correct a Reckoning.

r. Always when opportunity offers take the meridian altitude of the fun, or a star. And from thence by Prob. IX. Part. I. find the latitude. And this observ'd latitude is always to be depended on for true. Then if the observ'd latitude agree with your latitude by computation, then your reckoning admits of no correction.

2. If the computed and observ'd latitudes disagree: fee whether you have rightly allow'd for variation or lee-way; but particularly for currents-By these rectify the course and distance, as directed in the last problem; and if this makes the laritudes

If you have good reason to judge, that a current is the cause of your error, as is often the case; and you know the direction or course of it, but not its quantity; you may correct the departure by faying, As Radius: to correction in latitude:: so tan. currents course: to correction in departure.

2. But if the two latitudes cannot thus be made to agree: consider your course, and if it be nearer the meridian than east and west; then it is probable the error is in the distance sail'd. Then take the diff. latitude, and the departure, from the time of the last observation, and say,

As diff. latitude: To departure : : So error in latitude : To correction in departure. sich is to be added or subtracted, as the case sires, according as the ship hath out-run the coning, or the reckoning hath out-run the ship.

. But if your course be nearer the east or west the north or south; then the error is most ly to be in the course. Then taking the diff. ude and departure, from the time of the last ervation, say,

As departure:

To diff. latitude : :

So error in latitude:

To correction in departure.

But here if the course be very near east or west, a may save the labour of this correction, it is so all.

If you fail near 4 points from the meridian, you be more fure of one than the other; n you must correct the other, whether course or ance. But otherwise you must divide the disence between them, and correct both.

5. For correcting the longitude, take the merid. erence between the computed and observed laide: Then say,

As error in latitude :

To correction in departure : :

So merid. diff. lat. : ...

To correction in longitude.

Which is to be added or subtracted as the case juires.

6. The error in the distance may arise from the 3 or the inaccurate measuring the way of the ship

it. For generally speaking, the ship's way is ater than that given by the log; especially if a great

great sea sets after her. In this case, it is usual to allow one mile in 10, or less when the sea is less. And the contrary will happen if a sea be against the ship: For then the ship's way may be less than the distance measured by the log. The time and setting of the tides must also be carefully consider'd.

All or most of these things about correcting the departure, are only suppositions, and depend mostly upon the judgment of the artist; but though not infallible, are the only means afforded for making

these corrections.

7. When several ships sail upon the same voyage, the coincidence or concurrence of their reckonings will confirm them; and their disagreement may help to correct them all. And if you can get an account of any ships you meet, what longitude and latitude they suppose they are in: you may compare that with your own account; which perhaps may give you some light how to correct it.

'SCHOL.

If the much defired method of finding the longitude by fome observation or other, could ever be found out (which I doubt never will); then there would be no need of this proposition. For as by an observation of the sun, or a star the latitude is known; so by some like observation would the longitude be known. But this has hitherto prov'd a task insuperable.

The corrections here given suppose that there is not an error in both course and distance. And yet it is equally probable there may be in both as well as in one. Now if it happens that one of them nearly ballances the other, as to latitude; then we

are not sensible of any error, and yet in this case there must be an error in the longitude; though there is no possible way to discover it. Again, If they both tend one way, or make a confiderable diff. in the latitude, yet they may make little in the longitude: and yet we are obliged to correct the longitude in proportion to the latitude, though perhaps it needed none.

PROP. XXVII.

To keep a Journal, or Sca Reckoning.

A journal is a punctual writing down in the journal book, the courses, distances, dist. latitude, and departure, the ship makes every day; and what latitude and longitude she is in. And also the weather, and all remarks.

1. This book must be a quarto, of 2 or 3 quire of paper, or more, according to the length of the voyage. Each page must be rul'd into columns, of a fufficient depth, the same as you have on the log-board, in Prop. XXVI. and one towards the right hand, in which the corrected courses are to be put. The first column is for hours, number'd 2, 4, 6, &c. for common voyages; and 1, 2, 3, &c. for the East India voyages; which therefore must be made deeper. The second column is for the couries. The third for the knots, or distances run in an hour. The fourth winds. The 5th must be large, it contains Remarks, such as the transactions of that day, as winds, weather, currents, fetting of the fea, handing of fails, meeting or parting with thip, death of men, variation of the compass, and all other accidents and occurrences whatever; particularly the fun's altitude, declination, lat. by observation, true and magnetical amplitude, and variation. To these you must add a 6th co-

lumn for the courfes corrected.

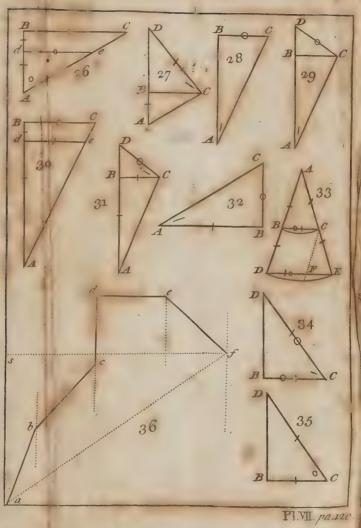
The title of the journal must declare the latitude and longitude of the place sail'd from, and also the latitude and longitude of the place sail'd to, or of the first place you come at, if you sail to several. And the course and distance from one to the other; to be sound by case I Mercator, and case 2 plain sailing.

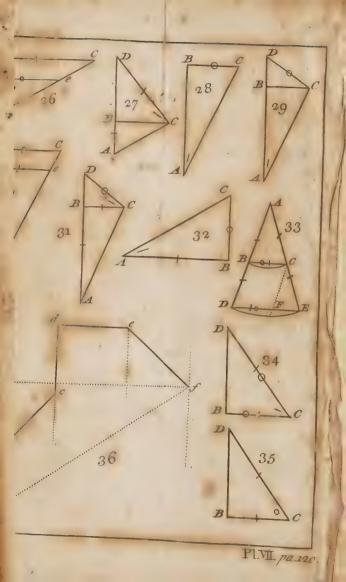
2. Below these you must have other columns, ruled in form of a traverse, as in Prop. XXIV. into this you must put the corrected courses, points, distances, northing, southing, easting, and westing, as found by Prop. XXV. I would put this into the journal, because, when any mistake happens it may easily be examin'd and corrected. And it takes but little room, for out at sea in long voyages, the winds are not so variable as near land, and a ship has no occasion to alter her course so often.

But if any one chooses rather to leave it out, he must be very correct in finding the diff. latitude and departure.

3. Near the bottom, you must make other short columns; in these are to be put the northing, southing, easting, and westing, the latitude and longitude; first by account, and then corrected; all which may be seen in the following pages. Your book must be made and ruled before you go to sea, and then it will be ready for use, which being done, every page will contain a day's reckoning.

4. Every





4. Every day at noon write into the journal book, the fame you find written on the log-board. And then you must work up your days reckoning, according to the directions of Prop. XXV. which you must write into the columns below, if you chuse to insert them in the book.

5. Having thus got the diff. latitude and departure, and latitude and longitude, put them into their respective columns at the bottom of the page, against the title (by account). Take care to get an obfervation of the sun or a star as often as you can, and from thence find the lat. by Prob. IX. Part I. And from this correct the place of the ship by Prop. XXVI. and put these corrected diff. lat. departure, latitude, and longitude, into the columns at bottom against the title (corrected). Also as often as you can, take an observation to obtain the variation, by Prob. XVI. P. 1.

After this manner you are to proceed every day from noon to noon, till the voyage be finish'd. And you must be sure to look out for land some days before you expect, by your reckoning, to be at it.

But instead of putting the remarks into a column

But instead of putting the remarks into a column on the left hand side, you may allow the whole page on the right hand for them if you please; and then you will have but one day's work in a leas. Or you may contrive any other method of keeping a journal, provided it be commodious and short; and so that you can but understand it clearly yourself. For different men will have different methods: But that method is the best which is the shortest, provided it be equally true.

Where you part with the land, you must pitch upon that, or some remarkable place to take your departure from; till such time as you get an ob-

fervation

fervation to fet all right. As in the following example of 3 days run, where the lat. long. and departure is reckon'd from the Lizard.

Example.

In the following form of a journal. In the first day, April 20, where you have a point variation, all the courses, when corrected, will differ a point, and besides where you have 1½ point lee-way, a N. W. b. N.½ W. course becomes a N. W. b. N. and I point lee-ways reduces an E. S. E. course to an E. Also as there is a current setting W.N.W. this is consider'd as a W.b.N. course, after allowing for variation; all which see in the sig. or table below it; from whence you get the diff. lat. 70, departure 36; and therefore the lat. 48 45, and longitude 12 01, sound by Prop. XXV. All these you have by account, as placed at the soot of the page; but none corrected for want of an observation.

In the 2d day, April 21, we get the fun's amplitude at fetting, and the next day his meridian altitude. And finishing that day's reckoning by Prop. XXV. we get the lat. 47 31, longitude 8 58, as below by account. But from the fun's declination 12 14, we get (by Prob. IX, Part I.) the latitute 47 54: fo that we have out-run our reckoning 23 miles fouth. Now, having the declination, we get the sun's true amplitude 18 30 (by Prob. IV.) and from this (by Prob. XVI.) we find the variation, which is 9 degrees. So now I fee we have allow'd too much variation, and therefore the fault must be supposed in the course. Proceeding then by Prop. XXVI, I find the correction in departure 21, and in longitude 30; whence we get the latitude and longitude corrected; the lat. 47 54, and long. 8 28. And the like for the third, or any other day's reckoning.

A

JOURNAL

Of a VOYAGE

IN THE

SWEEPSTAKES;

From the Lizard Lat. 49 55 N. Lon. 12 56. to Jamaica Lat. 18 o N. Long. 301 7.
In the Year 1754.

The Course S. 61 13 W.
Distance 3977 Miles.
A. B. Master. Kept by C. D. Mate.

A JOURNAL.

Monday April 20th, 1754.

Hours.	Courfes.	Knots.	Winds.
2 4 6 8 10	S.W.b.S. S. N.W.b.N. [‡] W.	7.1 7.5 8.0 8.5 4.6 5.3	N.W. W.N.W. W.b.N W.N.W S.W.
2 4 6 8 10 12	S.W. S.E. S.W. E.S.E.	5·4 5·5 8.0 4.1 4.2 4.1	W.b.S. N.N.W. E.S.E. S.

Courfes.	Poi.	Dift.	Nor.	Sou.	East.	West.
S.S.W. S.b.E. N.W.½W. N.W.b.N. S.W.b.S. S.E.b.E. E. Currents W.b.N.	2 1 4 ½ 3 3 5 8	14.6 16.5 9.9 5.4 17.7 4.1 4.1	6.6	14.7	3.2	5.6 7.3 3. 9.8 —
			11.7	16.7 35.0	10.7	28.7
		doubled	1	70.0		36.0

	Courses corrected.
Variation 1 point W.	s.s.w.
Fair brifk gale. Lost fight of the Lizard at 7, bearing N. ½ E. Past by the (Phænix) to the Westward.	S.b.E. N.W.±2W
ι ½ point lee-way.	N.W.b.N 3.W.b.S.
A Current fetting W.N.W. for 3 hours, at 2 miles an hour. I point lee way.	S.E.b.E. S.W.b.S. E.

1	April zi,	North.	South.	East.	West	Lat.	Long.
I	By account	_	70.0		36.0	48 45	12 01
	Corrected.						

G 3

Tuelday

A JOURNAL.

Tuesday April 21.

Hours.	Courses.	Knots.	Winds.
2 4 6 8 10	W.b.S	3.0 3.5 5.1 6.0 7.3	E.b.S. N.E.b.E.
2 4 6 8 10	S.W.b.W.	7·3 7·0 10.0 8·3 6·3 4·9	N.E,b.N. N.b.E.

1	Courfes.	Poi.	Distance.	Nor	South.	East.	West.
	W.S.W. S.W.b.W.	6	20.6		7.8	-	19.1
	S.W.	4	46.2	-	3.4	_	38.5
					36.9		61.0
			doubled		73.8		122.0

Remarks.	Courles corrected.
1 Point variation W.	W.S.W.
Sun's amplit, obf. 27 30. Saw a fail to the N.N.E.	
Snow and rain.	S.W.b.W.
Top tails reev'd.	
Hard gale,	
Clear again. Sun's mer. alt. 54 20 observ'd.	s.w.

April 22	North.	South.	Eait.	West.	Lat.	Long.
By account	and species a	73.8		122.C	47 31	8 58
Corrected		50.8		101.0	47 54	8 28

A JOURNAL.

Wednesday April 22.

diours.	Couries.	knots.	Winas.				
2 4 6 8 10	S.b.W.	0 0 1.0 1.2 1.5 2.0	W.				
2 4 6 8 10	S	2.4 3.1 3.1 3.0 3.4 3.4	s.w.				

Courles.	Points.	Distance.	Nor.	South.	East. West
S. ≩ E, S.S. E. ≟E.	3 2 1 2 1	8.1 16.0		8.0	6.9
				22.5	8.1
		doubled		45.0	16.2

Remarks.	Courses corrected.
Variation o d. W. No wind, fair weather. A fmooth sea. Lee-way 1 point.	S. 3 E.
Lee-way 1 ½ point.	S.S.E. ½E.

April 23.	Nor.	South.	East.	West.	Lat.	Long.
By account		45.0	16.2		47 9	8 52
Corrected.						

An alphabetical Table of the most remarkable Seaports, Capes, Islands, Straits, Gulfs, Bays, Harbours, Rocks, River-Mouths, in the World: with the Latitude, and Longitude, counted from the Meridian of the westermost of the Canary Islands.

Note, I. for Isle; B. for Bay.

A.					
	La	titude.	Lo	ng.	1
	D.	M.	D.	M.	
A BACCO I	26	30 N	300	50	l
Abdeleur I.	12	10 N	72	-	1
Aberdeen	57	24 N	16	33	
Aboo	60	40 N	39	20	
Abrollo I.	21	20 N	309	30	ı
Admiralty I.	75	5 N	78	0	ı
Agalega I.	9	37 S	73	21	ı
Alboran I.	36	10 N	15	40	
Alderney I.	49	16 N		15	ł
Alexandria	31	7 N		0	
Algiers	36	40 N		15	
Alicant	38	54 N	18	20	
Alligranfa I.	28	55 N	0	57	
Amboina	3	50 S		20	
Ameland I.	53	30 N		30	
Amsteldam I.	39	56 S	92	34	
Amsterdam	52	21 N	23	0	
Anain I.	119	42 N	114	45	
Ancona	43	31 N	32	50	
Andaman I.	13		109	35	
Andreo I.		2.	297	52	
Androis I.	18		299	10	
Anegada I.	8	0 1	315	26	
Angola	10		34 guilla	6	
		4711	2 ulli2	4 4 -	

	,La	titude.	Lo	ng.	
	D.	M.	D.	M.	
Anguilla I.	18	13 N	317	15	
Annabona I.	1	42 S	27	c	
Anout I.	156	44 N	29	8	
Antega I.	17	o N		50	
Anticosti I.	47	35 N	317	25	
Antilles If.	15	o N	308	o	
Antiochetta	36	40 N	49	47	
Antiochia	-135	54 N	57	30	
Antwerp	51	10 N	22	30	
Aquapulco	17	o N	271	42	
Aquatulco	15	27 N	277	7	
Archangel bar	65	5 N	53	40	
Arenfburg	58	o N	41	40	
Arian If.	54	55 N	8	20	
Arica	18	12 S	304	0	
Aruba I.	12		309	42	
Ascension I.	8	10 S	5	35	
Afinora I.	41	o N	27	40	
Affains B.	40		191	0	
Affene	4		17	10	
Athens	38	o N	42	40	
Atkins Key I.	22		303	55	
Atwoods Key's If. Azore If.	23	70.7	304	40	
Azore 11,	39	o N	350	0	
B.					
ь.	þ	1			
Baffin's B.	66	- N			
Bahama Bank, N. point	28		255	0	
Bahama II.	1		299	55	
Bajona If.	27		299	12	
Baldivia	42	- 1		46	
Bailafore —	39		296	50	
Bamf	ı	2 -1	16	30	
Banca I.	57	-		25	
Bandy I.	3	0 1		32	
Bantan I.	5		4 7	47	
Barcelona	5		C.	30	
G 6	19		bado		
		A 64.6	MINUTE OF	les	

· · · · · · · · · · · · · · · · · · ·	Lat	itude.	Lo	ng.
	D.	M.	D.	M.
Barbadoes I.	13	10 N	320	7
Barbuda I.	17	43 N	318	45
Bargazar point	56	30 N	356	30
Barfey L.	52	46 N	13	12
Bass I. See	49	ON	14	10
Bassos de Chagos I.	5	5 S	88	35
Batavia I.	5	37 S	130	37
Bayonne	43	50 N	16	40
Beachy	50	48 N	18	35
Beerenberg I.	71	45 N	22	40
Bell I. (America)	52	5 N	324	0
Bell I. (France)	47	20 N	15	O
Bell Sound	77	15 N	30	50
Bellfast	54	36 N	14	32
Bencola I.	3	50 S	119	23
Bengal	22	27 N	110	0
	60	o N	23	50
	32	30 N	316	40
Berwick : "	55-	50 N	16	31
Bieque I.	18	ON	314	55
Bilboa Wo	43 -	30 N	15	10
Bifcay B.	45	o N	16	0
Black point S.End	78	ON	28	40
	11	7 N	308	20
	50	45 N	16	35
	37	ON	25	10
Bonair I.	12	22 N	312	12
Bonaventure B.	3	28 N	298	4
	16	5 N	345	47
Borgo	60	40 N	47	26
Borneo I.	I	32 N	138	0
	55	27	33	3
Boston (New England)	+2	35 T	309	20
Bourd x	14	50 N	17	46
	14	35 N	343	4
Breda	51	30 N	23	15
	53	50 N	27	10
Brest	48	33 N		46
			В	rill

Latitude Long D. M. D.
Brill
Britfol 51 32 N 15 35 15 0 N 15 0
British If. Buchaness Buenos Aires Bull's B. Burlings Buffera Button's B. 53
Buchaness Buenos Aires Bull's B. Burlings Bushera Button's B. 57 55 N 13 50 320 40 47 40 N 49 32 7 55 8 8 67 15 8 66 0 N 255 0
Buenos Aires Bull's B. Burlings Buffera Button's B. 35 10 S 320 40 47 40 N 49 32 39 39 N 7 55 30 0 N 67 15 66 0 N 255 0
Bull's B. 47 40 N 49 32 Burlings 39 N 7 55 Buffera 30 0 N 67 15 Button's B. 66 0 N 255 0
Burlings Buffera Button's B. 39 39 N 7 55 30 0 N 67 15 66 0 N 255 0
Buffera Button's B 30 0 N 67 15 66 0 N 255 0
Button's B. 66 0 N 255 0
Button's M. 60 5 N 308 20
3 1 100 20
C
Cabos I
Cadiz 36 16 N 11 10
Cairo 30 5 N 52 30
Caldy I. 51 33 N 12 56
Calecut 11 17 N 93 4
Calais 50 57 N 20 10
Calmer 56 45 N 34 45
Camanes If. 19 0 N 297 10
Camarica B 48 25 N 13 42
Camofe 65 43 N 53 24
Campeche 19 20 N 285 5
Canary If. 27 56 N 2 0
Cancross bank, N. point 20 50 N 306 55
Candy I 35 22 N 43 9
Canea 35 30 N 42 22
Cantam 23 30 N 131 30
Cape Verd If 18 0 N 355 0
Cape Avalilla - 12 10 N 127 13
- Bajador 26 12 N 3 40
Barbador 39 0 N 46 0
Barbernola 38 35 N 46 5
Barcan 78 25 N 40 21
Bassos 4 0 N 68 0
Blanco, (America) 46 50 S 306 5
Blanco (Africa) 20 35 N 1 15
Cape

	Lat	itude.		ıg.	
	D.	M.	D.	M.1	
Cape Bona	37	5 N	28	10	
Bonavista	49	II N	326	7	
Briton	46		319	50	
Candinofe	69	27 N	60	40	
Cantin	32	16 N	8	50	
Catacho	21	12 N	339	15	
Charles	62	35 N	302	50	
Charles	37	14 N	303	55	
— Churchil —	59	ON	7	40	
Cipige -	42	o S	190	0	
Clear	51	10 N	7	40	
Cod	42	10 N	310	25	
- Cold	79	55 N	28	10	
Collone	37	30 N	23	14	
Colona	37	30 N	43	34	
Comerine	7	50 N	96	35	
Coquibaca -	12	50 N	307	30	
Corientes (Africa)	23	52 S	53	45	
Corientes (America)	19	40 N	267	40	
Corfe	4	40 N	20	34	
De Gat ·	37	3 N	19	8	
De Geer	30	4 N	8	0	
De Hague	49	46 N	16	4	
Del Ajuga	16	38 S	289	20	
Del Gado —	10	OS	58	0	k
De St. Andrews -	38	50 S	314	55	
— De tres forcas —	35	34 N	17	44	į
- De Verd	19	30 N	2	0	
Defolation	62	ON	335	0	
Elizabeth	62	2 N	311	20	
Fair .	34	o N	300	0	
Falfo	9	o S	.57	0	
Farewell	59	10 N	331	25	
- Finister -	43	6 N	8	10	
Florida	24	46 N	296	15	
Formoía -	4	40 N	26	10	
Frio .	22	52 S	337	40	
Gallo de Zelone	6	7 N	98	5.5	
				apel	
				-	

	La	titude.	Long.	¢ .
p	D.	M.	D. M.	
Cape Glado	25	50 N	81 44	
- of Good Hope -	34	25 S	35 35	
Guardufoy	II	50 N	70 40	
Hatteras	35	10 N	303 45	
- Henrietta Maria	155	6 N	295 8	1
Henry	137	ON	303 40	
Hinlopen	39	4 N	304 45	Į.
Hogue	49	46 N	16 4	1
— Honduras —	16	25 N	290 20	
Horn	57	58 S	298 15	
Jones	55	3 N	299 55	Н
Lagulias	35	35 S	36 50	Н
Malacca	20	25 N	121 30	
Martello -	38	o N	43 55	
Martin -	39	ON	18 38	
— Matapan —	36	25 N	40 30	-
Matricaria	15	23 N	70 20	
May	39	15 N	304 31	
- Miserato	32	43 N	34 33	
Monte	6	23 N	8 5	
- Monte Sancto	40	5 N	44 15	
— Muca	26	56 N	75 20	
Naffau -	8	25 N	320 15	
Negrais	26	23 N	111 15	
Negro	16	8 S	33 0	
Non	28	52 N	6 40	
- Olerado	23	41 N	2 20	
- Orange	4	5 N	326 45	
- Ortegal	44	2 N	10 30	
Palmaris	20	17 21	106 20	
Palmo	4	3 N	12 34	
Passero -	36	48 N	34 14	
Paul	37	58 N	17 48	
Pinas Pinas	44	45 N	12 10	
Race	46	-	324 45	
Roque	5	1	342 18	
Rofulgat	22	27 N	78 55	
Ray	48	21 NI	320 55	ť
*			Roxo'	

	La	titude. Long.
	D.	М. D. М.
Cape Roxo	12	0 N 2 10
- Rufato	33	15 N 40 5
Sable	43	45 N 314 45
Saint Anglo	36	41 N 41 30
St. Antonia	21	50 N 291 38
St. Augustine	8	5 S 342 32
St. John (Candy)	35	20 N 41 37
St. John (America)	50	9 N 325 35
- St. Lucas	23	25 N 266 14
St. Mary (Italy) -	39	56 N 37 10
- St. Mary (America)	47	10 N 324 50
- St. Sebastian	42	30 N 248 15
- St. Thomas	23	10 S 32 33
St. Vincent -	37	o N 8 38
Sapiensa	37	10 N 40 0
Sardini	35	35 N 45 50
Spartavento	38	o N 38 8
Spartel	35	46 N 12 15
Solomon	35	25 N 44 40
- Southampton -	61	57 N 289 40
Tenes	36	30 N 19 55
Three-points -	4	13 N 18 55
Tidelles —	37	4 N 23 10
Trefalgar	36	10 N 11 40
Verd	15	ON O O
Victory	52	15 S 294 50
Virgins	9	0 N 4 0
Virgin Mary	52	0 S 303 5
Walfingham -	63	5 N 300 30
Caperwick ———	59	20 Ni 28 20
Capria I.	43	6 N 27 50
Caragoli	19	30 N 3 20
Caribbee If.	16	0 N 318 0
Carlisle	54	45 N 14 45
Cartagena (Europe)	37	30 N 16 55
Carthagena (America)	10	50 N 302 20
Carthage	35	0 N 29 30
Caskets	49	50 N 15 38
	-	Cat

		La	titude.	Lor	ng.
		D.	M.	D.	
Cat I.	-	24.	25 N	302	50
Cathness		58	37 N	12	0
Cattaro	-	4.2	40 N	38	4.0
Cayenna I.	-	5	o N	320	25
Celebes I.		2	20 S	137	40
Ceuta .		35	50 N	13	10
Ceylon I.	-	35	30 N	100	0
Charles I.	the second secon	78	ON	32	0
Charles Town		32	40 N	299	20
Chefalonia I.		38	15 N	40	O
Cherry I.		74	35 N	36	15
Chiloa	(800)	42	o S	308	o
Christiana		59	10 N	27	55
· Christianstadt		56	35 N	33	0
Chufan If.	-	30	38 N	138	45
Cima		12	30 S	304	40
Civitavecchia		41	47 N	30	13
Cochin	-	9	58 N	94	55
Cocos I.		14	10 N	100	12
Coket I.		55	20 N	16	55
Columba	-	7	7 N	98	15
Comero I.	-	II	50 S	61	55
Commora If.		10	oS	63	0
Conception B.	Jan. 1997	47	5'3 N	324	0
Coningsberg	-	55	o N	38	40
:Constantinople	-	41	7 N	48	10
Contessa		41	30 N	43	0
Copenhagen		55	44 N	30	45
Corfu I.	-	39	45 N	38	52
Cork		51	49 N	8	4C
Corfica I.		42	o N	27	55
Corvo I.		40		348	15
Cosmelodo I.		10	o S		55
Cow and-Calf	-	51	22 N		34
Cromer		53	10 N		15
Crooked I.		22	2	304	10
Cross I.		66	31 N	2 (43
Cross point		72	o N	/	22
Cuba Î.		22	o NI2	299	cl
\$1.7 ph		0		t	he

Z. Z		1 0 1	2000	
		itude.	Lon	g.
1 0 11	D.	M.	D.	M.
the Cubbs —	54	18 N		20
Curafo I.	12	40 N		55
Cyprus I.	35	28 N	5 T	IC
D				
Dadul		4 BT	0.2	
Dago I.	18	3 N	1 "	10
Dantzick	59	0 N 22 N	41	IO
Dartmouth	54	27 N	37	IC
Dearfound	50	15 N		34
Defar	79	0 N	72	50
Delft	52	10 N	1 /	45
Deman	20	6 N	91	40
Dermemel	55	30 N	39	46
Derwinda	57	20 N	40	IC
Dewpoint	15	50 N		15
Diep	49	56 N	17	4
Dinhead	20	42 N	87	40
Dien I.	46	40 N	15	55
Digo Gratiosa I.	8	42 S	87	15
Digo Roys I.	19	45 S	79	45
Domenel's	57	30 N		IO
Dominico I.	15	35 N		43
Dort	51	45 N	23	0
Dover	51	15 N		28
Downs	51	25 N		31
Drakes B.	38	16 N		20
Drontem	63	30 N		40
Dublin	53	20 N	II	4
Dumfrife	55	28 N	14	40
Dundee	156	30 N	15	34
Dunkirk ———————————————————————————————————	51	o N		30
Durazzo	50	38 N		47
Durazzo	40	40 N	20	30
E				
Edinburgh		NT		
Edistana	155	57 N	1	24
	150	12 N	13	
			E	lbin

"	Lati	tude.	Lon	g. r
	D.	M.	D. 1	
Elbin	54	20 N	39	10
Elfingberg	56	o N	31	40
Elfinor	56	o N	30	42
Emden -	53	5 N	26	10
Enchuysen	52	50 N	23	15
Engano I.	5	40 S	119	3
Ephefus —	37	54 N	45	25
Escondite	18	20 N	1 /	IC.
Exuma I.	23	25 N	302	13
F				
D: 6 1 1				
Fairforeland ———	55	5. N	II	40
Fair I.	59	30 N		5°
Faro Sound	58	3 N	37	C
Farrahead	58	23 N	13	5
Fermo Fernando I.	43	10 N	15	30
Fero If.	62	35 N	30	5
Ferro I.	28	o N		42
Final —		10 N	27	_
Fisher's I.	44 70	o N	44	48
Fisher's If.	41	20 N		40
Flambrough Head —	54	8 N	18	10
Flores I. (Azores)	39	40 N		20
Floris I.	8	50 S	142	40
The Fly	53	18 N	23	45
Fontarabia —	43	30 N	15	30
Formentaria I.	38	44 N	20	c
Formofa I.	23	46 N	138	9
Fort St. George	13	8 N	99	10
Fortaventuro I.	27	54 N	4	46
Foul found	77	30 N	31	c
Freejuls	43	30 N	25	30
Fretum borough	69	55 N	80	15
Fuogo I.	14	42 N	343	42
Furness	51	is N	21	0
Fyal I.	38		350	54
				G

)	LATITUDE and LUN	GL	LUD		
		Lat	itude.	, Lo	ng.
	, G	D.	M.	D.	M
	Gallopega I.	0	0	288	0
	Galloway	53	10 N	17	25
	Gamart If.	65	48 N	350	40
	Gambaroon I.	27	30 N	74	46
	Gallitta I.	37	40 N	26	44
	Gelder	52	ON	23	30
	Genberman's Rocks	66	23 N	357	20
	Genoa	44	25 N	26	50
	Gibralter	36	II N	12	27
	Gigeria	37	6 N	24	40
	Girona	41	45 N	22	0
	Glasco	55	53 N	14	5
	Goa -	15	22 N	92	47
	Gomera I.	28	o N	0	44
	Gorgona I.	43	34 N	27	48
	Gothland I. — —	58	o N	37	0
	Gottenburgh -	57.	33 N	30	35
	Granado I. — —	12	7.N	317	40
,	Grand I. — —	44	o N	34	35
	Gratiofa — —	39	25 N	0	18
	Grey's I.	50	35 N	324	45
		66	51 N	349	57
	Grimsa I.	67	22 N	355	26
	Guaina I. — —	16	52 N	289	40
	Guardalupa I. — —	16	15 N	318	47
	Guatimala — —	14	25 N	273	10
		49	36 N	15	30
		54	o N	38	0
	T: 1	4 I	o N	43	10
		59.	50 N	43	0
	7	23	o N	90	30
	7.7	12	30 N	2 I	30
	TO C	24		288	0
	C.1.	27	ON	68	0
	0.1 .	10		290	10
p	. 011	41	10 N	41	0
	m	33	ON	39	0
	371		30 N	35	30
	Venice	14	o N	33	C
					H,

	1		1
\mathbf{H}_{-}	Lat	itude.	Long.
Hadeibarran 1	D.	M.	D. M.
Hacluit's Headland Halliford	79	55 N	
	64	30 N	343 27
Hambrough Harbour I.	53	41 N	28 34
Harlem	25	40 N	301 35
0.11.0	52	25 N	22 30
Hartland point	5 I	6 N	13 35
Hartlepool ———————————————————————————————————	54	40 N	17 16
Havana	52	II N	19 28
Havre de Grace	2.2	50 N	
Heel	50	o N	18.30
Hermanos I.	54	40 N	27
Helies found	3	2 S	82 10
Helighland —	79	15 N	30 15
Hispaniola I.	54	28 N	26 45
Hockfew -	19	10 N	~ 2 1
Hoingan ———	26		136 30
	33		137 15
Holy head Holy I.	53	23 N	13.30
Hondy B.	55	45 N	16 40
v	22	35 N 22 N	293 30
***	76		
TY C- 1	64.	42 N	
Hornfey I.	77.	23 N	0 0
TY 10 4 D	60	.0 S	190 0
Hull -		ON	,
Hyneago I.	53	48 N	17 43
Trylleago 1.	20	57 N	304 50
T			
. %			
Jago I		7A"	
Jamaica I.	15	20 IN	344 32
James Town			300 . 6
Japan Is.	37	10 N	303 Q
Jaque jaque	39	.0 N	
Java 1.	4	16 N	, ,
Ice point	7	40 S	
Tec Politic	17.7	40 N	
			Iceland

	Latitude.		Lor	g.
	D.	M.	D.	M.
Iceland I.	66	o N	350	0
Jersey I.	49	56 N	16	15
Illathera I.	25	o N	302	8
Joanna I.	12	15 S	62	43
Joppa	32	46 N	54	10
Juan Fernando I.	33	20 S	291	22
K				- 4
A				
Kalmer	56	40 N	34	50
Kaftof	44	o N	51	0
Kilduin	69	32 N	48	25
Kinfale	51	50 N	8	30
Koningfburg —	54	55 N	40	40
Kureshihii	41	40 N	57	50
_				
L				
La Serena	24	40 S	301	38
La Valona	40	56 N	39	34
La vera Cruz	19	15 N	277	45
Ladrone Is.	18	o N	162	0
Lambay	53	24 N	10	40
Lampo	30	10 N	38	35
Lancerotta I.	28	32 N	5	16
Landfort	58	40 N	36	30
Lands end	50	6 N	12	47
Langeness	66	56 N	5	10
Larissa	39	30 N	22	0
Larwick	58	54 N	27	30
Lawenburgh	53	20 N	29	10
Lees Foreland	78	50 N	41	35
Leghorn ————————————————————————————————————	43	18 N 0 N	28	40
Lemnos I.	39	50 N	15	15
Lepanto	38	20 N	43	37
Lefon I.	57	5 N	28	50
	58	30 N		3
	.) -	3021		boa

Lilboa I. Lima Limmeric Limpadofa I. Limpadofa I. Lifbon Lifbon Rock Liverpool Lizard Loefort I. London Londondery Long I. Lopas Lubeck Luconio I. Lunde Lundy I.	Lat D. 44 12 52 36 35 42 38 53 49 68 51 54 40 1	10 M. N. 30 S. 22 N. N. 58 N. N. 55 N. N. 55 N. N. 30	Lor D. 28 30-4 17 32 28 7 15 12 27 18 18 18 19 29 138 32 13	15 0 30 51 15 50 10 30 30 15 60 0 30 30 30 30
Maccao Madagafcar I. Madera Is. Maelftroom Maefterland Maerden Magadoxo Magellan Straits Mailla Majorca Malacca Malaca Malaga Maldivia If. Malique If. Malta I. Mansfield I.	22 32 67 57 58 2 51 33 36 4 9 36 54 66 66 66 66 66 66 66 66 66 6	13 N 29 N 30 N 30 N 58 N 58 N 58 S 55 N 8 N 30 N 15 N 20 N	132 58 0 30 29 27 62 302 125 19 118 21 32 13 302 Mai	45 45 56 0 55 53 40 16 40 25 45 29 40 18 20 20 20 20 20 20 20 20 20 20 20 20 20

	Lat	itude.	Lo	g.
	D.	M.	D.	M.
Margaritta I.	11	20 N	315	50
Marigallante I.	15	53 N	319	50
Maritimo I.	38	12 N	30	5
Marfeilles	43	20 N	23	25
Martinico I.	14	48 N	319	45
Marzaness	66	8 N	354	IO
Masipore -	16	30 N	ICO	7
Mauritius I.	20	5 S	73	15
May I.	15	16 N	345	30
Mayaguana I.	22	35 N	305	IC
Mayetta I.	14	ioS	63	55
Melinde	3	o S	58	10
Meraparvouz I.	2 I	57 N	303	30
Merchant's Foreland	63	41 N	355	C
Messina	38	22 N	34	35
Middleberg -	51	35 N	22	7
Milford	55	44 N	13	25
Mill.Is.	64	20 N	298	2
Mindano I.	6	30 N	137	0
Minorca Is.	39	48 N	20	50
Mocha	14	40 N	63	30
Modon	36	52 N	39	20
Mohilla I.	12	15 S.	61	51
Mollona	30	12 N	300	0
Mombafo	4	15 S	56	40
Monlock point	41	8 N	308	C
Monrose	56	40 N	16	25
Monserado -	6	5 N	8	50
Monferrat I.	16	40 N	318	35
Montpelier -	43	20 N	21	4¢
Morlaix	48	37 N	14	20
Mosaimbique	75	5 S	58	40
Mucaros I.	2 I	30 N	301	35
Mull J.	57	20 N	11	5 C
· · · · · · · · · · · · · · · · · · ·				
	-			
Nangafac ——	32	2 .	146	c
Nanquin	32	52 N		151
			N	an-

	Latitude.		Lor	ig.
	D.	M.	.),	M
Nantucket I.	40	58 N	309	42
Nantz	47	14 N	16	20
Naples	41	5 N	32	38
Narve	58	39 N	46	20
Nasfau I.	2	44 S	. 16	42
Naze of Norway	57	50 A	25	32
Negropont I.	38	30 N	43	52
Nevis I.	17	16 IV	;17	52
Newcastle	54	58 N	16	40
Newfoundland I.	49	o N	324	0
New York	41	ON	306	5
Nicarague Entrance	11	15 N	293	5
Nice	43	15 N	26	0
Nicober I.	2	44 S	116	42
Nimpo	30	0.N	120	0
Niphon I.	36	ON	155	0
Northbergen	66	16 N	23	50
North Cape (Lapland)	71	25 N	40	10
North Cape (America)	2	5 N	328	15
North Foreland	51	28 N	19	20
Nottenburgh -	60	o N	50	40
Nottingham I.	63	38 N	298	24
0				
•				
Oczakow	45	30 N	49	40
Oeland I.	57	ON	35	
Old Head	51	40 N	5	40
Oleron I.	46	ON	17	36
Orbitello	42	15 N	30	10
Oran	35	46 N	19	15
Orfordness	52	20 N	19	20
Orkney Is.	59	13 N	14	40
Oronoque -	8	15 N	319	5
Oftend	51	10 N	15	15
Otranto	40	52 N	37	10
Ovedo	43	30 N	II	0
Oyfel I.	58	O N	41	50
Н				P

A CONTRACTOR	29	1
P	Lati	itude. Long.
*	D.	M. D. M.
Padrabancha Rocks —	6	o N 88 30
	45	32 N 30 40
Padua	38	20 N 32 28
Palermo I.	28	50 N 0 10
Palma I.	40	50 N 31 10
Palmarolla I.	8	56 N 295 52
Panama	36	53 N 31 19
Pantalaria I.		
Panuco	23)
Papey I.	64) · · · · · · · · · · · · · · · · · · ·
Parumbuke	7	48 S 243 15
Parnaw	58	25 N 43 57
Patmos I.	37	30 N 45 10
Pekin	39	52 N 134 15
Pelting Sound -	00	32 N 47 0
Penmark	47	48 N 13 55
Petersburg	59	45 N 48 20
Philippine Is.	12	0 N 140 0
Pico I.	38	32 N 351 40
Pike of Teneriff	68	25 N I O
Piply	21	15 N 106 40
Pifa -	43	8 N 29 50
Piscadore Is.	23	30 N'135 45
Placentia	147	57 N 323 10
Planofa I.	42	32 N 28 49
Platewrack	20	3 N 310 0
Plymouth -	150	36 N 13 57
Point look out	76	40 N 34 35
Policastro	40	18 N 34 30
Poma I.	43	14 N 34 10
Pondy -	18	45 N 106 20
Pondicherry -	I I	54 N 98 30
Port del Gada	10	17 S 58 20
Port Mahon -	59	42 N 22 32
Port Nelfon -	57	5 N 285 20
Port Royal -	118	
Fort Steven	46	50 5 295 34
Porta Nova	11	45 N 97 54
		Porta

	Latitude.		Lor	ig.
	D.	M.	D.	M.
Porta Port -	41	18 N	-8	50
Porto	4E	10 N	10	20
Porto Bello —	9	33 N	298	25
Porto Rico	18	33 N	313	50
Porto Sancto I.	32	50 N	2	20
Portland —	50	30 N	15	22
Portland	64.	2 N	357	54
Portfmouth	50	48 N	17	10
Princes I.	6	30 S		12
Princeps I.	I	25 N		10
Providence I.	25	o N		25
Pullacat	13	30 N	98	32
				1
Q		1		- 1
Quabella I.				- {
	3	49 S	70	50
Quebeck ————————————————————————————————————	47	5 N	308	20
Quemoy —	63	32 N	9	19
	24	35 N	135	5
Quiconga — — — Quilo — —	10	o S	32	C
Quiola	8	50 N	94	0
Quipla	9	40 S	56	C
Quipia	37	o N	28	C
. R				1
DC			,	
	44	44 N	36	
	63	25 N		4C
2	60	28 N	40	45
	44	25 N	31	30
	46	13 N		4C
	61			
	59	o N	42	55
	36 -6	40 N	46	10
	56	50 N	43	a
	52	32 N		5
- Amazons	0		329	10
— Camerones	4	2 NI	3 I	20
Н 2			W1	VOC

4	Latitude.		Lo	ng. 1
	D.	M	D.	M.
River Congo	5	45 S	33	35
Croce	35		138	0
Danube	46	o N	50	0
de Angra	0	49 N	31	25
Churchil	59	ON	283	10
de Fuegos	0	o N	59	25
Don	5 I	o N	65	0
Dwina	65	o N	62	0
- Ebro	40	20 N	19	0
Elbe -	54	o N	28	0
Formofa	7	o N	25	50
— Gambia —	14	0 N	I	30
Ganges	23	o N	104	0
Garonne	44	o N	41.3	30
Grande (America)	3 L	55 S	356	30
Grande (Africa)	I'I	40 N	3	30
Guadiane —	36.	30 N	IO	0
Humber	53	30 N	18	12
Indus	25	o N	86	0
Infanto	30	o S	46	0
Julian	48	40 S	303	38
Kiang	32	o N	138	20
Lamas -	I	20 S	58	2.3
- Loyre -	47	o N	15	30
Nile	3 I	ON	50	0
Niper	47	30 N	ξI	0
Oby	70	o N	80	1 0
Oder	54	o N	28	0
Oronoque	10	o N	282	0
Plate	35	o S	292	0
Po Rhine	45	ON	31	0
Roine	52	o N	23	0
	42	40 N	22	20
Rupert —	5°I .	16 N	299	1 5
St. Andrew	5	o N	14	55
St. Francisco	10	55 S	340	24
	30	25 S	48	25
St. Mary	22.	08	53	0
			Sam	ion'

River Samfon Sana Senegal Sefter Severn Seyne Tajo Tees Thames Tiber Viffule Volga Volto Zambre Zara Rochel Rodonto Rome Romeras de Caffellanes I. Rook point Rofanna Rofes Rofloc Rotterdam Roven Rum Key I. Runnen I.	La D. 4216 5149 3859 5146 46517 4664 545517 4664 545517 4664 545517 4664 545517 4664 545517 4664 545517 5464 5464 5464 5464 5464 5464 5464 546	1 titude. M. NNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNN	D. 31 3		
Sable I. Sacatra I. Saint Antonio I. Augustine Bartholemew I. Brandon I. Catharines I. H 3,	44 12 17 30 17 16 28	54 N 38 S	73 342 300 317 82	5 47 22 20 25 40 20 int	

	Latitude.		Lo	ıg.	
	D.		D.	M.	
Saint Christopher's I	17	22 N	317	3.5	
Cruz.I.	17	38 N	315	34	
David's Head	51	55 N	12	48	
Domingo	18	15 N		20	
George I.	38	56 N	352	0	
Helena I.	16	6 S	12	30	
John de Lisbon ——	26	4 S	71	48	
John's Harbour	47	28 N		15	
Juan de novo I.	17	30 S		45	
Kilday	58	2 N		- 5	
Laurence I.	12	30 S	68	20	
Lucia I. (Cape Verd Islands)	16	45 N	342	40	
- Lucia I. (Caribbee Islands)	13	52 N	318	53	
Malo ——	48	60 N		20	
Martin's I.	18	5 N	317	30	
Mary's I. (Scilly)	49	58 N	11	50	
Mary's I. (Azores)	37	o N	355	53	
Matthews I	I	40 S	10	15	
Michael I.	38	o N	355	38	
Nicholas	16	40 N		20	
Paul I.	1		320	20	
Pedro I.	12	o N		0	
Salvador	13	o N		0	
Sebastian	13	32 N		43	
Thomas I.	0	0		8	
Valery	50	10 N		6	
Vincent I.	. 3	13 N		48	
Vincent I.	.6		342	32	
Sal I.	16		345	40	
Salamanca	17	ON	1	0	
Sallee :	33	43 N		40	
Salonica	ŤI.	30 N	.42	0	
Salibury I.	63/	48 N		40	
Sambrero I.	18'	40 N		40	
Sardinia I.	39	30 N		44	
Scanderoon	36	o N		8	
	54	20 N		30	
Scaw	57	26 N		20	
The state of the s			Sci	relin	

	ı Lati	tude.	Lon	9. 1	
	D.	M.		M.	
Schelin -	53	25 N	24	8	
Scio I.	38	20 N	42	5	
Scots fettlement -	8	9.1	299	25	
Segura port —	16	22 S	337	12	
Selam I.	8	20 S	120	23	
Semesto I. —	35	46 N	32	25	
Senegal -	15	16 N	2	30	
Senta —	35	55 N	12	23	
Serration —	8	36 N	5	55	
Sevil -	37	37 N		34	
Shark point — —	64	27 N		50	
Sheals -	55	2 N	16	50	
Sherbrough Fort	6	o N	5	0	
Shetland Is.	60	43 N	15	40	
Siam B.	13	o N	129	II	
Siatto I.	39	10 N	43	55	
Sicily I.	37	o N	32	0	
Sinfunday B.	42	45 S	309	10	
Sky I.	57	48 N	13	10	
Sline Head	53	20 N	6	55	
Sluyce	51	19 N	22	0	
Smyrna	38	30 N	45	37	-
Snow Hill	65	11 N 22 N	350		İ
Sound Royal -		0	353	27	ı
South Cape	44	0 S		20	
South Foreland	51	58 S	1 " 7		
Spirito Sancto	19	0 N	336	0	1
Spitsberg	78	35 N		40	
Spurn	53	10 N		48	Ì
Stadland	41	10 N		40	
Stalimene I.	50	9 N	15	5	
Start Point	62	o N	335	30	l
Staten I.	159	20 N	36	35	
Stockton Stockton	54	33 N			ŧ
Straelfound	54	45 N		30	
Straits of Annian	50	ON		-	
Babelmandel —	12	ÖN		30	ŧ
H 4			-	raic	

	Latitude.		. Long.	
	D.	M.	D.	M.
Straits of Coffa	44	30 N	55	С
Constantinople	41	ON	47	30
Corfica	42	o N	27	2C
Dampiers -	6	o S	165	С
- Davis's -	70	ON	292	C
Dover	51	ON	19	20
	36	ON	12	C
Hellespont —	40	ON	45	c
Hudson's	62	oN	275	C
- Magellan		40 N	293	C
Meffina	53	ON	34	c
Ormus	28	o N		c
		2 7	75	1
of the Sound -	56		30	40
Sunda	5	52 S	124	C
Uriez	46	ON		0
Weigate	71	ON	83	С
Strombello I.	39	o N	34	4C
Sumatra-I.	5	35 S	104	C
Sunda If.	5	o S	123	C
Sunderland	54	52 N		50
Suranam	6	o N	321	15
Surat	21	8 N	/ /	35
Surroy	17I	- 5 N	34	5C
Sufa	35	50 IV	28	12
Sweetnose	68	8 N	1 2	52
Syracule	37	15 N	34	45
				- 1
Т				
trans of an		2		
Tabasco	19		286	
Tadasock	149	01		4.
Tangier	35	55 N	II	
Taranto	10	40 N		
Tarragon	40	55 N		41
Taffo I.	40	10 N	8 1 4	5.
Tenerif I.	128	20 N	1	25
Tercera I.	38	53 N	1353	28
Terra del Fuogo I	54	08		
Terra del Gada	119	29 5		
1000	,	,	Tell	tigos
				0

	Latitude.		Long.		
	D.		D. I	VI.	,
Testigos I.	II	40 N	315	25	
Tetuan —	35	28 N	12	18	į
Texel —	53	10 N	23.	- 6	
Tobago I.	II.	10 N	318	50	Í
Todus Sanctus B.	13	o S	337	35	
Tongon	5-	10 S	57	17	
Topfham:	50	37 N	13	25	
Torneo	65	51 N		15	i
Tortofa	40	54 N		24	1
Toulon	43	6 N		50	
Trinidada	0	30 S		10	9
Trinidada I.	10		318	5	1
Trinity B.	48	27 N	323	15	1
Tripoli -	33	5 N	32	20	1
Tristian de Cunha I.	37	5 S	12	32	
Tromfound	70	18 N		10	1
Truxillo	9	40 S	305	0	
Tunis —	36	50 N	28	FO	1
Tunquin -	20,	50 N	128	15	١
Turks I.	21	35 N	308.	P	1
V	1				
	1	9.7			
Vagaron	17:	o N		0	
Valencia	39	15 N		40	
Valsterborn — —	55	20 N		5	
Varna —	4.5	o N		C	
Venice	45	18 N	1 -	20	
Verkin's I.	2	. 22 N		17	
Villarica	20	o N	283	C	Ē.
Viner's I.	53	' 5 N	294	57	
Virgin's I.	18.	23 N		48	
Virgin's Rocks	46	· 6 N	12 "	5	
Visegapatam -	17		103	17	4
Uraniburgh	55	54 N	31	0	
Ushant I.	48	30 N		. 5	
Uffica	138	54 N	32	14	1
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W	La	titude.	Lor	g. F
	D.	M.	D.	M.
Wardus	71	10 N	47	30
Waterford	52	7 N	10	20
Watling I.	24	7 N	303	20
Westmania If.	63	51 N	349	32
Wexford -	52	30 N	10	5-1
Whales Back -	65	27 N	357	37
Whales Head was a series -	177	18 N	39	4.0
Whitby -	54	30 N	17	20
-Whitehaven -	54	25 N	14	551
Wight I	51	o N	16	30
Wilby -	57	37 N	37	C
Wilmar -	54	30 N	30	16
Wyborg —	50	.20 N	47	36
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X				
and the second			n	- 1
Xango a minute of the same	12	o S	58	C
1 14 1 10 2 1			1	
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The Transfer of the Control		NI	¥.0	
Yarmouth -	52	45 N		5
Yas de Amber 1.	0	0	70	10
Yas de Digo roys I.	0	10 N	9.0	I
Yla I.	56			14
Yvica	39	5. N	21	
ž				
E Company				
77 Y	27	47 N	39	20
Zant I.	37.	ON		10
Zara	10	10 N	3. 5	
Zeila	33	ON		
Zuchris	17	1 N		22
Zunaquitta I.	1.	4 N		4
Zuphen.	152	4 1	4)	1

An A'phabetical T A B L E of Sea Terms.

BAFT or Aft. Backwards, behind, towards the stern. Aboard. In the ship, Aloft, On high. Alsof. At a distance; falling from the wind. Amain. All at once. Avast. Stop, hold.

B

to Bale. To empty water with buckets. Beacons. Fires or lights on the sea coast, to prevent ship-wreck, invasion, &c.

to Bear in. To fail towards.
to Bear off. To keep off; to thrust off.
to Bear up. To keep more into the wind. Becalm'd. Wanting wind.

to Belay. To fasten a running rope after it is haled; which is done by folding it feveral times about fome timber head, &c.

to Bend. To bind; to fasten.

Berth. A convenient place, and distance to moor in.

Bight. Any part of a rope as it is coil'd up.

on Board. In the ship. Bulg'd. Stav'd, broke in.

Bunt. The bag of a fail.

By a Wind. Near the wind; or as near against it as possible.

Captain. The commander of a ship, having a H 6 commission.

A TABLE of SEA TERMS.

Close. Near to.

· 156

to Cond. To direct the man at the helm how to fteer.

Crank. Apt to lie aside, or turn over to Cun. To direct the steering.

D

Dead Ropes. Those which run not in blocks.

Dead Water. The eddy at the stern of the shipto Drive. To fall away with the wind or tide.

E

to Eafe. To flacken.

End for End. When a rope is all run out.

Eow. All pull together.

F

Fack or Fake. One circle of a rope coil'd up, the Fall. That part of a rope which is pull'd at, to Fall off. To go further from the wind. to Fend. To defend, to thrust off. to let Fly. To let go.

Fore and aft. Along the ship, from head to

Foul. When a rope is fo' intangled, that it cannot run.

Founder'd. Sunk, by taking in water.

Fraight or Freight. The burthen of goods a ship carries.

to Furl. To bind up close.

G

to Gripe. To-run too much into the wind.

A TABLE of SEA TERMS.

to Gull. To Gall, to eat or wear.

H

Handspike. A wooden leaver, to heave with.

to Hale. To pull at a rope.

to Hail. To call at; as Ho, the hip.

Head sea. A great sea meeting the ship a-head.

to Heel. To lie or lean to one fide.

to Hitch. To catch a thing with a rope or hook.

to Hoist. To hale up.

Home. Comes toward you.

Ironfick. When the nails and bolts are eaten away with rust.

K

a Kenk. A fmall turn or fnarle, on a rope.

T.

Larboard. The left fide of the ship, as a man looks forward.

Large Wind. When a ship goes almost before the wind, or when the wind comes on the quarters, that is, makes half a right angle, or more with her way.

to Lash. To bind any thing to the ship sides, &c.

Lasking Wind. A large wind. to Lay the Land. To get without fight of land.

Lee. Fromwards the wind.

Lee Shore. The shore on which the wind blows. Leeward. From the wind; or the place towards which the wind blows.

158 A TABLE of SEA TERMS.

Loof up. Keep near the wind. to Loom. To appear.
Luff. Loof.

M

to Moor. To lye at anchor, by help of two anchors, &c.

N

Neap'd. A ship is neap'd, when the tides are

fo small as not to carry her out.

Near the Wind. This is when a ship fails with her head almost against the wind, or as near as she can come. This is also call d, By a wind, or Upon a wind.

No near. Come no nearer the wind, but keep

more to leeward.

O

Offing. The part of the fea at a good distance from the land.

to Overhale. To hale back. Overfet. Turn'd over.

P

a Peek. Right under; a-cross.

to Pitch. To fail with the ship's head in and out of the sea, so as to endanger the masts; to tos forward and backward.

Port. The left or larboard side. A haven.

to Purchase. To gain, or bring in.

Q

Quarters. The back parts of the ship, adjoining to the steerage. Quarter

Quarter Watch. When only a quarter of the

company watches.

Quarter Winds. Are those which come upon the quarters, or make about half a right angle with the keel.

to Quoil. To lay the fakes of a rope round about,

upon one another.

R

a Reach. The distance between two turnings of a river.

to Reeve. To put through.

to Ride. To be kept in one place by an anchor, or anchors.

Right the Helm. Put it streight; or to neither side.

Rife the Tack. Slacken it.

a Road. A place where a ship may ride at anchor near the land.

S

to Seaze. To make fast; to bind together.
Seeling. Rocking from one side to the other.

to Send. To fall with the head or stern into the trough of the sea.

Sheering. When a ship goes not steady, but in and out.

Slatch. The part of a rope that bags or hangsloofe.

a Spell. Any one's turn to labour.

to Splice. To make the ends of ropes fast together, by working strands into one another.

Speening. Putting a ship right before the wind and sea, without any sail, in a storm.

to Spring. To crack. Standing

Standing Ropes. Such as run not in blocks. Starboard. The right side of the ship, when you look forward.

Steady. Keep the helm at rest.

to Stow. To put goods into a ship in proper order. Strap. The rope spliced about a block, commonly with an eye.

to Strike. To let fall the fails; to beat on the

ground.

to Tack about. To bring a ship about, so that her head may lie as much to the right hand of the wind, as it did before to the left: and the contrary.

under a Tack. When she sails close by a wind, o

near the wind.

Tacks aboard. When the starboard tack is aboard, the starboard side of the sail is hal'd forward by the Tack; and the larboard fide, backwards by the sheet; and then the wind comes on the. starboard fide of the ship; and she makes her' way to the left hand of the point the wind blows from, or to the right of the direct way of the wind; and on the contrary, when the larboard tack is aboard, the wind comes on the larboard fide.

Taunt Mast. A high mast in proportion for the

ship.

Taught, Tight, stiff, fast.

Thus, Thus. When the ship is right steer'd.

Tide and half Tide. A tide three hours longer or later.

Tight. Water proof. to Tow. To drag after the ship.

Trim. The posture or position she sails best in.

Trough

Trough of the Sea. The hollow between two waves.

Try. To go under the main fail, or mizen fail, only.

V

to Veer out. To let a rope run out. Veering. Sailing large.

W

Wake. The smooth, white, frothy, water, astern of the ship; running out to a good distance. This shows the way the ship has fail'd. Walt. Wanting ballast.

to Warp. To hale a ship to any place with a haw-

fer, when the wind is wanting.

Watch. Half the ship's company, which keeps watch for four hours at sea.

to Weather. To get to windward.

Weather Bow, Weather Side, &c. That next the weather or wind.

Weather Shore. That from whence the wind comes.

Wending. Turning about, when lying at anchor.

to Wind. To bring the ship's head about.

Windward. I hat part from whence the wind comes; and opposite to the leeward.

a Windward Tide. That which goes with the

a Wreck. A ship cast up, that perish'd at sea.

Y

Yare. Nimble, ready, quick.
to Yaw. To go in and out, or to the right and left,
with the head.



A Traverse TABLE, or Table of Difference of Latitude, and Departure in Wiles; to every quarter Point of the Compass, and every Degree of the Quadrant.

To find the diff. Latitude and Departure for any Course and Distance.

RULE.

Look for the course at the head or soot of the table where you can find it, and then for the distance on the left hand side; Against which distance, in the column of the course, you have the distant and departure, in their proper columns; under the words Lat. Dep. if the course is on the top; and above the words Lat. Dep. if at bottom of the table. If the distance be greater than the table contains (which seldom happens), it must be taken out at twice or thrice.

Examp. 1. Let the distance sail'd be 24 miles, and the course $3^{\frac{1}{2}}$ points from the meridian. Under $3^{\frac{1}{2}}$ points, and over against 24 on the side, you have 18.6 for the diff. lat. and 15.3 for the

departure.

Examp. 2. Let the distance run be 85 miles, and the course 67 deg. from the meridian. Because the distance exceeds the table, it must be taken out at twice, for the two distances 60 and 25 which make 85. Thus, above 67 the course at bottom, and against 60 on the side, you have the dist. lat. 23.4, and departure 55.2: Again, Above 67, and against 25, you have the dist. lat. 9.8, and departure 23.0, therefore the whole dist. lat. is 33.2; and the whole departure 78.2.

				-
D	是 Point.	½ Point.	3 Point.	1 Point.
7	Lat. Dep.	Lat. Dep.	Lat. Dep.	Lat. Dep.
I	1.0' 0.0	1.0 0.1	1.0 0.1	1.0 0.2
2	2.0 0.1	2.0 0.2	2.0 0.3	2.0 0.4
3	3.0 0 1	3.0 0.3	3.0 0.4	2.9 0.6
4	4.0 0.2	40 0.4	4.0 0.6	3.9 0.8
5	5.0 0.2	5.0 0 5	5.0 0.7	4.9 1.0
6	6.0, 0.3	60,06	5.9 0.8	5.9 1.2
7	7.0 03	7.0 0.7	6.9 1.0	6.9 1.4
8	8.0 0.4	8.0 0.8	7.9 1.2	78 1.6
9	9.0 04	9.0 0.9	8.9 1.3	8.8 1.8
10	10.0 0 5	10.0 1.0	C.9 I.5	98 2.0
II	11.0 0.5	109 1.1	10.9 1.6	10.8 2.1
12	12.0 0.6	11.9 1.2	11.9 1.8	11.8 2.3
13	13.9 0.6	129 1.3	129 1.9	12.8 2.5
14	14.0, 0.7	13.9 1.4	13.9 2.0	13.7 2.7
15	15.01 0.7	14.9 1.5	14.9 2.2	14.7 2.9
10	160 00 08	15.9 1.6	15.9 2.3	15.7 3.1
17	17.0 08	16.9 1.7	16.9 25	10.7 3.3
18	180 0.9	17.9 1.8	17.8 2.6	17.7 3.5
19	19.0 00	18.9 1.9	188 28	18 6 3.7
20	20.0 1.0	19.0 2.0	19.8 2.9	196 3.9
21	21.0 1 0	[-c.9, 2.1	20.8 3.1	20 0 4.1
22	22.0 1.1	21.9 2.2	21.8 3.2	21.6 4.3
23.	1 3	22.9 2.3	22.8 3.4	226 4.5
24.	1-4-1	23.9 2.4	23 8 3.5	23.6 4.7
25	25 0 1.2	24.9 25	24 8 3.7	24.5! 49
26	260 1 3	25.9 2.0	25.7: 3.8	25.5 5.1
27	27.0 1 3	26.9 2.7	26.7 4.0	26.5 5.3
28	28.0 1.4	127 9 2.8	27.7 4.1	27.5 5.5
29	29.0 1.4	28.9 29	28.7 4.3	128.4 5.7
30	30.0 1.5	29.9 2.9	29.7 4.0	9 4 5.8
	Dep Lat.	Dep ar.	Dep. at.	Dep Lat.
1	74 Point.	117 T Out.	7 4 Point.	7 Points.
-				-

D	& Point.	Point.	3 l'oint.	I Point. 1
. F	Lat Der	Lat. Dep.	L t. Dep.	Lat. Dep.
Dif. 31 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 57 57 58	-	-	30.7 4.6 31.7 4.7 32.7 4.9 33.7 5.0 34.6 5.2 35.6 5.3 36.6 5.5 37.6 5.6 38.6 5.8 30.6 5.9 40.0 6.1 41.6 6.2 42.5 6.4 43.5 6.5 44.5 6.7 45.5 6.8 46.5 7.0 47.5 7.1 48.5 7.2 49.5 7.3 50.4 7.5 51.4 7.6 52.4 7.8 53.4 7.9 54.4 8.1 55.4 8.4 57.4 8.5	
59 60	59.9 2.9	59.7 5.9	58.3 8.6 59.3 8.8	57.9 11.5
	Dep. Lat.	Dep. Lat.	Dep. Lat.	Dep. Lat.
7	7 3 Point	7 & Point.	7 1 Point.	7 Points.

15.1	L Poin'.	T Point.	1. 3 Point.	2 Points.
Jut.	L:.1.11).	at. Dep	.10-1.	L t. Dep.
	1.0, 0	1.00.3	0.9 0.3	0.9 0.4
2	1.9 0.5	1,90.6	1.9 0.7	1.8 0.8
3	2.9 0.7	2.90.9	2.8 1.0	2.8 1.1
5	3.9 I.0 4.8 I.2	3.81.2	3.8 1.3	3.7 1.5 4.6 1.9
6	5.8 1.4	5.7 1.7	5.6 2.0	5.5 2.3
7	6.8 1.7	6.72.0	6.6 2.4	6.5 2.7
8	7.8 1.9	7.6 2.3	7.6 2.7	7.4 3.1
9	8.7 2.2 9.7 2.4	9.62.6	8.5 3.0 9.4 3.4	8.3 3.4 9.2 3.8
11		10.5 3.2	10.3 3.7	10.2 4.2
12	10.7 2.7	11.5 3.5	11.3 4.0	11.1 4.6
13	12.6 3.1	12.4 3.8	12.2 4.4	12.0 5.0
14	13.6 3.4	13.44.1	13.2 4.8	13.0 5.4
15	14.6 3.6	14.3 4.4	14.1 5.1	13.9 5.8
16	16.5 4.1	15.34.7	15.0 5.4	14.8 6.1
18	17.5 4.4	17.2 5.2	16.9 6.0	16.7 6.9
19	18.4 4.6	18.25.5	17.9 6.4	17.6 7.2
20	19.4 4.8	10.15.8	18.8 6.7	18.5 7.6
21	20.4 5.0	20.1 6.1 21.0 6.4	19.7 7.0	19.5 8.0
23	21.3 5.3	22.05.7	20.7 7.4	21.3 8.8
24	23.3 5.8	23.07.0	22.6 8.0	22.2 9.1
25	24.2 6.0	23.97.3	23.5 8.4	23.1 9.5
26	25.2 0.3	24.97.6	24.4 8.7	24.0 9.9
27	26.2 6.5	25 8 7.9	25.4 9.0 26.3 9.4	25.0 10.3 25.9 10.7
29	28.1 7.0	27.7 8.5	27.2 9.7	26.8 11.1
30	29.11 7.3	28.7 3.7	28.2 10.1	27.7 11.5
	Dep. Lat.	Dep. Lat.	Dep. Lat.	Dep. Lat.
1	16 3 Point.	6 ½ Point.	6 B Point.	6 Points.

-				
	1 4 Point.	Point.	1 3 Point.	2 Points.
	in 1Dep.	Lat. Dop.	Lat. Dep.	Lat. Dep.
31	30.1 7.5	29.0 9.0	29.1 10.4	28 (11.9
32	31.0 7.7	30.6 9.z	30.110.8	29.5 12.3
33	32.0 8.0	31.6 9.5	31.011.1	30.5 12.7
34	33.0 8.2	32.5 9.8	31.9 11.4	31.413.1
35	34.0 8.5	33.5 10.1	32.9 11.8	32.3 [3.5
36	34.9 8.7	34.4 10.4	33.8 12.1	33.2 13.8
37	35.9 9.0 36.9 9.2	35.4 10.7	34.8 12.4	34. I 14. 2
39	37.8 9.4	36.3 11.0	35.7 12.8 36.7 13.1	35.014.6
40	38.8 9.7	38.311.6	37.7 13.5	36.915.3
41	39.8 9.9	39.211.9	38.(13.8	37 8 15.7
42		40.212.2	39.6 14.1	38.7 16.1
43		41.112.5	40.5 14.5	39.616.5
44		42.1 12.8	41.4 14.8	40.616.9
45	43.7 10.9	43.0 13.0	42.4 15.1	41.517.2
46		44.0 13.3	43.3 15.5	42.4 17.6
47		44.913.6	44.3 15.8	
48	1 1 1	45.9 13.9	45.2 16.1	
49		46.9 14.2	46.2 16.5	
50		47.8 14.5	47.1 16.8	
5 1		48.8 14.8		
52		49.7 15.1	49.017.5	
53		50.715.4	49.5 17.9	
5		52.616.0	51.8 18.6	
5		53.5 16.3		
5		54.5 16.6	31.	
5.	8 56.314.0	55.416.9		
		56.4 17.1	1 55.6 9.0	
16	9 57 - 14 - 3	57.417.4		2 55.2 23.0
	Dep Lit.	Dep. Lat	. Dep. Lat	. Dep. Lat.
1	6 3 Point	6 2 Point	6 + Poin	t. 6 Points.

101	2 Point.	2 Foint.	2 3 Point.	3 Points.
F	L Dep.	Lat. Dep.	Lat. Dep.	Lat. Dep
1	0.9 0.4	0.0 0.5	0.9 0.5	0.8 0.6
2	1.8 0.9	1.8 0.9	1.7 1.0	1.7 1.1
5	2.7 1.3	2.6 1.4	3.4 2.1	2.5 1.7
4 5	3.6 I.7 4.5 2.I	3.5 I.9 4.4 2.4	3.4 2.1	4.2 2.8
1	5.4 2.6	5.3 2.8	5.1 3.1	5.C 3.3
7	6.3 3.0	6.2 3.3	6.0 3.6	5.8 3.9
8	7.2 3.4	7.0 3.8	6.9 4.1	6.7 4.4
- 9	8.1 3.8	7.9 4.2	7.7 4.6 8.6 5.1	7.5 5.0
10	9.0 4.3	8.8 4.7		
11	9.9 4.7	9.7 5.2	9.4 5.6	9.2 6.1
13	11.7 5.6	11.5 6.1	11.1 6.7	10.8 7.2
r4	12.6 6.0	12.4 6.5	12.0 7.2	11.7 7.8
15	13.5 6.4	13.2 7.0	12.9 7.7	12.5 8.3
16	14.5 6.9	14.1 7.5	13.7 8.2	13.3 8.9
17	15.4 7.3	15.0 7.9	14.6 8.7	14.2 9.4
18	16.3 7.7	15.9 8.4	15.4 9.2	15.0 10.0
19	18.1 8.6	17.6 9.4	17.110.3	16.611.1
21	19.0 9.0	18.5 9.8	18.010.8	17.5 11.7
22	19.9 9.4	19.410.3	18.911.3	18.3 12.2
2:	20.8 9.8	20.3 10.8	19.7 11.8	19.2 12.8
: 24	21.7 10.3	21.211.2	20.1 12.3	20.0 13.3
125	22.6 10.7	22.1 11.7	21.4 12.8	20.8 13.9
121	23.5 11.1	23.6 12.2	22.3 13.3	21.7 14.4
127	1 8	24.7 13.1	24.0 14.3	22.5 15.0
. 20	11 7 3	25.6 13.6	24.9 14.8	24.1 16.1
: 30	27.112.8	26.5 14.1	25.7 15.4	24.0 16.7
1	Dep. Lat.	Dep. Lat.	Dep. [lat.	Dep. Lat.
	15 3 Point.	5 ½ Point.	5 4 Point.	5 Points.
1				

Dia	2 Yount	-1 'oin'	3 Point	3 Poin
7	Lat De j	Lat. Lie	Lat. isty.	La
31	28.0[13.	27.41 1.5		4,
32	28.913.	28.2 : 5.0	27. 5.4	26
33	29.8 14.1	29.115.5	28. 6.9	27. 8
34	30.7 14.6	30.0 15.9	29. 17.4	28.
35	31.6 15.0	30.0 16.4	10.017.0	20. 6
3¢	32.5 15.4	31. 16.6	30.9 18.5	29. :0
3-	33.415.8	32.6 17.4	31.7 19.0	30.: 0.
38	34.3 16.3	33.5 17.9	32.019.5	31. i.
39	35.2 16.7	34.4 18.4	33.4 20.1	32. 1.
40	35.1 17.1	35.3 18.9	31. 20.1	33. 2.
41	37.0 17.0	36.2 19.3	55.1 21.1	34. /4.
42 43	37.5 18.0	37.119.8	36.021.6	34. 3.3
44	38.8 18.4	38.4 20.3 38.8 20.8	36.9 22.1	35- 23.6
45	40.(19.1	39.7 21.2	28.6 23.1	36. 34.
46	41.(19.7	40.6 21.7		
17	42.5 20.1	41.5 22.2	40.2 24.2	30. 25.6
18	43.4 20.t	42.4 22.7	41.1 24.7	39. 25.
19	44.5 21.0	43.2 23.2	12.0 25.2	40 27.
;0	45.2 21.4	44.1 23.6	12 6 25.7	41. 27.
5 I	46.121.8	45.C 24.1	+3.7 20.2	42. 28.
32	47.0 22.3	45.0 24.5	14.6 26.7	43.2 28.9
53	47.9 22.7	46.8 24.9	45.4 27.2	44.1 29.4
;4	48.8 23.1	47.7 25.4	46.327.7	44.0 ;0.0
55	49.7 23.6	48.5 25.9	47.1 28.3	45.: 30.E
56	50.6 24.0	49.4 26.4	48.c z8.8	46.0 1.1
57	51.524.4	50.3 26.8	18.5 29.3	47.4 31.7
;8	52.4 24.8	51.2 27.3	19.7/29.8	
50	53.3 25.2	52.6 27.8	50.1 30.3	
1,0	54.2 25.6		\$1.5 30.8	
	Dep. Lat.	Dep. Lat.	Dep. Lat.	Dep ar.
1	53 Point	5½ Point	5 Point.	5 Points.

	1 1 Pointe	137 Points.	33 Points.	4 Points.
Dif.	Lat. Dep.	Lat. Dep.	Lat. Dep.	Lat. Dep.
1				
2	0.8 0.0	0.8 0.0	1.5 1.3	1.4 1.4
3	2.4 1.8	2.3 1.9	2.2 2.0	2.1 2.1
4	3.2 2.4	3.1 2.5	3.0 2.7	2.8 2.8
5	4.0 3.0	3.9 3.2	3.7 3.4	3.5 3.5
16	4.8 3.6	4.6 3 8	4.4 4.0	4.2 4.2
7 8	5.6 4.2	5.4 4.4	5.2 4.7	4.9 4.9
8	6.4 4.8	6.2 5.1	5.9 5.4	5.7 5.7
9	7.2 5.4	7.0 5.7	6.7 -6.0	6.4 6.4
10	8.0 6.0	7.7 6.3	7.4 6.7	7.1 7.1
I I	8.8 6.6	8.5 6.9	8.1 7.4 8.6 8.0	7.5 7.8
12	9.6 7.2	9.2 7.5	8.9 8.0 9.6 8.7	8.5 8.5
13	10.4 7.8	10.8 8.8	10.4 9.4	9.9 9.9
15	12.0 9.0	11.6 9.4	11.110.0	10.610.6
16	12.8 9.6	12.4 10.1	11.9,10.7	11.3 11.3
1-	13.6 10.2	13.2 10.7	12.6 11.4	12.012.0
18	14.4 10.8	14.0 11.3	13.412.0	12.7 12.7
19	15.2 11.4	14.7 12.0	14.1 12.7	13.4 3.4
20	16.111.9	15.5 12.7	14.813.4	14.1 14.1
21	16.912.5	16.3 13.3	15.0 14.1	14.8 14.8
2.	17.7 3.1	17.113.9	16.3 14.8	15.615.6
23	18.5 13.7	17.5 [4.6]	17.1 15.5	16.316.3
22	19.3 14.3	18.(15.3	18.6 16.8	17.717.7
[20.2 16.6	19.3 17.5	18.418.4
2:	20.6 5.5	21.0 17.2	20.118.1	19.119.1
28	22.5 16.7	21.7 17.8	20.7 18.8	19.819.8
20	23.3 7.3	22.5 18.4	21.5 19.5	20.5 20.5
30	1.1 17.9	23.1 9.0	22.2 20.1	21.221.2
	Dep. Lat.	Dep. Lat.	Dep Lat	Dep. Lat.
	13 Points.	4½ Points.	4 Points.	4 Points.
-				

1	3 Points.	2½ Points.	132 Points.	4 Points.
	Lat. D-p.	Lat. Dep.	Lat. Dep.	La Dep.
31	24.010.5	24.0119.0	23.0 20.8	21.921.9
132	25.7 19.1	24.7 20.3	23.7 21.5	22.5 22.6
33	26.5 19.7	25.5 20.9	24.4 22.1	23-323.3
35	27.3 20.3	26.2 21.5	25.2 22.8	24.020
50	28.1 20.9	27.0 22.2	25.6 23.5	24.724.7
37	28.9.21.5	27.8 22 8	26.7 24.1	25.425.4
38	29.7.22.1	28.6 23.4	27.4 24.8	20.2 26.2
39	30.5 22.7	29.324.1	28.1 25.5	26.9 26.9
10	31.323.3	30.1 24.7	28.6 26.2	27.6 27.6
11		30.925.4		28.3 28.3
12	32.0 34.4	31.626.0	30.4.27.5	29.029.0
+3	33.7 25.0	33.2 37.2	31.428.9	29.7,29.7
1.1	35.3 26.2	34.027.8	32.6 29.5	30.4 30.4
115	36 1 26.8	34.8 28.4	33.430.2	31.831.8
145	36.0 -7.1	135.5 29.1	34.130.9	32.5.32.5
1.7	37.7 28.0	36.329.7	34.931.5	33.2 33.2
118	38.5:8.6	37.130.3	35.6 32.2	33.933.9
49	39 3 29.2	37.9 51.0	35.3 32.9	34.734.7
20	40.1 29.8	138.731.7	37.033.6	35.435.4
7.1	41.030.4	39.5 32.3	37.834.3	36.1;36.1
52	41.8 31.0	40.3 32.9	38.535.0	36.8 36.8
53	12.(31.6)	41.133.0	39.2 35.6	37.5 37.5
55	\$3.4 \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	41.2 4.3	40.0 36.3	38.2 38.2
				38.9 38.9
56	45.6 3.4	43.435.0	41.7 37.6 42.8 38.3	39.6 39.6
58	45.1 34.6	45.0 36.8	43.039.0	40.340.3
59	47.4 35.2	45.8 37.41	43.8 39.6	41.741.7
50	48.1 35.7	46.438.1	44.540.3	42.442.4
	Dep. Lat	Dep. Lat.	Dep. Lat.	Dep. Lat.
	4 Points.	4 Points.	41 Points.	4 Points.
-	14			

-	-				1.0	- D		- 0	
15		1 Degi	ree.	2 De	g.		eg.	4 D	
15		Lat. 11	Dep.	Lat il	Jep	Lat 1	ep.	Lat	Dep.
	1	1.0	0.0	1.0	0.0	1.0	0.0	1.0	0.1
1	2	2.0	0.0	2.0	0.1	2.0	0.1	2.0	0.1
	3	3.0	0.1	3.0	0.1	3.0	0.2	3.0	0.2
1	4	4.0	0.1	4.0	0.1	40	0.2	4.0	0.3
L	5	5.0	0.1	5.0	0.2	5.0	0.3	ζ.(0.3
	6	0.0	0.1	6.0	0.2	6.C	0.3	6.C	0.4
1	7	7.0	0.1	7.0	0.2	7.C	0.4	7.0	0.5
П	8	8.0	0.1	8.0	0.3	8.c	0.4	8.c	0.6
ı	9	9.0	0.2	9.0	0.3	9.0	0.5	9.0	0.6
I	0	10.0	0.2	10.0	0.4	10.0	0.5	10.0	0.7
I	1	11.0	0.2	11.0	0.4	11.C	0.6	11.0	0.8
1	2	12.0	0.2	12.0	0.4	12.0	0.6	12.0	0.8
1	3	13.0	0.2	13.0	0.5	13.0	0.7	13.0	0.9
	4	14.0	0.2	14.0	0.5	14.0	0.7	14.0	1.0
I	5	15.0	0.3	15.0	0.5	15.0	0.8	15.0	1.0
I	6	160	0.3	16.0	0.0	16.0	0.8	16.0	1.1
	7	17.0	0.3	17.0	0.6	17.0	0.9	17.0	1.2
- 1	8	18.0	0.3	18.0	0.6	18.0	0.9	17.5	1.3
- 1	19	19.0	0.3	19.0	0.7	19.0		18.0	1.3
	20	29.0	0.4	20.0	0.7	20.0	1.0	19.0	1.4
	21	21.0	0.4	21.0		21.0	1.1	20.0	1.5
	22	22.0	0.4	22.0		22.0	1	21.0	1.5
_	23	23.0	0.4	23.0	_	23.0		22.0	
-1	24	24.0	0.4	24.0		24.0		23.9	
	25	25.0	0.4	25.0	0.9	25.0	1.3	24.0	1.7
- 1	26	20.0	0.5	26.0	0.9	26.0	,	25.0	1.8
	27	27.0	1 -	27.0		27.0		26.	1.9
- 1	28	1	1	28.0		28.0	1 ,	27.0	
1	29	11	-	29.0		29.0	-	28.0	
I	30	30.0	0.5	30.0		30.0	1.6	29.	2.1
		Dep	Lat.	Dep	Lat.	Dep	ILat.	Dep	.Hat
1		80 1)eg.	88	Deg.	87	Deg	86	Deg.
	-						-		

□ #	1 De	gree.	2 De	grees	11 3 1	Deg.	4 I)eg.
	Lat.	Dep	Lat	Dep.	Lat.	Lat. Dep.		Dep.
31	31.0	0.5	31.0	1.1	31.0	1.6	30 9	2.2
-32	32.0	0.6	32.0	1.1	31.9	1.7	31.9	2.2
33	33.0	0.6	33.0	1.2	32.9	1.7	32.9	2.3
34	34.0	0.6	34.0	1.2	33.9	1.8	33.9	2.4
35	35.0	0.6	35.0	1.2	30.9	1.8	34.9	2.4
36	36.c	0.6	36.0	1.3	35.9	1.9	35.9	2.5
37	37.0	0.7	37.0	1.3	36.9	1.9	36 9	2.6
38	38.0	0.7	38.0	1.3	37.9	20	37.9	2.7
39	39.c	0.7	39.0	1.4	38.9	2.0	38.9	2.7
10	40.0	0.7	40.C	1.4	39 9	2.1	39.9	28
41	41.0	0.7	41.0	1.4	40.9	2.1	40.9	2.9
4.2	42.0	0.7	42 (1.5	41.9	2.2	41.9	2.9
143	43.C	0.8	43.C	1.5	42.9	2.2	142.9	3.0
14	44.C	0.8	44.	1.5	43.9	2.3	143.9	3.1
45	45.C	0.8	45.0	1.6	44.9	2.4	44.9	3.1
46	46.c	0.8	40.C	1.6	45.9	2.4	45.9	3.2
47	47.C	0.8	47.C	1.6	46.9	2.5	46.9	3.3
48	48.c	08	48.c	1.7	47.9	2.5	47.9	3.4
49	49.c	0.9	49.C	1.7	48.9	2.6	48.9	3.4
50	50.c				49.9		49.9	3.5
51	51.0	0.9	51.0	1.8	50.9	2.7	50.9	3.6
52	52.C	0.9	52.0	1.8	51.9	2.7	51.9	3.6
53	53.0	0.9	530	1.8	52.9	2.8	52.9	3.7
54	54.C	0.9	54.C	1.9	53.9	2 9	53.9	3.8
							1	
56	56.C	1.0	56.c	2.0	55.9	2.9	55.9	3.9
58	57.C 58.0	1.0	57.c	2.0	56.9	3.0	56.9	4.0
39	59.C	1.0	59.0	2.1	57.9	3.1	57.8	4.1
50	60.c	1.0	60.0	2. I	59.5	3.1	59 8	4.2
	Dep.	-	Dep.		Dep.	Lat	Dep.	
11		Jeg.		eg.	87 D		86 I	
-	1 09 2	reg.	00 L	reg. 1] 0/ D	cg. 1	1 60 1	7. E.

121	5 Deg.	6 Deg.	7 Deg.	8 Deg.
7	Lat. Dep.	Lat iDe .	Lat Dep.	Lat Dep.
i	1.0 0.1	1.0 0.1	1.0 0.1	1.0 0.1
2	2.0 0.2	2.0 0.2	2.0 0.2	2.0 0.3
3	3.0 0.3	3.0 0.3	3.0 0.4	3.0 0.4
4	4.0 0.4	5.0 0.5	4.0 0.5	4.0 0.6
5				
1	7.0 0.6	7.0 0.7	6.0 0.3	5.9 0.8
7	8.0 0.7	7.0 0.7 0.0 c.8	7.0 1.0	6.9 1.0 7.9 1.1
C	9.0 0.8	8.9 0.9	8.0 1.1	8.9 1.2
ic	10.0 0.9	9.9 1.0	9.4 1.2	9.9. 1.4
11	11.0 1.0	10.9 1.1	10.C 1.3	10.9 1.5
12	12.0 1.0	11.9 1.2	11.9 1.5	11.9 1.7
113	12.9 1.1	12.9 1.3	12.9 1.6	12.8 1:8
14	13.9 1.2	13.9 1.4	13.9 1.7	13.8 1.9
15	13.9 13	14.0 1.5	14.0 1.8	14.8 2.1
1(15.9 1.1	15.9 1.7	15.9 1.9	15.8 22
17	16.9 1.5	15.9 1.8	16.9 2.1	16.8 2.4
110	17.0 1.6	17.9 1.9	17.4 2 2	17.8 2.5
2:	100 1.7	10.9 2.1	10.8 2.4	10.8 2.8
21	2.9 18	20.9 2 2	20 8 2 6	20.8 2.9
22	21.0 1.0	21.9 2.3	21 8 2.7	21.8 3.1
-2:	22.9 2.C	22.9 2.4	22.8 2.8	22.8 3.2
24	23.9 2.1	23 9 2.5	23 8 2.9	23.8 3.3
25	24 9 2 2	24.9 2.6	248 30	24.8 3.5
2	25 9 2.3	;25.9, 2.7	25.0 3.2	25 7, 3.6
27	20.9 2.4	25.9 2.8	26.8 3.3	20.7 3.7
28	27.9 24	27.8 2.9	27.8 3 4	27.7 3.9
25		28.8 3.0	28 8 3.5	28.7 40
130	20.0 2.6	29.8 3.1	208 27	207 1.2
1	Dep. Lat	Dep Lat	rep Lat	J Dep lat
1	85 Deg	134Degree	13 iveg.	82 Deg.

2	5 Deg.	6 Deg.	7 Deg.	8 Deg.
F	Lat. Per	Lat. Dep.	Lat. Dep.	Lat. [Dep.
31	30.6 2.7	30. 3.2	30.8 3.8	30.71 4.3
32	31.9 2.8	3,1.5 3.3	31.8 3.9	31.7 44
33	32.9 20	32. 3.4	32.7 4.0	32.7 4.6
34	33. 3.0	33. 3.5	33.7 4.1	33.7 4.7
35	34 9 3.1	34. 3.7	34. 4.3	34.7 4.9
34	35.6 3.1	35.1 3.8	35.7 4.4	35.6 5.0
37	35 5 3.2	36.1 3.9	36.7 4.5	36.6 5.1
35	37.9 3.3	37.8 4.0	37.7 4.6	37.6 5.3
39	38.4	38.8 4.1	38.7 4.8	38.6 5.4
40	39.8 3.5	39: 4.2	39.7 4.9	39 6 5.6
41	40.8 36	40.1 4.3	40 7 5.0	40.6 5.7
12	41.8 3.7	41.1 4.4	41-7 5.1	41.6 5.8
43	42.8 38	42. 4.5		42.6 60
44	43.8 38	4.6	143.7 5.4	14.6 6.3
45				
40	4.5.8 4.0	45. 4.8	. 1	45.5 0.4
47	40.8 4.1	46. 4.9	11 1 1	47.5 0.7
48	47.8 4.2 48.8 4.3	47. 5.0	48.6 6.0	48.5 6 8
50	49.8 4.4	49. 5.2	49.6 6.1	49.5 7.0
-			50.6 6.2	50 5 7.1
51	50.8 4.4	50.7 5.3	11 / /	51.5 7.2
53	52.8 4.6	52.7 5.5	52.6 6.5	52.5 7 4
54	538 47	53.7 5.6		1 1
55	54.8 4.8	54. 5.7	54.6 6.7	53.5 7.5
56	55.8 49			55.5 7.8
157	56.8 50	56. 6.0	56.6 6.9	56.4 7.0
158	57.8 5.1	57. 6.1		57.4 8.1
150	58.8 5.2			58.4 8.2
160				59.4 8.3
	Dep Dat	Dep. Lat.	Dep. Lat.	Dep Lat
	85 Deg.	84 Deg	83 Deg.	82 Deg
-	, 0			

[-	
SILC	1 9 ex.	11 10 Deg.	11 Deg.	12 Deg.
-	la limp.	. r.at Dep	Lat. Dep.	Lat. Dep
	1.0 0.2	1.6 0.2	1.0 0.2	1.0 0.2
1	2.(0.3	2.0 0.3	2.0 0.4	2.0 0.4
2	3.4 Co:	2.9 0.5	2.9 0.6	2.9 0.5
4	3.0 0.0	35, 0.7	3.9 0.8	3.9 0.8
-	4. 0 8	4.0 0.9	4.9 0.9	4.9 1.0
	5.5 0.0	5.5 1.0	5.9 1.1	5.9 1.2
6,5	6.6 1.1	6.5 1.2	6.9 1.3	6.8 1.5
6	7.5 1.2 8. 1.5	7.5 1.4 8.c 1.6	7.8 1.5	7.8 1.7
110	0.0 1.6		9.8 1.7	9.8 2.1
ī,				Commence and Commercial Commercia
13	11.8 1.9	11 8 2.1	10.8 2.1	10.8 2.3
1 2	12.8 2.0	12.8 2.3	12.8 2.5	11.7 2.5
14.	13.8 2.2	13.8 2.4	13.7 2.7	13.7 2.9
15	14.8 2.3	14.8 2.6	14.7 2.9	14.7 3.1
16	15.8 2.5	15.7 2.8	15.7 3.0	15.6 3.3
17	16.8 2.7	16.7 2.9	16.7 3.2	16.6 3.5
3.1	17.8 2.8	17.7 3.1	17.7 3.4	1.7.6 3.7
IC	18.8 3.0		18.6 3.6	18.6 3.9
20	19.7 3.1	197 3.5	19.6 3.8	19.6 4.2
21	20.7 3.3		20.6 4.0	20.5 4.4
22	21.7 3.4		21.6 4.2	21.5 4.6
23	22.7 3.6		22.6 4.4	22.5 4.8
25	23.7 3.8	11 " .1 " 1	23.6 4.6 24.5 4.8	23.5 5.0
21				24.4 5.2
2	25.7 4.1		25.5 5.0 26.5 5.1	25.4 5.4 26.4 5.6
28	27.6 4.4	11 /1 / /	26.5 5.1 27.5 5.3	26.4 5.6 27.4 5.8
20	28.6 4.		28.5 5.5	28.4 6.0
36	20.6 4.		29.4 5.7	29.3 6.2
	Dep Lat	-	Dep Lat.	Dep. Lat.
	81 Deg.	80 De.g	79 Deg.	78 Deg.
-	В.	1100 20.8	11/9 20.8.	11 /0 206.

1		14	
D o Deg.		11 Deg.	12 Deg.
Lat. Dep.	Lat. Dep.	Lat. Dep	Lat. Dep.
31 30.6 4.9	30.5 5.4	30.4 5.9	30.21 0.4
32 31.6 5.0	31.5 5.5	31.4 6.1	31.: 6.6
33 32.6 5.2	32.5 5.7	32.4 6.3	32.3 6.9
34 33.6 5.3	33.5 5.9	33.4 6.5	33.2 7.1
35 34.6 5.5	34.5 6.1	34.4 6.7	34.2 7.3
36, 35.5 5.6	35.4 6.2	35.3 6.9	35.2 7.5
37 36.5 5.8	36.4 6.4	36.3 7.1	36.2 7.7
38 37.5 6.0	37.4 6.6	37.3 7.2	37.2 7.7
39 38.5 6.1	38.4 6.8	38.3 7.4	38.1 8.1
40 39.5 6.3	39.4 6.9	39.3 7.6	39.1 8.3
41 40.5 6.4	40.4 7.1	40.2 7.8	40.1 8.5
42 41.5 6.5	41.4 7.3	41.2 8.0	41.1 8.7
43 42.5 6.7	42.3 7.5	42.2 8.2	42.1 8.9
44 43.5 6.9	43.3 7.7	43.2 8.4	43.0 9.1
45 44.4 7.0	44.3 7.8	44.2 8.6	44.C 9.4
46 45.4 7.2	45.3 7.9	45.2 8.8	45.6 9.6
47 46.4 7.3	46.3 8.1	46.1 9.0	46.0 9.8
48 47.4 7.5	47.3 8.3	47.1 9.2	47.0 10.0
49 48.4 7.7		48.1 9.3	47.9 10.2
50 49.4 7.8		49.1 95	48.9 10.4
51 50.4 8.0		50.1 9.7	49.5 10.6
		51.0 9.9	50.9 10.8
		52.010.1	51.811.0
			52.8 11.2
		According to the last of the l	53.8 11.4
		55.010.7	54.8 11.6
			55.811.8
			56.7 12.1
			57.7 12.3
	_		8.7 2.5
-			Dep. Lat.
S1 Deg.	80 Deg. 11:	79 Deg. 11	78. Deg l

r magarati										
15	13 Deg.	14 Deg.	15 Deg.	16 Deg.						
, if	Lat. Dep	Lat. Dep.	Lat. Dep.	Lat. Dep						
1	1.0 0.2	1.0 0.2	1.0 0.3	1.4 0.3						
2	1.9 0.4	1.9 0.5	1.9 0.5	1.9 0.5						
3	2.9 0.7	2.9 0.7	2.9 0.8	2.9 0.8						
4	3.9 0.9	3.9 1.0	3.9 1.0	3.8 1.1						
5	4.9 1.1	4.8 1.2	4.8 1.3	4.8 1.4						
6	5.8 1.3	5.8 1.4	5.8 1.5	5.7 1.6						
7	6.8 1.6	6.8 17	6.8 1.8	6.7 1.9						
8	7.8 1.8	7.8 1.9	7.7 2.1	7.7 2.2						
9	8.8 2.0	8.7 2.2	8.7 2·3 9.7 2.6	8.6 2.5						
	9.7 2.2	9.7 2.5	Street, Street	9.6 2.8						
II	10.7 2.5	11.6 2.9	10.6 2.8	10.6 3.0						
12	11.7 2.7	11.6 2.9	11.6 3.1	11.5 3.3						
13	12.7 2.9	13.6 3.4	13.5 3.6	12.5 3.6						
15	14.6 3.4	14.5 3.6	14.5 3.9	14.4 4.1						
16	15.6 3.6	15.5 3.9	15.5 4.1	15.4 4.4						
17	16.6 3.8	16.5 4.1	16.1 4.4	16.3 4 7						
18	17.5 4.0	17.5 4.4	17.4 4.7	17.3 5.0						
19	18.5 4.2	18.4 4.6	18.4 4.9	18.3 5.2						
20	19.5 45	19.4 4.8	19.3 5.2	19.2 5.5						
21	20.51 4.7	20.4 5.1	20.2 5.4	20.2 5.8						
22	21.4 4.9	21.3 5.3	21.2 5.7	21.1 6.1						
23	22.4 5.2	22.3 5.6	22.2 6.0	22.1 6.3						
24	23.4 5.4	23 3 5.8	23.2 6.2	23.1 6.6						
25	24.3 5.6	24.3 6.0	24.1 6.5	24.0 6.9						
26	25.3 5.8	25.2 6.3	25.1 6.7	24.9 7.2						
27	26.3 6.1	26.2 6.5	26.1 7.0	25.9 7.4						
28	27.3 6.3	27.2 6.8	27.0 7.2	26.9 7.7						
.29	28.2 6.5	28.1 7.0	28.0 7.5	27.8 8.0						
30	29.2 6.7	29 1 7.3	29.0 7.8	28.8 8.3						
	Dep. Lat.	Dep. Lat.	Dep. Lat	Dep. Lat						
	77 Deg.	75 Deg.	75 Deg.	74 Deg						

-				
13	13 Deg.	14 Deg.	115 Deg.	1 16 Deg.
	Lat. Dep.	Lit. Dep.	Lat. Dep.	Lat. Dep.
3	30.21 7.0	30.1 7.5	29.1 8.0	29 8 8.5
32	31.2 7.2	31.0 7.7	30 (8.3	30.7 8.8
33		32.0 80	31.0 8.5	31.7 9.1
34		33.0 8.2	32.8 8.8	32.7 9:4
33	4 '	34 0 8.5	13 1 90	33 6 9.6
136		34.9 8.7	34 2 9.3	34.6 9.9
137		35.9 9.0	35.7 9.6	35.6 10.2
38		36.9 9.2	36.7 9.8	36.5 10.5
39		37.8 9 4	37.7 10.1	37.5 10.7
40	112-1-	38.8 9.7	38.6 10.3	38.4 11.0
41	11	39.8 9.9	39.0 10.6	39.4 11.3
142		40.7 10.2	40.6 10.9	40.4 11.6
+3 +4		41.7 10.4	41.5 11.1	41.3 11.8
45	42.9 9.9	42.7 10.6	42.5 11.4	42.3 12.1
46			143. [11.5]	43.2.12.4
47	45.810.6	44.6[11.1]	44.4 11.9	44.2 12.7
48	46.7 10.8	46.511.6	45.4 12.2	45.2 12.9
49	47.7 11.0	1 2 1	17.3 [2.7]	46.1 13.2
50	48.7 11.2	48.5 12.1	48.2 12 0	47.1 13.5
51	49.7 11.5	49.5 12.3	49.3 13.2	
52	50.711.7	50.5 12.6	50.2 13.5	49.0 14.0
53	51.611.9	51.412.8	51.2 3.7	50.914.6
54	52.6 12.1	52.4 13.1	52.2 14.0	51.9.14.9
55	53.6 12.4	53.4 13.3	53.1 14.2	52 9 15.2
56	54.5 12.6	54.3 13.5	54.1 14.5	53.8,15.4
57	55.5 12.8	55.3 13.8	55.1 14.8	54.8 15.7
58	56.5 13.0		56.c 1.5.0	55.8 16.0
59	57.5 1.3.3	57.2 14.3	57.0 15.3	56.7 16.3
00	58.5 1.3.5	58.2 14.5	58.0 15.5	57.716.5
	Dep. Lat.		Dep. Lat.	Dep. [Lat.]
	77 Deg. 11	76 Deg. H	75 Deg. 1	· 74 Deg:
-				

0	17 Deg.	18 Deg.	19 Deg.	20 Deg.
Σift.	Lat Dep	Lat. Dep.	Lat. Dep.	Lat. Dep.
I	1.0 0.3	0.9 0.3	0.9 0.3	0.9 0.3
2	1.9 0.6	1.9 0.6	1.9 0.6	1.9 0.7
3	2.9 09	2.8 0.9	2.8 1.0	2.8 1.0
4	3.8 1.2	3.8 1.2	3.8 1.3	3.8 1.4
5 6	4.8 1.5	4.8 1.5	4.7 1.6	4.7 1.7
6	5.7 1.7	5.7 1.8	5.7 1.9	5.6 2.0
7 8	6.7 2.0	6.7 2.2	6.6 2.3	6.6 z.4
	7.6 2.3	7.6 2.5	7.6 2.6	7.5 2.7
9	8.6 2.6	8.6 2.8	8.5 2.9	8.5 3.1
10	9.6 2.9	9.5 3.1	9-5 3-3	9.4 3.4
II	10.5 3.2	10.5 3.4	10.4 3.6	10.3 3.8
I 2	11.5 3.5	11.4 3.7	11.3 3.9	11.3 4.1
13	12.4 3.8	12.4 4.0	12.3 4.2	12.2 4.4
14	13.4 4.1	13.3 4.3	13.2 4.6	13.2 4.8
15	14.3 4.4	14.3 4.6	14.2 4.9	14.1 5.1
16	15.3 4.7	15.2 4.9	15.1 5.2	15.0 5.4
17	16.3 5.0	16.5 2.5	16.1 5.5	16.0 5.8
18	17.2 5.3	17.1 5.6.	17.0 5.9	16.9 6.2
19	18.2 5.5	18.1 5.9	18.0 6.1	17.9 6.5
	19.1 5.8	190 6.2	18.9 6.5	18.8 6.8
21	20.1 6.1	20.0 6.5	19.9 6.8	19.7 7.2
22	21.0 6.4	20.9 6.8	20.8 7.2	20.7 7.5
23	22.0 6.7	21.9 7.1	21.7 7.5	21.6 7.9
25	22.9 7.0	22.8 7.4 23.8 7.7	22.7 7.8 23.6 8.1	22.5 8.2
26				23.5 8.5
	24.9 7.6	24.7 8.0	24.6 8.5	24.4 8.9
27	25.8 7.9 26.8 8.2	25.7 8.3 26.6 8.6	25.5 8.8	25.4 9.2
29	27.7 8.5	27.6 9.0	26.5 9.1 27.4 9.4	26.3 9.6
30	28.7 8.8	28.5 9.3	27.4 9.4 28.4 9.8	27.2 9.9 28.2 10.3
	Dep. Lat.	-	1	
	-			Dep. Hat.
-	173 Deg.	72 Deg.	171 Deg.	70 Deg.

4 best	L. T. Davi	11 - 0 D		
150	17 Deg.	18 Deg.	19 Deg.	20 Deg.
1	Lat. Dep.	Lat. Dep.	Lat. Dep.	Lat. Dep.
31	29.6 9.1	29.5 9.6	29.3 10.1	29.1/10.6
32	30.6 9.3	30.410.0	30.3 10 4	30.010.9
33	31.6 9.6	31.410.2	31.210.7	30.911.3
34		32.3 10.5	32.111.1	31.911.6
35	33.5 10.2	33.3 10.8	33.111.4	32.9 12.0
36	34.4 10.5	34.2 11.1	34.011.7	33.8 12.3
137	35.4 10.8	35.211.4	35.0 12.1	34.8 12.6
38	36.3 11.1	36.111.7	35.9 12.4	35.7 13.0
39	37.3 11.4	37.112.0	36.9 12.7	36.6 13.3
40	38.2 11.7	38.0 12.4	37.8 13.0	37.613.7
41	39.2 12.0	39.012.7	38.8 13.3	38.5 14.0
142	40.2 12.3	39.913.0	39.7 13.7	39.5 14.4
143	41.1 12.6	40.913.3	40.7 14.0	40.4 14.7
144	42.1 12.9	41.8 13.6	41.614.3	41.3 15.0
45	43.0 13.1	42.8 13.9	42.6 14.6	42.3 15.4
46	44.0 13.4	43.7 14.2	43.5 15.0	43.215.7
47	44-9 13-7	44.7 14 5	44.4 15.3	44.2 16.1
48	45.9 14.0	45.6 14.8	45.4 15.6	45.116.4
49	46.9 14.3	46.6 15.1	46.3 15 9	46.016.8
50	47.8 14.6	47.5 15.4	47.3 16.3	47.0 17.1
51	48.8 14.9	48.5 15.8	48.216.6	47.917.4
52	49.7 15.2	49.4 16.1	49 2 16:9	48.9 17.8
53	50.715.5	50.4 16.4	50.1,17.3	49.818.1
54	51.6 15.8	51.3 16.7	51.117.6	50.7 18.5
55	52.6 16.1	52.3 17.0	52017.9	51.718.8
50	53.5 16.4	53.3 17.3	52.9 18.2	52.6 19.2
57	54.4 16.7	54.217.6	53.9 18.6	53.6 19.5
58	55.4 17.0	55.2 17.9	54.8 18.9	54.5 19.8
59	56.4 17.2	56.118.2	55.8,19.1	55.4 20.2
6c	57.4'17.5	57.118.5	36.719.5	56.4 20.5
	Dep. Lat.	Dep. Lat	Dep. Lat.	Dep. Lat.
	. 73 Deg.	72 Deg.	71 Deg.	70 Deg.
-				-

-	_								
13	ب ب	21 1	Deg.	1 22	Deg.	23.1	Jeg.	24 1	Jeg.
1	1	Lat.	Det.	Lacil	Dep.	Lat.	Dep	Lat.	U.p.
	1,	0.9	1 0.4	0.0	0.4	0.9	0.4	0.9	0.4
1	2	1.0	0.7	1.8	0.7	1.8	0.8	1.8	0.8
	3	2.8	11	2.8	1.1	2.8	1.2	2.7	1.2
	4	3.7	1.4	3.7	1.5	3.7	1.6	3.6	1.6
	5	4.7	1.8	4.6	1.9	4.6	1.9	! 4.6	20
	6!	5.6	2.1	5.6	2.2	5.5	2.3	5.51	2:4
	7 8	6.5	2.5	6.5	2.6	6.4	2.7	6.4	
ı	8	7.5	2.9	7.4	3.0	7.4	3.1	7.3	3.2
н	9	8.4	3.2	8.3	3 4	8.3	3.5	8.2	3.7
I	0	9.3	3.6	9.2	3.7	9.2	3.9	9.1	
I	I	10.3	3.9	10.2	4.1	10.1	4.3	10.0	4.5
1	2	11.2	4.3	11.1	4.5	11.0	4.7	11.0	4.9
I	3	121	4.7	12.0	4.9	12.0	5.1	11.9	5.3
1	4	13.1	5.0	13:0	5.2	12.9	5.5	12.8	5.7
I	5	14.0	5.4	13.5	5.6	13.8	5.9	13.7	6.1
Į	6	14.9	5.8	14.8	6.0	14.71	6.2	14.0	6.5
	7	15.9		15.8	6.4	15.6	6.6	15.5	6.9
	8	16.8	6.4	16.7	6.7	16.6	7.0	16.4	7.3
	9	17.7	6.8	17.0	7.1	17.5	7.4	17.4	7.7
2	0	18.7	7.2	18.5	7.5	18 4	7.8	18.3	8.1
2	1	19.6	7.5	19.5	7.9	19.3	8.2	19.2	8.5
3		20.5	7.9	20.4	8.2	20.2	8.6	20.1	8.0
2	~	21.5	8.2	21.3	8.6	21.2	9.0	21.0	9.3
2		22.4	8.6	22.2	9.0	22.1	9.4	21.9	9.8
2	5] !	23.3	9.0	23.2	9.4	23.0	9.8	22.8	10.2
2	- 13	24.3	9.3	24.1	9.7	23.9		23.7	
2		25.2	9.7	25.C	10.1	24:8		24.7	
2	- 13		10.0	26 C	10.5	25.8	10.9	25.6	1
20	/ 8	27.1	10.4	26.0	10.9	26.7	11.3	21	11.8
130	-	-		27.8	11.2	27.6	Perfection or named	27.4	
	100	Dep		Dep.		Dep	i,at.	Dep.	Lat
1	11	1.9 1	Jeg. 1	081	jeg.	671	Jeg.	60 1	Jeg

_				
15	21 Deg.	22 Deg.	1 23 Deg.	24. Deg.
7.7	Lat. Dep	Lat. Dep	Lat. Dep.	Lat. Dep.
31	28.9[11.1	28.7[11.0	28.5,12.1	28.3 12.6
32		29.7 12.0	29.5 12.5	29.2 13.0
33	11- 1	30.6 12.4	30.4 12.9	30.1 13.4
34	11- 1	31.5 12.7	31.3 13.3	31.1 13.8
35	32.7 12.5	32.4 13.1	32.2 13.7	32.0 14.2
36	33.5 12.9	33.2 13.5	33.114.1	32.9 14.7
37	34.5 13.3	34.113.9	34.1 14.4	33.8 15.1
38	35.5 13.6	35.0 14.2	35.0 14 8	34.7 15.5
39	36.4 14.0	36.914.6	35.915.2	35.6 15.9
40				36.5 16.3
41	38.3 14.7 39.2 15.1	38.015.3	37.7 10.0	37.5 16.7
12	40.115.4	39.9.16.1	39.6 16.8	38.4 17.1
44	41.115.8	40.8:16.5	40.5 17.2	40.2 17.9
45	42.016.1	41.7 16.8	41.417.6	41.118.3
46	42.9 16.5	42.6,17.2	42.3 18.0	42.C 18.7
1-7	43.9 16.7	43.6 17.6	43.3 18.4	42.0 19.1.
18	44.8 17.1	44.5 180	44.2 18.8	43.8 19.5
19	15.717.5	45.4 18.3	45.1 19.2	44.7 19.9
50	+6.717.9	46.4 18.7	46.0 9.5	45.5 20.3
51	17.6,18.3	47.3 19.1	46.9 19.9	4.6.t 20.7
;2	48.5 18.6	48.219.4	47.920.3	47.5 21.1
53	19.5 19.0	49.1 19.8	48.8 20.7	49.2 22.0
54	50.4 19.3	50.1 20.2	50.6 21.5	50.2 22.4
55	52.3 20.1		51.5 21.0	51.2 22.8
57	3.2.20.4	51.921.0	52.5 22.3	52.1 23.2
.:8	54.1 20.8	53.8.21.7	53.4 22.7	53.0 23.6
50	55.121.1	54.7 22.1	54.3 23.6	53.6 24.0
٥٥	16.021.5	55.622.5	55.2 23.4	54.8 :4.4
	Dep. Lat.	Dep. Lat.	Dep. Lat	Dep. Lat.
	69 Deg.	68 Deg.	67 Deg.	66 Deg.
-				

13	1 25 Deg.	1 26 Deg.	27 Deg.	1 28 Deg.
1.7	Lat. Dep.	Lat. Dep.	Lat. Dep.	Lat. Dep
1	0.(0.4			
2	1.5 0.8	1.8 0.9	1 8 0.0	1.8 0.0
	11 6			
3	2.7 1.3	2.7 1.3	2.7 I.4 3.6 I.8	
4	3.6 1.7	3.6 1.7		3.5 1.9
5	4.5 2.1	4.5 2.2	4.5 2.3	4.4 2.3
6	5.4 2.5	5.4 2.6	5.3 2.7	5.3 2.8
7 8	6.3 3.0	6.3 3.1	6.2 3.2	6.2 3.3
	7.2 3.4	7.2 3.5	7.1 3.6	7-1 3.8
9	8.2 3.8	8.1 3.9	8.0 4.1	7.9 4.2
10	9.1 4.2	9.0 4.4	8.9 4.5	8.8 4.7
11.	10.0 4.6	9.9 4.8	9.8 5.0	9.7 5.2
12	10.9 5.1	10.8 5.3	10.7 5.4	10.6 5.6
13	11.8 5.5	11.7 5.7	11.6 5.8	11.5 6.1
14	12.7 5.9	12.6 6.1	12.5 6.2	12.4 6.6
15	13.6 6.3	13.5 6.6	13.4 6.8	13.2 7.0
16	14.5 6.8	14.4 7.0	14.3 7.3	14.1 7.5
17	15.4 7.2	15.3 7.4	15.1 7.7	150 8.0
18	16.3 7.6	16.2 7.9	16.0 8.2	15.9 8.4
119	17.2 8.0	17.1 8.3	16.9 8.6	16.8 8.9
20	18.1 8.4	18.0 8.8	17.8 9.1	17.7 9.4
21	190 8.9	18.9 9.2	18.7; 9.5	18.5 9.9
32	19.9 9.3	19.8 9.7	19.6,10.0	19.4 10.2
23	20.8 9.7	20.7,10.1	20.5 10.4	20.3 10.8
24	21.7 10.1	21.6 10.5	21.4 10.9	21,211.3
25	22.7 10.6	22.511.0	22.3.11.3	22.111.7
31.	23.611.0	23.4,11.4	23.211.8	23 0 12.2
27	24.511.4	24.3 11.8	24 1 12 3	23.8127
28	25.411.8	25.2,12.3	24.9 12.7	24.7 13.1
29	26.312.3	26.1 12.7	25.8113.2	25.613.6
30	27.2 12.7	27.0 13.1	26.7,13.6	26.5 14.1
	Dep. Lat.	Der. Lat.	Dep. Lat.	Dep. Lat
	65 Deg.	64 Deg.	63 Deg.	62 Deg.
-	of Deg.	Ot Defe	oy Deg.	oz Deg.

			-	
DI	25 Deg. 1	26 Deg.	27 Deg.	28 Deg.
÷.	Lat. Dep	Lat. Hep.	Lat. Dep.	Lat. Dep.
31	28.1 13.1	27.9;13.6	27.114.1	27.4 14.5
32	29.013.5	28.8 14.0	28.5:4.5	28.2 15.0
33	29.9.139	29.7 14.4	29.4 14.9	29.1 15.5
34	30.8 14.4	30.6 14.9	30.215.4	30.0 16.0
35	31.7 14.8	31.5 15.3	31.215.9	20.9 16.4
36	32.6 15.2	32.4 15.8	32.1 10.3	31.8 16.9
37	33.5 15.6	33.2 16.2	33.016.8	32.7 17.4
38	34.4 16.0	34.1 16.6	33.9 17.2	33.5 17.0
39	35.3 16.5	35.017.1	34.7 7.7	34.4 18.4
40	36.2 16.9	35.9!17.5	35.6 18.2	35.3 18.8
41	37.2 17.3	36.8 18.0	36.5 18.6	35.2 19.2
42	38.1 17.7	37.718.4	37.4 19.1	37-1 19-7
43	39.0 18.2	38.6 18.8	38.319.5	38.6 20.6
44	39.918.6	39.5 19.3	39.2 20.0	
45	40.8 19 0	40.4 19.7	40.1 20.4	3//
46	41.719.4	41.3 20.2	41.020.9	40.6 21.6
47	42.6 19.9	42.2 20.6	41.921.3	41.5 22.1
48	43.5 20.3	43.1 21.0	42.8 21.8	43.3/23.1
49	44.420.7	44.0 21.5	43.7 22.2	44.1 23.5
50	45.3 21.1	44.9 21.9		
51	46.221.5	45.8 22.3	45.4 23.2	45.0 23.9
52	47.1 22.0	46.7 22.8	46.3 23.6	46.8 24.9
53	48.0 22.4	47.6 23.2	48.1 24.5	47.7 25.3
54	48.9 22.8	49.4 24.1	49.025.0	48.6 25.8
55			49.9 25.4	49.4 20.3
55	50.7 23.7	50.3 24.5	50.8:25.9	50.3 26.8
57 58	51.7 24.1	52.1 25.4	51.7 26.3	51.2 27.2
	53.5,24.9	53.0 25.5	52.6 26.8	52.1 27.7
59	54.4 25.4	53.9 26.3	53.5 27.2	53.0 8.2
	Dep. Lat.	Dep. Lat	Dep. Lat.	Dep Lic.
		64 Deg.	63 Deg.	62 Deg.
-	ος Deg.	104 Deg.	103 2008. 1	8

		-				
13	29 Deg. 1	:0 Deg. 1	31 Deg.	3? Deg.		
-	at Dep	Lac. Dep.	[a. D.p.]	Lat. Dep		
1	0.00.5	0 (1 0.5	0.91 0.5	0.81 0 5		
2	1.7 1.0	1.7 1.0	1.7 1.0	1.7 1.1		
3	2.(1.4	2.6 1.5	2.6 1.5	25 1.6		
+	3.5 1.0	3.5 2.0	3.4 2.1	3.4 2.1		
1	4 4 2 4	4.3 2.5	4.3 2.6	4.2 2.6		
0.	5.2 2.9	5.2 3.0	5.2 3.1	5.1 3.2		
7	6.1 3.4	6.1 3.5	6.1 36	5.9 3.7		
8	7.0 3.9	6.9 4.0	6.9 4.1	6.8 4.2		
9	7.9 4.4	7.8 4.5	7.7 4.6	76 4.8		
1.0	8.7 4 8	8.7 5.0	8.6 5.1	8.5 5.3		
1.	9.t 5.3	9.5 5 5	9.4 5.7	9.3 5.8		
: 2	10.5 5.8	10.1 6.0	10.3 6.2	10.2 6.4		
13	11.4 6.3	11.3 0.5	11.1 6.7	11.0 6.9		
14	12.2 6.3	12.1 7.0	120, 7.2	11.9 7.4		
15	12.1 7.3	13.0 7.5	13.9 7.7	12.7 7.9		
100	1 14.C 7.7	19 8.0	13.7, 8.	13.6 8.5		
7	11.0 8.2	14.7 8:5	14.6 8.8	14-4 9.0		
. 18		15.6 9.0	15.4 9.3	15.3 9.5		
1 .		16.5 9.5	16.3 9.8	16.110.1		
2 C	1 5 9.7	17.4 14.0	17.110.3	17.0106		
21	18.4 10.2	18.2 10.5	18.0,10.8	17.811.1		
2.2	11.7	19.011.0	18.911.3	18.6 11.7		
2.2		19.911.5	19.7,11.8	19.5 12.2		
		20.8 12.0	20.6 12.4	20.3 12.7		
3 5		21.6 12.5	21.412.9	21.2 13.2		
2(1	22.5 13.0	22.3.13.4	22.013.8		
27		23.4 13.5	23.1 13.9	22.914.3		
28	1 1 1	24.2 14.0	24.0,14.4	23.714.8		
20		25.114.5	24.9 14.9	24.(15.4)		
30		26.015.0	25.715.4	Name of Street Orange Street		
	Dep. Lat.	Dep. Lat.	Dep lant.	Dep. List.		
	U Deg.	no D.g	1 59 L1 g.	58 Deg.		
-						

461				
151 2	9 Deg.	30 Deg.	31 Deg.	32 Deg.
1 1 L	at. Dep.	Lat. Dep	Lat. Dep.	Lat. Dep
31 27 28 33 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	at. Dep. 17. 15.0 15.0 15.0 15.5 16.0 15.5 16.5 17.0 16.5 17.0 16.5 17.4 17.9 18.4 17.9 18.9 18.9 18.9 18.9 18.9 18.9 18.9 18	20.8 15.5 27.7 16.0 28.6 16.5 29.5 17.0 30.3 17.5 31.2 18.0 32.0 18.5 32.9 19.0 33.8 19.5 34.6 20.0 35.5 20.5 36.4 21.0 37.2 21.5 38.1 22.0 39.0 22.5 39.8 23.0 40.7 23.5 41.6 24.0 42.4 24.5 43.3 25.0 44.2 25.5 45.0 26.0 45.9 26.5 46.8 27.0 47.6 27.5 48.5 28.0 49.4 28.5 50.2 29.0 51.1 29.5 52.0 30.0	26.(10.0) 27.4 16.5 28.3 17.0 29.3 17.5 30.6 18.0 30.6 .8.5 31. 9.1 32.6 9.6 33.2 20.1 34.3 10.6 35.1 21.1 36.6 21.6 36.6 22.1 37.7 22.6 38.6 23.7 40. 24.2 41.1 24.7 42.6 25.2 42.9 25.7 43.7 26.3 44.6 26.8 45.4 27.3 46.1 27.8 47.1 28.3 48.6 28.8 48.1 29.4 49.7 29.9 50.6 10.4 51. 0.0	20.3 10.4 27.1 17.C 28.C 17.5 28.6 18.C 29.7 18.5 30.5 19.1 31.4 19.0 32.2 20.1 33.1 20.7 33.6 21.2 34.8 21.7 35.6 22.8 37.5 23.8 39.5 24.4 39.5 24.4 39.5 24.4 39.5 24.4 41.5 26.5 43.2 27.0 44.1 27.6 44.9 28.1 45.8 28.6 46.6 29.1 47.5 29.7 48.1 30.2 49.1 30.7 50.6 31.3 50.6 31.8 Dep Lat
	61 Deg.	60 Deg.	1 59 Deg.	1 49 ries

	Dog	At Dog	At Dep 6	Dan
15 33	-	34 Deg.	35 Deg.	36 Deg.
		Lit. Dep.	Lat. [Dep.]	Lat. Dep.
1 1	.8 0.5	0 8 0.6	0.8, 0.6	0.8 0.6
	.7 1.1	1.7 1.1	1.6 1.1	1.6 1.2
1 - 13	.5 1.6	2.5 1.7	2.5 1.7	2.4 1.8
	.4 2.2	3.3 2.2	3.3 2.3	3.2 2.3
1	3 27	4.1 2.8	4.1 2.9	4.C 2.9
	.0 3.3	5.0, 3.4	4.9, 3.4	4.8 3.5
	.9 3.8	5.8 3.9	5.7 4.0	5.7 4.3
	7 4.4	6.6 4.5	6.5 4.6	6.5 4.7
9 7	.5 4.9	7.5 5.0 8.3 5.6	7.4 5 2 8.2 5.7	7.3 5-3 8.1 5.9
	3.4 5 4		1	
	9.2 0.0	9.1 6.1	9.0, 6.3	8.9 6.5
	0.1 6.5	9.9 6.7	9.8 6.9	9.7 7.9
1 13	7.1	10.8 7.3	10.6 7.5	10.5 7.6
	7.7 7.6 2.6 8.2	11.6 7.8	11.5 8.0	11.3 8.2
	3.4 8.7	13.3 8.9	13.1 9.2	12.9 9.4
	4.3 9.3	14.1 9.5	13.9 9.8	13.7[10.0]
		14.9,10.1	14.7.10.3	14.610.6
	6.8 10.9	15.710.0	15.6 10.9	15.411.2
			16.4 11.5	
	7.6.11.4	17.411.7	17.2 12.0	17.012.3
	8.5 12.0	18.2112.3	18.012.6	17.8 12.9
	9.3.12.5	19.0 12.8	18.8 13.2	18.6 13.5
	1.013.6	19.9,13.4	19.7 13.8	19.4 14.1
-				
	1.814.2	21.5114.5	21.3 14.9	21.015.3
	2.6 14.7	22.4 15.1	1 1 2 2	21.8 15.9
	3.5 15.2	23.2,15.6	22.9 16 1	23.5 17.0
	5.2 16.3	24.0.16.8	24.6 17.2	24.317.6
	Dep. Lat.	-	-	Dep. Lat.
		Der hat	Dep. Lat.	-
	57 Deg.	50 Deg.	55 Deg.	54 Deg.

-				
15	33 Deg.	34 Deg.	1 35 Deg	
- 1.7	Lat. Dep.		1	30 Deg.
-		Lat. L	Lat Dep	Lat Den.
31		125 7 17.3	25.4 17.8	
32	1 1 1 1	26.5 17.9	26.2 18.3	25.1 18.2
33	1 1	27.4 18.4	27.0 18.9	1 7
34	, , , , ,	28.219.0	27.5 19.5	26 7 19.4
30	29.419.1	29.0196	28.7 20.1	27.5 20.0
36	30.219.6	29.8 20.1		28.3 20.6
37			29.5 20.6	29.1 21.2
3.8		30.7 20.7	30.3 21.2	29.9 21.7
39	1 2 / 1	31.521.2	37.1 21.8	30.7 22.3
4.0		32.321.8	32.0 22.3	31.5 22.0
tions.	CONTRACTOR OF THE PARTY NAMED IN	33.2 22.4	32.8 22.9	32.723.5
41	1 0 1 1	34.0 22.9	33.6 23.5	33.224.1
42		34.8 23.5	34.4 24.1	34.0 24.7
43	1 3 - 3 - 4	35.6 24.0	35.2 24.6	34.8 25.3
44	1 2 7 7	36.5 24.6	36.c 25.2	35.625.9
45	1 2/1/17/19	37.3 25.2	36.025.8	36.4 26.4
46	38.6 25.0	38.1 25.7	37.7 26.4	The same of the sa
47	39.4 25.6	39 0 26.3	38.5 27.0	37.227.0
48	40.2 25.1	39.8,26.8	39.2 27.6	38 0 27.6
49	41.1 26.7	40.6 27.4	40.1 28.2	38.8 28.2 39.6 28.8
50	41.927.2	41.428.0	41.0 28.8	40.4 29.4
51		42.3 28.5		Andrew Street, or other Designation.
52		43.1,29.1	41.8 29 2	41-3 30.0
53	44.5 28.9	43.929.6	43.430.4	12.1,0.(
54	45.329.4	44 7 30.2	44.2 31.0	42.931.2
55	46 1 30.0	45.630.7	45.131.5	43.731.7
56		46.431.3		44.5 32 3
57	47.831.0	47.331.9	45.9 32.1	45.3 32.0
58	48.731.6	48.1 32.4	46.7 32.7	46.1 33.4
159	49.5 32.1	48.9 33.0	47.5 33.3	46.9 34.
16c	150.3132.7	49.7 33.5	48.3 33.8	47.7,34.7
	Dep. Lat.			48.5 35.2
		Dep. Lat.	Lep Lat	Dep. Lat
-	57 Deg. 1	56 Deg.	55 Deg.	54 Deg.

151	37 D.g.	38 Deg	39 Deg.	40 1 eg.
Dic	Lat. Dep	Lit.D p	at. Dep.	Lat. Dep.
-	0.81 0.0	0.8 0.6	0.81 0.7	0.8 0.6
	1:6 1.2	1.6 1.2	1.4 1.3	1.5 1.3
2	2.4 1.8	2.4 1.8	2.3 1.9	2.3 1.9
2	3.2 2.4	3.1 2.5	3.1 2.5	3.1 2.6
3	4.0 3.0	3.9 3.1	3.5 3.1	3.8 3.2
(4.8 3.0	4.7 3.7	4.6 3.8	4.6 3.9
7	5.6 4.2	5.5 4.3	5.4 4.4	5.4 4.5
	6.4 4.8 7.2 5.4	6.3 4.9	6.2 5.0	6.1 5.1
10	8.0 6.0	7.1 5.5	7.5 5.7	6.9 5.8 7.7 6.4
1 :	5.8 0.6	8.7 6.8	8.5 6.9	8.4 7.1
1	9.6 7.2	9.4 7.4		9.2 7.7
I	10.4 7.8	10.2 8.0	9.3 7.5	10.0 8.4
1.	11.2 8.4	1.0 8.6	10.0 8.8	10.7 9.0
1:	12.0 9.0	11.8 9.2	11.(9.4	11.5 9.6
it	12.8 9.0	12.6 9.8	12.4 10.1	12.3 10.2
17	13.010.2	13.4 10.5	13.2 .0.7	13.010.5
IE	14.4 10.	I 4.2 I I.1	13.(11.3)	13.8 11.6
20	15.211.4	15.8123	14.12.0	14.5 12 2
-				15.3 12.9
21	17.613.4	16.5 12.6	16.2 13.2	16.1 13.5
22	18.413.8	17.3 13.5	17.113.8	16.8 14.1
24	19.2 14.4	18.914.8	18. 15.1	18.415.4
25	20.6.15.0	19.7'15.4	19. 15.7	19.116.1
2(20.8 15.0	20.5 10.0	20.: 6.4	19.916
27	21.6 16.2	21.316.(21.(17.0)	20.713
28	22.4 16.5	32.117.2	21.8 17.6	21.4 15.0
25	23.2 17.4	22.8 17.	22. 8.3	22.2 18.6
3°	24.0 18.0	23.618.	23.5 18.9	23.019.1
	Dep Lat	Dep. Lai	Dep. Lat.	Dep. Lar
1	53 Deg.	52 Deg.	51 Deg.	50 Deg.
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1.	Lat. Dep.	Lat. Dep	Lat. Dep Lat. De	er.
31	24. 118.0	24.119.1	24.1/19.5 23 7/19	0.9
32	25.(19.3	25.2197	24.9 20.1 21.5 20	
33	25.2 19.9	26.0 20.3	25.6 20.8 25.3 21	. 2
34	27.1 20.5	26.8 20.9	26.121.4 20.021	.9
35	27.6 21.1	27.(21.5	27.2 22.0 26.8 22	.5
36	28 ; 21.7	28.4 22.2	28.0 22.7 27 6 23	. I
37	29.5 22.3	29 2 22.8	28.8 23.3 28.3 23	
38	30. 22.9	29.9 23.4	29.5 23.9 29.1 24	
39	31.1 13.5	30.7 24.0	30.3 24.5 29.6 25.	. 1
40	31.6 4.1	31.5 24.6	31 1 25.2 30.6 25.	.7
+1	32.7 4.7	32.3 25.2	31.9 25.8 31.4 20.	
42	33.5.5.3	33.1 :5 9	32.6 20.4 32.2 27.	- 1
143	34.25.5	33 5 26.5	33.427.1 32.927.	6
44	35.1136.5	34.7 27.1	34.2 27.7 33.7 28.	3
45	35 6 27.1	35.: 27	35.0 28.3 34.5 28.	91
46	30. 77	36.2 28.3	35-7129.0 35 2 29.	U
47	37. [:8.]	37 C 28.9	36.5 29.6 36.6 30.	2
4.8	38 3 .8.9	37.8 2 7.5	37.3 30.2 36.8 30.	9
49	39. 29.5	38 (0.2	38.130.8 37.531.	5
50	3', 30.1	30. 10.8	38.9 31 5 38 3 32.	1
151	40.7 10.7	40.231.	39.0 32.1 39.1 32.	81
52	41. 31.3	41 C 32.0	40.432.7 39.833.	4
53	42. ;1.9	41.8 32.6	41.2 33.3 40.6 34.	I
54	42. 32.5	42.5 3.2	12.0 34.0 41.4 34.	
55	43.0 13.1	13.3 33.9	42.7 34.6 42 1 35.	- [
55	44.7 3.7	44.1 34.5	43.5 35.2 42.9 36.0	
57	45.1.4.3	44 5 15 1	44.3 35.9 43. 36.0	_
58	46 3 4.9	45 7 35.7	45 1 35.5 44.4 37.3	-
59	47.1 35.5	40.5 jt.3	45.8 37.1 45.2 37.9	
60	47-116.1	17-31:6.9	46.(37.8 46.0 38.0	
	Dep. Lat.	Dep. Lat.	Dep. Lat. Dep. Lar	
	53 Deg	52 Deg.	51 Deg. 11.50 Deg.	1
No.				

an I	Dec.	La Dan	La Dea I	L L Dec
Dia.	41 Deg.	42 Deg.	43 Deg.	44 Deg.
-	Lat. Dep.	Lat Dep.	Lat. Des	Lat. Dep.
1	0.71 0.7	0.7 07	0.7 0.7	0.7 0.7
2	1.5 1.3	1.5 1.3	1.5 1.4	1.4 1.4
3	2.3 2.0	2.2 2.0	2.2 2.0	2.2 2.1
4	3.0 2.6	3.0 2.7	2.9 2.7	2.9 2.8
5	3.8 3.3	3.7 3.3	3.7 3.4	3.6 3 5
6	4.5 3.9	4.5 4.0	4.4 4.1	4.3 4.2
7	5.3 4.6	5.2 4.7	5.1 4.8	5.0 4.9
8	6.0 5.2	5.9 5.3	5.8 5.5	5.7 5.6
9	6.8 5.9	6.7 6.0	6.6 6.1	6.5 6.2
10	7-5! 6.6	7.4 6.7	7.3 6.8	7.2 6.9
11	8.3! 7.2	8.2 7.4	8.01 7.5	7.9 7.6
12	9.1 7.9	8.9 8.0	8.8 8.2	8.6 8.3
13	9.8 8.5	9.7 8.7	9.5 8.9	9.3 9.0
14	10.6 9.1	10.4 9.4	10.2 9.5	10.1 9.7
15	11.3 9.8	11.110.0	11.010.2	10.8 10.4
16	12.1 10.5	11.9,10.7	11.710.9	11.5,11.1
17	12.8 11.1	12.6 11.4	12.411.6	12.2 11.8
18	13.6,11.8	13.412.0	13.212.3	12.9 125
19	14 3,12,5	14.112.7	13.9,13.0	13.713 2
20	15.1 13.1	14.9 13.4	14.613.6	14.413.9
11	15.8,13.8	15.6 14.0	15.4 14.3	15.1 14.0
12	16.6,14.4	16.3 14.7	16 1 15.0	15.8 15.3
23	17.415.1	17.115.4	16.8,15.7	16.5 16.0
24	18.1,15.7	17.816.1	17.5 16.4	17.3 16.7
25	18 9 16.4	186167	18.3.17.1	18.0.17.4
26	19.6,17.1	19.317.4	19.0 17.7	18.7 18.1
27	20.4 17.7	20.1 18.1	19.7 18.4	19.4 18.8
28	21.1 18.4	20.8 18.7	20.5 19.1	20.119.4
29	21.919.0	21.5 19.4	21.219.8	20.9 20.1
30	22.6/19.7	22.3 20.1	21.9 20.5	21.6 20.8
	Dep. Lat.	Dep. Lat.	Dep. Lat.	Dep. Lat.
1	49 Deg.	48 Deg.	47 Deg.	46 Deg.
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Dift.	41 Deg.	42 Deg. 1	12 1100 1	A A Bearing
1.71		1	4, 200	44 Deg.
	Lat. Dep.	Lat. Dep.	Lat. Dep.	Lat. Dep.
31	23.4 20.3	23.0 20.7	22.0,21.1	22.3 21.5
32	24.1 21.0	23.8 21.4	23.4 21.8	23.022.2
33	24.921.7	24.5 22.1	24.1 22.5	23.7 22.9
34	25.6 22.3	25.3 22.7	24.9 23.2	24.5 23.6
35	26.4 23.0	26.0 23.4	25.623.9	25.2 24.3
36	27.2 23.6	26.7,24.1	26.324.5	25.9 25.0
37	27.9 24.3	27.5 24.7	27.0,25.2	26.6 26.7
38	28.7 24.9	28.225.4	27.8 25.9	27.3 26.4
39	29.4 25.6	29.026.1	28.5 26.6	28.0 27.1
40	30.2 26.2	29.7 26.8	29.2,27.3	28.8 27.8
41	31.0,26.9	30.5,27.4	30.0 28.0	29.5 28.5
42	31.7 27.5	21.228.1	30.7 28.6	30.2 29.2
43	32.5 28.2	31.9 28.8	31.429.3	30.929.9
144	33.2 28.9	32.7,29.4	32.2 30.0	31.6,30.6
45	34.0 29.5	33.4'30.1	32.9 30.7	32.3 31.3
46	34.7 30.2	34.2 30.8	33.6 31.4	33.132.0
47	35.5 30.8	34.9 31.4	34.4 32.1	33.8 32.6
48	36.331.5	1 35. / . 3 4. 1	35.1 32.7	34.5 33.3
49	37.0 32.1	36.4 32.8	35.133.4	35.2 34.0
50	37.7 32.8	37.233.5	30.634.1	
51	38.5 33.5	37.9,34.1	37.334.8	36.7 35.4
52	39.234.1	38.6,34.8	38.035.5	37.4 36.1
53	40.0'34.8	39.435.5	38.8 36.1	38.136.8
54	40.835.4	40.1 36.1	39.5 36.8	39.6 38.2
55	41.5 36.0		40.2 37.5	Personal Property and
56	42.3 36.7	41.6 37.5	41.0 38.2	40.3 38.9
57	43.0.37.4	42.438.1	41.7 38.9	41.0 39.6
58	43.838.1	43.1 38.8	42.4 39.5	41.740.3
59	44.5 38.7	43.8 39.5	43.8 40.9	43.241.7
-	45.3139.4	-		Dep. Lat.
	Dep. Lat.	Dep. Lat.	Dep. Lat.	-
	40 Deg.	48 Deg. 1	47 Deg. 1	1 46 Deg.

		,	1	Dag I
101	1 45 Deg. 1		Dift	45 Deg
13	Lat Dep.			Lat. Dep.
I	0.71 0.7		; 1	21.921.9
2	1.4 1.4		;2	22.6 22.6
3	2.1 2.1		33	23.3 23.3
4	2.8 2.8		34	24.0,24.0
	3.5 3.5		35	24.7 24.7
5	4 2 4.2		30	25.445.4
3 1	4.9 4.9		37	26.1 26.1
7 8	5.7 5.7		38	26.9 26.9
9	6.4 6,4		39	27.627.6
10	7.1 7.1		40	28.3 28.3
11	7.8 7.8		‡ I	29.029.0
12	8.5 8.5		12	29.729.7
13	9.2 9.2		+3	30 4 30.4
14	99 9.9		14	31.131.1
15	10.6 10,6		15	31.831.8
16	11 3 11.3		45	32.5,32.5
17	12.0 12.0		47	33 233.2
18	112.7 127			33.933.9
19	13.4 3.4		49	34.034.0
20	14.114.1		50	35.335.3
21	14.8,14.8		51	36.136.1
3.2	15.5,15.5		52	36.836.8
23	15.3 6.3		53	37.5 37.5
24	17.017.		54	38.238.2
25	17.717		55	The same of the sa
36	18.418 4		156	39.039.6
27	19.1 9.1		57	40.3 40.3
28	19.819.8		58	41.041.0
'9	20.5 20.5		159 160	41.741.7
30	21.231.1		OC	42.442.4
	Dep. Lat			Dep. Lat.
	11 45 Des.	1	-	1 45 Deg.
-	A STATE OF THE PARTY OF THE PAR			

TABLE

OF

MERIDIONAL PARTS.

To find the Meridional Parts for any Latitude; and the contrary.

RULE.

Seek the Degrees at the Head of the Table; and the Minutes on the left Hand Side. And in the Angle of meeting you have the Meridional Parts required.

EXAMPLE.

To find the M. P. for 42°: 38'. In the Column 42, and over-against 38 is 2833, the Merid. Parts of 42°: 38'.

Again, to find the M. P. for 73°: 25'. In the Column 73, and over against 24,26, you have 6617, 6624; and the Mean is 6620, the Merid. Parts fought.

And if the M. P. be given to find the Degrees and Minutes answering. Find the nearest Number in the Table, and you have the Degrees at Top, and the Minutes on the Side of the Table.

Thus, the M. P. being 2833, the Degrees and Minutes answering is 42°: 38. And if the M. P. be 6620, the Degrees belonging thereto will be found 73°: 25'.

2 2 62 122 182 242 302 363 4 4 64 124 184 244 304 365 6 6 6 6 126 186 246 306 367 8 8 68 128 188 248 308 369 367 361 369 369 361 361 361 361 361 361 372 372 372	Degrees of Latitude.							
2 2 62 122 182 242 302 363 4 6 6 6 6 6 126 186 246 306 367 8 8 8 68 128 188 248 308 369 10 10 70 130 190 250 310 371 112 12 72 132 192 252 312 373 14 14 74 134 194 254 314 375 16 16 76 136 196 256 316 377 18 18 78 138 198 258 318 379 16 16 76 136 196 256 316 377 18 18 78 138 198 258 318 379 17 18 18 78 138 198 258 318 379 17 18 18 78 138 198 258 318 379 18 18 22 22 82 142 202 262 322 383 18 22 24 24 84 144 204 264 324 385 12 22 28 88 148 208 268 328 389 30 30 90 150 210 270 330 391 18 36 36 96 156 216 276 336 397 18 36 36 96 156 216 276 336 397 18 36 36 96 156 216 276 336 397 18 38 38 98 158 218 278 338 399 18 28 28 28 28 28 28 28 28 28 28 28 28 28	7							
4 4 64 124 184 244 304 365 6 6 6 6 6 126 186 246 306 367 8 8 8 68 128 188 248 308 369 10 10 10 70 130 190 250 310 371 12 12 72 132 192 252 312 373 14 14 74 134 194 254 314 375 16 16 76 136 196 256 316 377 18 18 78 138 198 258 318 379 20 20 80 140 200 260 320 381 22 22 2 82 142 202 202 322 383 22 24 24 84 144 204 264 324 385 28 88 148 208 268 328 389 23 30 30 90 150 210 270 330 391 32 32 32 383 30 30 90 150 210 270 330 391 33 33 39 34 34 34 54 154 214 274 334 395 336 36 96 156 216 276 336 397 34 34 34 54 154 214 274 334 395 336 36 96 156 216 276 336 397 34 34 34 54 154 214 274 334 395 336 36 96 156 216 276 336 397 34 34 34 54 154 214 274 334 395 336 36 96 156 216 276 336 397 34 34 34 54 154 214 274 334 395 34 36 36 96 156 216 276 336 397 34 34 34 40 100 160 220 280 340 401 24 242 10 162 222 282 342 403 24 444 104 164 224 284 344 405 44	421							
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14 14 74 134 194 254 314 375 4 16 76 136 196 256 316 377 4 18 78 138 198 258 318 379 20 20 80 140 200 260 320 381 383 22 22 22 322 383 32 322 383 32 324 385 32 324 385 32 324 385	431							
16 16 76 136 196 256 316 377 18 18 78 138 198 258 318 379 20 20 80 140 200 260 320 381 22 22 82 142 202 262 322 383 24 24 84 144 204 264 324 385 26 26 86 146 206 266 326 387 28 28 88 148 208 268 328 389 30 30 90 150 210 270 330 391 32 32 92 152 212 272 332 393 34 34 94 154 214 274 334 395 36 36 96 156 216 276 335 397 404 40 40 100 160 220 280 340 401 424 42 10- 162 222 282 342 403 444 44 44 104 164 22	433							
18 18 78 138 198 258 318 379 20 20 80 140 200 260 320 381 22 22 82 142 202 262 322 383 24 24 84 144 204 264 324 385 26 26 86 146 206 266 326 387 28 28 88 148 208 268 328 389 30 30 90 150 210 270 330 391 32 32 92 152 212 272 332 393 34 34 94 154 214 274 334 395 36 36 96 156 216 276 335 397 40 40 100 160 220 280 340 401 42 42 10- 162 222 282 342 403 44 44 104 164 224 284 344 405	435							
20 20 86 140 200 260 320 381 22 22 82 142 202 262 322 383 24 24 84 144 204 264 324 385 26 26 86 146 206 266 326 387 28 28 88 148 208 268 328 389 30 30 90 150 210 270 330 391 32 32 92 152 212 272 332 393 34 34 94 154 214 274 334 395 36 36 96 156 216 276 335 397 40 40 100 160 220 280 340 401 42 42 10 162 222 282 342 403 <t< td=""><td>437</td></t<>	437							
22 22 82 142 202 202 322 383 23 23 23 23 23 23 23 23 23 23 23 23 23	439 441							
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26 26 86 146 206 266 326 387 28 28 88 148 208 268 328 389 30 30 90 150 210 270 330 391 23 232 36 36 36 36 36 3	443 445							
28 28 88 148 208 268 328 389 4 30 30 90 150 210 270 330 301 4 32 32 92 152 212 272 332 393 4 34 34 4 40 100 160 220 280 340 401 4 4 4 4 104 164 224 284 344 405 4	447							
30 30 90 150 210 276 330 391 4 32 32 92 152 212 272 332 393 4 34 34 94 154 214 274 334 395 4 36 36 96 156 216 276 336 397 4 38 38 98 158 218 278 338 399 4 40 40 100 160 220 280 340 401 2 42 42 10 162 222 282 342 403 2 44 44 104 164 224 284 344 405 2	449							
34 34	451							
34 34 94 154 214 274 334 395 4 36 36 96 156 216 276 336 397 4 38 38 39 4 40 40 100 160 220 280 340 401 4 242 10 162 222 282 342 403 4 444 104 164 224 284 344 405 4	453							
38 3	455							
40 40 100 160 220 280 340 401 4 +2 +2 10	157							
42 42 10 162 222 282 342 403 2 44 44 104 164 224 284 344 405 2	459							
44 44 104 164 224 284 344 405	461							
	163							
140,40 100 100 220 280 340 407 2	1.65							
	167							
	169							
	171							
	173							
	175 177							
	179							
6060 120 180 240 300 361 421 4	181							

7 7	S. Degrees of Latitude.						
lin	8	2	-	-			
-	-	9	10	11	12	1.13	14
0	481	542	603	664	725	787	818
2	1 , 0	544	605	6.6	727	789	850
4		546	607	668	729	791	852
6	1	548	609	670	731	793	855
8	1 12-	550	611	672	733	795	857
IC	492	552	613	674	735	797	859
12	1 11	554	615	676	737	799	861
14		556	617	673	740	801	863
10	1	558	619	680	742	,803	865
18)	560	621	682	744	805	867
20	502	562	623	684	746	807	860
22	504	564	625	686	748	809	871
24		566	627	688	750	811	873
26	508	568	629	690	752	813	875
28	510	570	631	692	754	815	877
30	512	573	633	695	756	817	879
32	514	575	635	697	758	820	881
34	516	577	638	699	760	822	883
36 38	518	579	640	701	762	824	886
40	520	581	642	703	764	825	888
<u> </u>		583	644	705	766	828	89c
42	524	585	646	707	768	830	892
44	526	587	648	709	770	832	894
46 48	528	589	650	711	772	834	896
50	530	591	652	713	774	836	898
-		593	654	715	761		900
52	534	595	656	717	778	840	902
54 56	536	597	658	719	781	842	904
58	538 540	599	662	721	783	844	901
130	542	603	664	723	785	846	908
1	3441	003.	0041	7251	787	8481	91.

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lir				5 05	Latit	uae.	
-	15	16	17	18	19	20	21
С	910	97	1035	1098	1161	1225	1289
2	9121	975	1037	1100	1163	1227	1291
4	914	977	1039	1102	1166	1225	1293
6	917	979	1041	1104	1168	1231	1296
8	9191	981		,		1234	1298
10	021	983	1046	1100	1172	1236	1300
12	923	985	1048	IIII	, ,	1238	1 - 1
114	925	987	1050	1 "		1240	
116	927	-				1242	
18	929	991				1244	1 "
20	931	99				3 121t	1311
22	933	990	1 -			1248	1 1
24	935				3 1 1 8 7	1	
2(937	1000				1253	
35	1	1002		'	8119	1 1	
30	941	100.	1067	-	0119		-
3:		100:			2,119		
34		1008	071		,	7 1 26	1 -
36		1010	107	3 113		126	
3.8	950	1012	107		0120	2 I 266	
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4.	754	101		1	1	6 1 270	001
	56	1018	1	1 .		8 127	
11	958	1021					1 338
45	1 06 -	1022				2 1 27	
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50		1031					5 1 3 4 9
58		1033			9 122		1 22
,(1973	11077	109	0110	1 124	120	41354

13	31		Degrees of Latitude.	
1	3	22	23 24 25 26 27	28
-	0	1354	1419 1484 1550 1610 1684	1751
1	2	1356	.42111480 1552 1019 1086	1753
	4	1358	1423 1488 1554 1021 1008	1750
1	6	1360	1425 1491 1557 1623 1690 1427 1493 1559 1625 1692	1760
8	8	1364		1762
1-	2	1307		1765
	4	1	1112111400 15051103211099	1767
		1371	1142011201112001103411/01	1769
		1373	1438 1504 1570 1036 1704	1771
		1375		-
		1377	1442 1508 1574 1041 1768	1778
2	4	1379		1781
2	8	1284	1440 1515 1581 1648 1715	1783
3	0	1386	1451 1517 1583 1650 1717	
2	2.	1288	1453 1519 1585 1652 1719	
12	1	1300	1456:1521 1587 1054 1722	1790
			1458 1523 1590 1657 1724	
-		1395	1 / 1 Office of the Firm of	1 97
		130-		A reason to the last
		1399	1404 1530 1596 16 5 1731	1 1
H	4	1403	11269 1534 1001 1000 1.735	1803
14	18	1405	11471 1537 1003 1070 1/37	0.0
15	0	1408	1473 1539 1005 1072 1740	
5	2	1410	1475 1541 1607 1674 1742	1812
5	4	11112	114771543[1219[19//]1/44	10
5	1	1414	1480 1545 1612 1679 1747 1482 1548 1614 1681 1749	-
3	50	410	1484 1550 1616 1684 1751	1819
-	-	7.7		

				C 7	. 1		
S.		1)	egrees	of Lai	1!11de.		
-	29	30	31 1	3.2	33	34	35
Ĉ	1819	1888	1958	2028	2100	2171	2214
2	1822	1891	1960	2031	2102	2174	2247
4	1824	1893	1963	2033	2104	2176	2249
6	1826	1895	1965	203.5	2107	2179	2252
	1828	1898	1967	2038	2109	2181	2254
01	1831	1900	1970	2040	2111	2183	2256
12	1833	1902	1972	2042	2114	2180	2259
	1835	1904	1974	2045	2116	2188	2261
	1838	1907	1977	2047	2119	2191	2264
	1840	1909	1979	2050	2121	2193	2266
	1842	1911	1981	2052	2123	2196	2269
	1845	1914	1984	2054	2126	2198	2271
	1847	1916	1986	2057	2128	2200	2274
	1849	1918	1988	2059	2131	2203	2276
	1851	1921	1991	2061	2133	2205	2278
30	1854	1923	1993	2064	2135	2208	2281
132	1856	1925	1995	2066	2138	2210	2283
	1858	1928	1998	2069	2140	2213	2286
-	1861	1930	2000	2071	2143	2215	2288
	1863	1932	2002	2073	2145	2217	2291
40	1865	1935	2005	2076	2147	2220	2293
42		1937	2007	2078	2150	2222	2296
	1870	1939	2009	2080	2152	2225	2298
	1872	1942	2012	2083	2155	2227	2301
	1874		2014	2085	2157	2230	2303
50	1877	1946	2017	2088	2159	2232	,2206
	2 1879	1948	2019	2090	2162	2234	12308
	1881	1951	2021	2092	2164	2237	2311
-	6 1884	1 111	2024	2095	216-	2239	2313
	8 1880	1 / /	2026	2097	2169	2242	2315
160	011888	1958	12028	2100	2171	12244	2318

13		Di	egrees o	f Latin	ude.		
in	36	37	38			1 AI	1 42
0			-	39	40	-	42
1-		2393	2468	2545	2022	2702	2782
_	2320	2395	2471	2547	2625	2704	1784
	2323	2398	2473	2550	2628	2707	2787
	2325	2400	2476	2553	2630	2710	2790
	2328	2403	2478	2555	2633	2712	2792
10		2405	2481	2558	2636	2715	2795
12	1 223	2408	2483	2560	2638	2717	2798
	2335	2410	2485	2563	2641	2720	2801
	2338	2413	2489	2566	2644	2723	2803
	2340	2415	2491	2568	2646	2725	2806
-	2343	2418	2494	2571	2649	2728	2809
	2345	2420	2496	2573	2051	2731	2811
	2348	2423	2499	2575	2654	2733	2814
26	2350	2425	2501	2578	2657	2736	2817
28	23.53	2428	2504	2581	2659	2739	2820
30	2355	2430	2505	2584	2652	2741	2822
	2358	2433	2507	2586	2605	2744	282;
	2360	2435	2512	2589	2667	2747	2828
	2363	2438	2514	2591	2670	2749	2830
	2365	2440	2517	2594	2673	2752	2833
40	2368	2443	2519	2597	2675	2755	2836
142	2370	2445	2522	2599	2678	2758	2839
	2373	2448	2524	2602	2680	276c	2841
4.6	2375	2450	2527	2604	2683	2763	2844
48	2378	2453	2529	2607	2686	2765	184
50	2380	2456	2532	2610	2688	2768	284C
52	2383	2458	2535	2612	2691	2771	3852
	2385	2461	2537	2615	2694	2774	285-
156	2388	2463	2540	2617	2696	2776	2851
158	2390	2466	2542	2620	2699	2779	280C
160	2393	2468	2545	26221	2703	2782	2862

-			Degree	e of	atitu	do	
111		-		_	_		
-	.1 7	14	45	4.6	47	48	49
C	25	21)1.	3030	3116	3203	29 23	3382
2	25 11	34.79	3033	3118	3206	;295	3385
4	2869	2951	3036	3121	3209	3298	3388
6	2871	'953	3038	3124		3301	1391
8	287;	295	3041		3214	1304	3594
10	287	2059	3044	3130	3217	. 107	3397
I Z	2840	2902			3220	.310	3400
14			3050			3313	3403
16	2885		3053			3316	3407
18	2888			3142		3319	3410
20	289	-		3144		3322	2413
22	2893	2976	3061	3 · 47		3325	3416
24	~	2979	306;	3150	3238	3328	3419
26	1		3067			3331	3422
28	1		3070			3334	3425
-	2904		3073		3247	3337	:428
10	2907	2990	3075		3250	334C	3431
1	2910	2993	3078	3105	3253	3343	3434
1 -	2913	2990	3081	2171	3250	334C	3437
40	2915	2999	3084		3262	3349	3440
P0-	-	-			-	3352	3443
42			30,0			3355	3446
44	2924	2010	3095	3182	13271	3358	3449
6 "	2920	,013	3098	1180	3271	3364	3453 3456
50	2932	3016	3101	3188	3277	3367	3459
	-				3280	337¢	
52	2935		3104		3283	3373	3462
	294		3110		13286	3376	3468
1	2943		3113		3289		3471
	2946		3116				3475
-		-		J	4 /	55	717

21	<u></u>)egree	es of 1	atitu	de.	
Ain				-			56
-	50		52	53	54	55	
0	3475			3764			
2	3478	3572	3669	3758	3868	3972	4078
	3481	3575	3672	3771	3872	3975	4081
6	3484	3578	3675	3774	3875	3979	4085
8	3487	3582	3678	3777	2878	3982	4088
10	3490			3780			
12	3493	3588	3685	3784	3885	3989	4096
14	3496	3591	3688	4787	3889	3993	4100
16	3499	3594	3591	3791	3892	3990	4103
18	3503	3597	3095	3794	3895	4000	4100
20	3506	3600	3698	3797	3899	4003	4110
22	3509	3604	3701	3801	3902	4007	4114
24	3512	3607	3705	3804	3906	4010	4117
26	3515	3604 3607 3610	3708	3807	3909	4014	4121
28	3518	11014	17/44	R) or .	137-3	11/	11
130	3521	3017	3714	3814	13910	4021	4120
32	3525	3620	3718	3817	3920	4024	4132
134	13528	3 3623	3721	3821	13923	14028	14135
136	3531	1362t	3724	3824	13920	14031	14139
138	3 3 5 3 4	13630	13728	3827	13930	4035	14143
40	3537	7 3633	3731	3831	3933	403	4140
4	2 2545	3626	3734	13834	13937	404	2 4150
114	13543	3 3 5 3 9	3737	13838	13940	14040	74154
140	5 354	73043	13741	3841	13944	1404	9/415/
145	312550	0 2046	13744	113844	13947	1405	314101
5	355	3 3 6 4 9	3747	13848	3951	405	34104
	2/2001	12552	2751	12851	13954	400	04108
1	112 P C	A PAPP	オクファイ	112855	12616	1400	140/4
	ht2 FO	712350	12/5/	1,5056	1390	1400	117-13
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6	0 356	9/3665	13764	1386	13968	407	4141.8
A							

Post;	- ;	Dègrec.	e of I	atitudi		
È			60 1	61	62	60
P 5	58	59			-	63
0 4183	1294	4409	4527	4649	4775	4905
2 4185	4298	4413	4531	4654	4780	4910
44190	4302	4417	4535	5658	4784	4914
64194	4306	4421	4539	4662	4788	4919
8 4197	4310	4425	4543	4666	4792	4923
10,4201	4313	1429	4547	4670	4797	4927
124205	1317	4433	4551	4674	4801	4932
14 4209	4321	4137	4555	4678	4805	4936
16,4212	4325	4441	4559	4683	4810	4941
18 4216	4329	4444	4564	4687	4814	4945
20 4220	4332	4448	4568	4691	4818	4950
22 42 23	4336	4452	4572	4695	4822	4954
24 4227	4340	4456	4576.	4699	4827	4959
26,4231	4344	4160	4580	4704	4.831	4963
28 4235	1348	4464	4584	4708	4835	4967
30,4238	+352	-	1588	4712	4840	4972
324242	1355	4472	4592	4716	4844	4976
34, 246	1359	14476	4596	1720	4848	4981
3614249	4363	4480	4600	4724	4853	4985
384253	4371	4488	4608	4729 4733	4861	4990
42 4261					-	Manhall Adminis
4414264	4375	4492	4613	4737	4866	4999
46 1268	4382	4500	621	4746	1875	5003
48 4272	4386	4504	4625	4750	4879	5012
504276	4390	4508	4629	4754	4883	5017
524279	4394	4512	4633	4758	4808	5022
544283	4398	4516	4637	4763	1892	5026
56,4287	4402	14520	4601	4767	4896	5031
58 4291	4405	4523	4645	4771	4901	5035
104294	4409	14527	4649	4775	14905	5010

Degrees of Latitude. 5 64 65 66 67 68 0 5040 5179 5324 5474 563 2 5044 5184 5320 5480 563	5795 5966 7 5801 5971
0 5040 5179 5324 5474 563	5795 5966 7 5801 5971
	7 5801 5971
2 5044 528 4 8220 5.0-1-6	1 2 - 371
2 5044 5184 5329 5480 563	
45049 5189 5334 5485 564	2 5806 5977
6 5053 5193 5339 5490 564	7 5812 5982
8,5058 5198 5344 5495 565	3 5818 5980
10 5063 5203 5349 5500 565	8 5823 5995
12 5067 5208 5354 5505 566.	1 5829 : 6001
14,5072 5212 5359 5511 566	5834 6007
16 5076 5217 5364 5516 567	
18 5081 5222 5368 5521 5686	
20 5086 5227 5373 5526 568	5851 6025
22 5090 5232 5378 5531 5691	5857 6031
24 5095 5236 5383 5537 5696	5863 6037
26,5100 5241 5388 5542 5701	
28,5104 5240 5393 5547 5707	
30 5109 5251 5398 5552 5712	5880 6054
32,5114 5256 5403 5557 5718	5886 6060
34 5118 5261 5409 5563 5723	5891 6066
36 5123 5265 5414 5568 5729	5897 6072
38 5127 5270 5419 5573 5734	5903 6078
40 5132 5275 5424 5578 5740	15909 6084
42 51 37 5280 5429 5584 5745	5914 6091
44 5142 5285 5434 5589 5751	5919 6097
46 5146 5290 5439 5594 5756	5925 6103
48 5151 5295 5444 5599 5762	5931 6109
50 5156 5299 5449 5605 5767	5936 6115
52 5160 5304 5454 5610 5773	5942 6121
54,5165 5309 5459 5615 5778	5948 6127
56 5170 5314 5464 5621 15784	5954 6133
58 5174 5319 5469 5626 5790	5960 6139
60 5179 53.24 5474 5631 5795	5966 6146

-							
Z			Degre	es of i	Latitu	de	
1	71	72	73	74	75	76	77
0	6146	6335	6534	674t	9,50	410	7467
2	6152	5341	6541	6753	0978	7218	7476
4	6158	6348	0548	676c	398	7227	7484
6	6164	6354	5555	6768	1992	1235	493
8	6170	6361	0562	6775	7002 7010	7244	7502
12	618:	6374	6576	679c	7018	/2t I	7520
14	6189	6380	6583	0797	7026	7209	4529
10	6195	6387	6506	2020	7034	7278	7538
20	6207	5400	6602	6810	7042	~200	7540
21	6220	5412	6617	6824	7058 7066	7312	7500
26	6226	6420	621	6841	7074	7221	7584
28	0233	6426	6631	684c	7082	7320	7594
30	6.230	6432	6638	6846	7090	7338	7604
					7098		
34	6251	6446	6653	6871	7106	7355	7622
36	62;8	6453	6660	6875	7114	7364	7631
38	6264	646c	6667	6880	7122	7372	7641
					7130		
142	6277	6473	6681	6902	7138	739C	7660
114	6283	6480	6688	6900	7146	7398	7669
10	0290	0887	6695	6917	7154	74.07	7678
-0	6200	6500	6710	6000	7162	7415	7088
			6710		7170	-	-
							7707
27	315	6524	6724	5077	7180	7441	7716
58	5228	6527	5725	195:	7202	7158	7726
10	6335	6524	571t	5070	7210	745	7726 7736 7745
-	233	377	14	347		1	1777

3		D_{ℓ}	grees	of La	titude.	
in.	78	79	80	81	82	83
0		8046	8375	8739	9146	95 0 t
2	The state of	8057	8380	8752	9161	9622
4	7764	8068	8398	8705	9175	9639
	7774				9190	9056
8	7784	8 0 89			9204	9689
	7794	8110)234	970(
	7803 7813		3457	3820	9248	9723
	7823	8131	8469	8843	1263	9740
	7833	8142	8481	8857	9278	9757
20	7843	8153			9293	9774
22	7853	8164	8504	8883	9308	9792
	7863	3175	8516	8896	9323	9809
	7873	3100	8520	3022	9338	9844
	7883	8206	8553	3937	9368	
	7903				1383	9875
24	7913	8229	8577	13964	9399	9897
36	7923	8240	8589	8978	9414	9915
138	7933	1 2	8601	8991	9430	9933
	7943	Commence on contracts			9446	9951
42	7953 7964 797	8273	8020	9019	9401	9979
144	17904	3205	8651	1903	7477	10000
18	7984	13307	866	10001	9509	10025
150	7994			9075		1004
30	18005	3320	808	9080	9541	10001
154	8015	3341	18701	19103	9557	10080
106	18026	13352	18714	19115	5.9573	10099
158	8036	8364	872	9132	19590	
150	18040	10375	0/30	1914	3.9000	0137

1	3		Do	grees of	Latitua	de.	
1	n.	84	85	86 1	.87	88	89
1	0	10:37	10,65	11533	12522	13916	16300
ı	2	10156	10788	11562	12560	13974	16416
	4	1 - 1 9 1	10811	11591	12599	14033	16537
	6	1 2-	10834	11620	12639	14093	16661
	8	1.00.7	10858	11650	12679	14154	16792
	IC	- JT	10881	11680	12719	14216	16926
	12	10254	10905	11710	12760	14279	17067
		19274	10929	11740	12801	14343	1721.3
	18	10294	10953	11770	12842	14408	17366
	20	1- "J-T.	11002	11801	12927	14475	17526
	-	-		-	(commercial control co		
	21	10354	11027	11863	12970	14612	17870
	26	10395	11077	11927	13059	14756	18252
		10416	11102	11960	13104	14830	18461
		10437	11127	11992	13150	14906	18682
	32	10457	11152	12025	13196	14983	18920
		110478	11178	12059	13243	15062	19174
		10499	11204	12092	13290	15143	19450
		10521	11230	12126	13338	15226	19749
	+9	10542	11257	12160	13386	15311	20076
		2/10564	11283	12194	13435	15398	20439
		110585	11310	12229	13485	15487	20843
		10607	11337	12265	13536	15579	21303
		10629	11365	12300	13588		21832
	1-	-	11392	12336		15770	22450
		110674	11420	12372	13694		23226
	10	10719	11440	12409	13748		24215
		3 10742	11504	12483	13859		
-		10765	11533	12522	13916	1 /	
8	-	1	, , , ,		3)	1	

A TABLE of the Angles, which every Point of the Compass makes with the Meridian; serving, by Inspection, to turn the Rumbs into Degrees; and the contrary.

Rumbs.	Rumbs.	Points.	D. M	Rumbs_	Rumbs.
North.	South.	0	0 (North	South.
N. by E.	S. by E.	0 4 0 1 0 2 0 3 4 1	2 45 5 36 8 26 11 15	N. by W.	S. by W.
N. N. E.	S. S. E.	1 1 2 1 3 2 2	16 52 19 41 22 30	N. N. W.	3. S. W.
N.E. by N.	S. E. by S.	2 1 2 2 2 3 4 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		N.W. by N.	ž.W. <i>b</i> _y S.
N. E.	S. E.	3 ¹ / ₄ 3 ¹ / ₂ 3 ³ / ₄ 4	36 34 39 22 42 11 45 0		s. w.
N. E. by E.	S. E. by E.	4 ⁴ / ₄ 4 ¹ / ₂ 4 ⁴ / ₄ 5	47 49 50 38 53 26 56 15		SW. <i>by</i> W
E. N. E.	E. S. E.	5 ¹ / ₄ 5 ¹ / ₂ 5 ³ / ₄ 6	59 4 61 53 64 41 67 30		<u>w.s.w</u> .
E. br N.	E. by S.	0 ½ 6 ½ 6 ¾ 7	70 19 73 8 75 56 78 45	W. by N.	W. by S.
Eaft.	East.	7 ¹ / ₄ 1 7 ² / ₂ 7 ³ / ₄ 8	81 34 84 23 87 11 90 0	337.0	West.



TABLE

,O F "

Logarithmic Sines, Cosines, Tangents and Cotangents.

To find the Sine, Tangent, &c. of any Number of De-

RULE.

Find the Degrees at Top of the Table, the Minutes on the left Hand; against which, under the Title Sine, Tan. &c.

is the Sine, Tangent required.

Or, if the Degrees exceed 45°, find them at the Bottom; and, against the Minutes on the right Hand, above the Words Sine, Tang. &c. you have the Sine or Tangent fought.

Note, If the Degrees exceed 90, subtract them from 180, and take the Remainder. Or rather find the Degrees at Top or Bostom, and the Minutes under or above, on the same

Side.

EXAMPLE.

The Sine of 17^d 23 min. is 9.47532; and the Cofine 9.97969. The Tan. of 125^d 47^m, or of 54^d 13^m is 10.14219,

and Cotan. 9.85780.

And if the Sine, or Tangent, &c. be given, the Degrees answering to it may be found by seeking the given Sine or Tangent in its proper Column. Thus, if the Cosine be 9.76271, the Number of Degrees answering is 54^d 37^m.

When you cannot find it exactly, take the nearest. Thus, if the Tangent be 10.66735, the nearest is 10.66758, whose

N. of Degrees is 77d 52m.

Sire. Coline. Tangent. Cotang.	29
	_
	50
	59
	58
	57
	56
6 7.24187 9.99999 7.24187 12.75812;	55
1/.24.0/ 3.33333 /.24.0/ 12./30.2	5+
7 7.30882 9.99999 7.30882 12.69117 8 7.36681 9.99999 7.36681 12.63318	53
9 7.41796 9.99999 7.41796 12.58203	51
10 7.46372 0.99999 7.46372 12.53027	50
11 7.50511 9.99999 7.50512 12.49487	49
12 7.54290 9.99999 7.54290 12.45709	48
13 7.57766 9.99999 7.57767 12.42232	47
14 7.60985 9.99999 7.60985 12.30014 15 7.63981 9.99999 7.63982 12.36017	46
	45
1,00,04 3,99999 7,00,04 12,03213	44
17, 7.69417 9.99999 7.69417 12.30582 18, 7.71899 9.99999 7.71900 12.28099	43
19 7.74247 9.99999 7.74248 12.25751	41
20 7.76475 9.99999 7.76476 12.23523	40
21 7.78594 9.99999 7.78595 12.21404	i man I
22 7.80614 9.99999 7 80615 12.19384	10/1
23 7.82545 9.99999 7.82546 12.17453	
24 7.84393 9.99998 7.84394 12.15605	10
7.00100 9.99990 7.0 11 12113032	- 2
7.07000 9.99990 , .07070 1.12.12120	J 7
7.89508 9.99998 7.89500 12.10490 28 7.91087 9.99998 7.91080 12.08910	23
29 7.92611 9.99998 7.9261 12.07386	
36 7.94084 9.99998 7.94085 12.05914	
Cofine. Sine. Cotang. Tangent.	Z
190 89 Dig	The latest series

. <u> </u>	o Digre				-
Sin	Sine.		σ	1 0	179
-	-	Cosine.	Tangent.	Cotang.	
30	7.94084	9.99998	7.94085	12.05914	30
31	7.95508	9.99998	7.95509	12,04490	29
32	7.96886	9.99998	7.96888	12.03111	28
33	7.98223	9.99998	7.98225	12.01774	27
34	7.99519	9.99997	7.99521	12.00478	26
35	8.00778	9.99997	8.00780	11.99219	25
36	8.02002	9.99997	8.02004	11.97995	24
37	8.03191	9.99997	8.03194	11.96805	23
38	8.04350	9.99997	8.04352	11.95647	22
39	8.05478	9.99997	8.05480	11.94519	21
40	8.06577	9.99997	8.06580	11.93419	20
41	8.07649	9.99996	8.07653	11.92346	19
42	8.08696	9.99996	8.08699	11.91300	18
43	8.09718	9.99996	8.09721	11.90278	17
44 45	8.10716	9.99996	8.10720	11.89279	16
-	-	9.99995	8.11696	11.88303	15
46	8:12647	9.99996	8.12050	11.87349	14
47 48	8.13581	9.99995	8.135,85	11.86414	13
19	8.14495	9.99995	8.14499	11.85500	12 11
50	8 15390	9.99995	8.15395 8.16272	11.84604	IO
-	-	9.90095		11.83727	
51	8.17123	9.99995	8.17132	11.82867	9
53	8.17971	9-99995	8.17976	11.82023	7
54	8.18798	9.99994	8.19615	11.80384	6
55	8.20407	9.99994	8.20412	11.79587	5
56		9.99994			
57	8.21189	9.99994	8.21195	11.78804	4
58	8 21958 8. 22 713	9.99994	8.22719	11.77280	2
59	8.23455	9.99993 9.99993	8.23462	11.76537	I
60	8.24185	9.99993	8.24192	11.75807	0
	Coline.	Sine.	Cotang.	Tangent.	7-
		Orne.	Carrong.	89 Degre	199
90	,			7 - 5,0	

1 Degree			I	78
Sine.	Cosine.	Tangent.	Cotang.	
3.24135	9.99993	8.24192	11.75807	40
. 1.24903	9.99993	8.24910	11.75089	59
28.25609	9.99992	8.25616	11.74383	58
38.26304		8.26311	11.73688	57
8.25988	1 1 1 1 1	8.26995	11.73004	50
8.27661	-	8.27669	11.72330	55
8.28324		8.28332	11.71667	54
8.28977		8.28985	11.71014	53
8.29620 98.30254		8.29029 8.30263	11.69736	51
108.30879		8.30888	11.69111	50
3.31495	9.99990	8.31504	11.68495	49
12 3.32102	9.99990	8.32112	11.67887	48
1: 3:32701	9.99990	8.32711	11.67288	47
143.33292	9.99989	8.33302	11.66697	4(.
1 : 8.33875	9.99989	8.33885	11.66114	45
1. 3.34450	9.59989	8.34461	11.65538	44
17 3.35018	9 99989	8 35028	11.64971	43
188.35578	9.99988	8.35589	11.64410	42
15 8.36131	9.99988	8.36142	11.63857	41
	-			
21 8.37217	9.99987	8.37229	11.62770	39
23 3.38276	9.99987	8.38288	11.61711	37
24 8.38796	9.99987	8.38809	11.61190	3£
25 8 39310	9.09986	8.39323	11.60676	35
zt 8.39817	9.99986	8.39831	11.60108	
27 8.40319	9.99986	8.40333	11.59666	33
28 3.40816	9.99985	8.40830		
298.41306		8.41321	11.58678	
30 8.41791		8.41806		30
Cofine.	Sine.	Cotang.	langent.	12
91			88 Degre	es.

31	1 Degree.			I	78
in.	Sine.	Cosine.	Tangent.	Cotang.	_
30	8.41791	9.99985	8.41806	11.58193	3
31	8.42271	9.99984	8.42286	11.57713	29
32	8.42746	9.99984	8.42761	11.57238	28
33	8.43215	9.99984	8.43231	11.56768	27
34	8.43579	9.99983	8.43696	11.56303	25
35	8.44139	9.99983	8.44156	11.55843	
35	8.44594	9.99983	8.44611	11.55388	24
37	8.45044	9.99982	8.45061	11.54938	22
38	8.45489	9.99982	8.45506	11.54493	21
39	8.45930	9.99981	8.45948	11.53615	20
40	8.46266		8.46817	11.53182	19
41	8.46798	9.99981	8.47245	11.52754	18
12	8.47226	9.99980	8.47669	11.52330	17
143 44	8.47649	9.99980	8.48089	11.51910	16
45	8.48484	9.99979	8.48505	11.51494	15
46	8.48896	9.99979	8.48916	11.51083	14
47	8.49303	9.99978	8.49325	11.50674	13
48	8.49707	9.99978	8.49729	11.50270	12
149	8.50107	9.99978	8.50129	11.49870	H
50	18.50504		8.50526	11.49473	10
51	8.50897	9.99977	8.50920	11.49079	9.
52	8.51286	9.99976	8.51309	11.48690	
53	8.51672	19.99976	8.51696	11.48303	7 6
54	1)))	9.99976	8.52079	11.47920	5
25	8.52434		8.52458	1	4
56	8.52810	9-99975	8.52834		3
57		9.99974	8.53207	11.46422	2
58	1 2000	9.99974	8.53577	/	1
59	1 10/	9.99973	8.54308	1	0
-	0.44201	Sine.	Cotang.	Tangent.	2
1_	Cofine.	l oine.	00,000	88 Degr	ees.
191 88 Digress					

1.7	2 Degrees				177
in.	Sine.	Cosine.	Tangent.	Cotang.	1
C	8.54281	9.99973	8.54308	11.45091	60
1	3.54042	9.99973	8.54669	11.45330	55
2	3.54999	9.99972	8.55026	11.44973	58
3		9.99972	8.55381	11.44618	57
4 5	1 221)	9.99971	8.:57 33 8.56082	11.44266	5£
	-	9.99971		11.43917	55
7	1 2 277	9.99970	8.56429	11.43570	54
8		9.99970	8.57113	11.42886	53 52
9		9.99969	8.57451	11.42548	51
10	8.57756	9.99968	8.57787	11.42212	50
I 1	8.58089	9.99968	8.58120	11.41879	45
I 2	8.58419	9.99967	8.58451	11.41548	48
13	3.58746	9.99967	8.58779	11.41220	47
14	3.59072	9.99967	8.59105	11.40894	46
16	-			11.40571	45
17	8.59715	9.99906	8.59749	11.40250	44
18	8.60348	9.99965	8.60383	11.30616	+3 42
19	3.60662	9.99964	8.60697	11.39302	41
20	8.60973	9.99963	8.61009	11.38990	40
21	8.01282	9.99903	8.61318	11.38681	35
22	3.61589	9.99962	8.61626	11.38373	38
23	8.61893	9.99962	8.61931	11.38068	37
	3.62196 8.62496	9.99951	8.62234	11.37765	36
26	-		-	11.37464	35
	8.62794 8.63 0 91	0.99960 9.99960	8.62130	11.37165	34
28	8.53385	9.99900	8.63425	11.36574	32
29	8.63677	9.99959	8.63718	11.36281	31
3°	8.63967	9.99958	8.64009	11.3599c	3C
	Cosine.	Sine.	Cotang.	Tangent.	Σ
92				87 Degre	ees.

12	2 Degi	rees.				
lin	Sine.	1 Cosine.	Tangent.	Crtang.		
30	-			1	1	
		9.09958	8.64009	11.35990		
31	8.64256	9.99958	8.64298	111.3570	1-9	
33	10 6 0	9.99956	8.64870	11.35414	1-7	
	8.65110	9.99956	8.65153	11.34840	1 1	
	8.65391	9.99955	8 65435	11.34564		
	8.65670	9.99955	8.65714	-	24	
37		9.99954	9.65992	11.34007	23	
38	8.65223	9 99954	8.66268	11.3373.	22	
	8.66496	9.99953	8.66543	11.33451	21	
40	8.65768	9.99952	8.66815	11.33184	20	
41		9.99952	8.07086	11.32913	19	
	8.67308	9.99951	8.67356	11.32043	18	
	8.67575	9.99951	8.67623	11.32376		
	8.67840	9.99950	8.67889 8.68154	11.32110		
Total Section 1	THE RESERVE AND ADDRESS OF THE PARTY OF THE	9.99949	7	11.31845	15	
	8.68366 8.68627	9.99949	8.68417 8.68 6 78	11.31582	14	
	3.68886	9.99948	8.68938	11.31321	13	
	8.69143	9.99947	8.69195	11.30803	11	
	8.69399	9.59946	8.69452	11.30547	10	
	8.69654	9.99946.	8.69708	11.30291	0-	
	8.69907	9.99945	8.69961	11.30038	9 8	
	8.70158	9.99944	8.70213	11.29786	7	
54	8.70408	9.99944	8.70464	11.29535	6	
55	8.70657	9.99943	8.70713	11.29286	_5	
	8.70904	9.99943	8.70901	11.29038	4	
	8.71150	9.99942	8.71.208	11.28791	3	
	8.71395	9.99941	8.71453	11.28546	2	
	8.71638	9.99941	8.71697	11.28302	I	
	8,71880	9.99940	8.71939	11.28060	0	
-	Cofine.	Sine.	Cotang.	Tangent.	Z	
	92 87 Degrees.					

13	3 Degr	ces.	`	1	76
77	Sine.	Cosine.	Tangent.	Cotang.	1
0	8.71880	9.99940	8.71939	11.28000	60
I	8.72120	9.99939	8.72180	11.27819	59
	8.72359	9.99939	8.72420	11.27579	58
3	8.72597	9.99938	8.72658	11.27341	57
	8.72833	9.99937	8.72895	11.27104	56
1-1		9.99937	8.73131		55
	8.73535	9.99936	8.73366	11.26633	54
8	8.73766	9.99935	8.73599	11.26168	53 52
9	8.73996	9.99934	8.74062	11.25937	51
10	8.74225	9.99933	8.74292	11.25707	50
11	8.74453	9.99932	8.74520	11.25479	49
	8.74680	9.99932	8.74747	11.25252	48
	3.74905	9.99931	8.74974	11.25026	47
	8.75129	9.99930	8.75198	11.24801	46
	3.75352	9.99930	8.75422	11.24577	45
178	3.75574	9.99929	8.75645	11.2+354	44
188	3.75795 3.76015	9.99928	8.75866 8.76087	11.24133	43
198	3.76233	9.99927	8.76306	11.23693	42
	3.76451	9.99926	8.76524	11.23475	40
- Allegan Dist	3.76667	9.99925	8.76741	11.23258	39
228	3.76882	9.99924	8.76957	11.23042	38
	3.77096	9.99924	8.77172	11.22827	37
	.77310	9.99923	8.77386	11.22613	36
Contract of the last	.77522	9.99922	8.77599	11.22400	35
	.77733	9.99921	8.77811	11.22188	34
27 8	3.77943	9.99921	8.78022	11.21768	33
	3.78360	9.99920	8.78440	11.21559	32
	3.78567	9.99918	8.78648	11.21351	3C
-	Cofine.		Cotang.	Tangent.	Ž
9			,	86 Degrees	-1
73					

13	1 3 Degi	176	7				
777	Sine	Co/ine.	Tangent.	Cotang.			
30	8.78567	9.99918	8.78648	11.21351	30		
31	8.78773	9.99918	8.78855	11.21144	29		
32	8.78978	9.99917	8.79061	11.20938	28		
33	8.79182	9.99916	8.79266	11:20733	27		
34	8.79385	9.99915	8.79470	11.20529	26		
35	8.79588	9.99915	8.79673	11.20326	25		
36	8.79789	9.99914	8.79875	11.20124	24		
37	8.79989	9.99913	8.80276	11.19923	23		
39	8.80387	9.99912	8.80475	11.19524	21		
40	8.80585	9.99911	8.80674	11.19325	20		
41	8.80781	9.99910	8.80871	11.19128	19		
12	8.80977	9.99969	8.81068	11.18931	18		
143	8.81172	9 99908	8.81264	11.18735	17		
144	8.81366	9.99907	8.81458	11.18541	16		
45	8.81559	9.99906	8.81652	11.18347	15		
46	8.81752	9.99966	8.81846	11.18153	14		
47	8.81943	9.99905	8.82038	11.17961	13		
18	8.82134	9.99904	8.82229	11.17770	12		
49	8.82324	9.99903	8.82610	11.173.89	10		
-	The state of the s		8.82799	11.17200	9		
51	8.82701 8.82838	9.99901	8.82987	11.17012	8		
53	8.83074	9.99900	8.83174	11.16825	7		
54	8.83260	9.99899	8.83361	11.16638	6		
55	8.83445	9.99898	8.83547	11.16452	5		
56	3.83629	9.99897	8.83732	11.16267	4		
57	8.83813	9.99896	8.83916	H.16083	3		
58	8.83995	9.99895	8.84099	11.15900	2		
59	3.84177	9-99894	8.84282	11.15717	0		
60	3.84358	9.99894	8.84464	11:15535	1.		
	Cofine.	Sine.	Cotang.	Tangent.			
1 93	93 86 Degrees.						

1 4 De	grees.		179		
Sine.	Cofine.	Tangent.	Cotang.		
08.84358	9.99894	8.84464	11.15535	60	
18.8453	9.99893	8.84645	11.15354	59	
28.8471	8 9.99892	8.84825	11.15174	58	
3,8.8489		8.85005	11.14994	57	
48.8507	5 9.99890	8.85184 8.85362	11.14815	56	
		8.85540	The Person Name of Street, or other Desires, or	-	
6 8.8542	4 9.99887	8.85717	11.14459	54	
88.8578	0 9.99886	8.85893	11.14106	52	
98.8595	4 9.99885	8.86068	11.13931	57	
108.8612	8 9.99885	8.86243	11.13756	50	
118.8630	1 9.99884	8.86417	11.13582	49	
128.8647		8.86590	11.13409	48	
138.8664		8.86763	11.13230	47	
14,8,8681		8.86935	11.13064	46	
16 8.8715		-			
178.8732	5 9.99878	8.87446	11.12723	44	
18 8.8749		1	11.12383	42	
1198.8766		8.87784	11.12215	4.1	
208.8782	8 9.99875	8.87952	11.12047	40	
21 8 8799			11.11879	39	
228.8816	1 1 1 1 1 1		11.11713	38	
238.8832		8.88453	11.11546	37	
24 8.8849		1	11.11381	36	
26 8.8881		-		35	
27 8.8898	80 9.99868	8.89111	11.11052	34	
28 8.8914	2 9.99867	8.89274	11.10725	32	
20 8.8930	3 9.99866	8.89436	11.10563	31	
30 3.8946		8.89598	11.10401	30	
Cofine.	Sine	Cotang.	Tangent.	N	
1 91					

9 0-0-					_
13	4 Degre	es.		175	_1
n.	Sine.	Cosine.	Tangent.	Cotang.	
30	8.89461	9.09865	8.89598	11.10401	33
131	8.89024	9.99804	8.89759	11.10240	29
32		9.99863	8.89920	11.10079	28
33	8.89943	9.99862	8.90080	11.09919	27
3.4		9.99861	8.90239	11.09760	26
35	8,00250	9.99860	8.90398	11.09601	25
34	8.90416	9.99859	8.90556	11.09443	24
37		9.99858	8.90714	11.09285	23
	8.90729	9.99857	8.90871	11.09128	22
39	1 / /	9.99856	8.91184	11.08815	20
-					
41	1 1 1:	9.99854	8.91340	11.08659	19
42	1- /	9.99852	8.91649	11.08350	17
	18.91655	9.99851	8.91803	11.08196	16
4		9.99850		11.08043	15
-	68.91959	9.99849		11.07890	14
4		9.99848		11.07738	
	8 8.92261	9.99847		11.07586	12
	9 8.92411	9.99846	8.92564	11.07435	
5	08.92560	9.99845	8.92715	11.07284	. 10
15	18.92710	9-99844	8.92865	11.07134	
	28.92858	9.99843		11.06984	8
	38.93006	9.99842		11.06835	
	48.93154	9.99840	8.93313	11.06686	
5	5 8.93301	9.99839		11.06538	1-1
5	5 8.93448				
. 5					
5	8 8.93739				
12	98.93884	1, ,			4 0
0	08.94020	Sine.	Cotang.	Tangent.	- E
1_	1 Cosine.	i sine.	Gorang.	85 Degree	-
1	94		V	of Degree	-

1	2	Dg	·ees.		17	4
1	17.	Sine.	Cofine.	Tangent.	Cotang.	
ı	0	8 94029	9.99834	8.94195	11.05804	60
	1	8.94173	9.99833	8.94340	11.05659	59
	2	8.94317	9.99832	8.94485	11.05514	58
ı	3	8.94460 8.94603	9.99831	8.94629	11.05370	57 56
ı	5	8.94745	9.99828	8 94916		55
ı	6	8.94887	9.99827	8.95059	11.04940	54
ı	7	8.95028	9.99826	8.95202	11.04797	53
I	8	8.95169	9.99825	8.95344		52
ı	10	8.95309	9.99824	8.95485	10 1	5 I 50
1		8.95449	9.99823			49
I	12	8.95589 8.95728	9.99822	8.95767		48
1	13	8.95867	9.99819	8.96047	11.03952	47
ł	14	8.96005	9.99818	8.96186	11.03813	46
		8.96142	9.99817	8.96325		45
ł	1 (8.96280	9.99816	8.96463	777-1	44
I	18	8.96416 8.96553	9.99813	8.96601 8.9673 9		43
I	15	8.96689	9.99812	8.96876		41
L	20	8.96824	9.99811	8.97013		40
1	2.1	8.96959	9.99810	8.97149		39
8	22	8.97094	9.99809	8.97285		38
3		8.97228	9 99808	8.97420		37 36
		8.97362	9.99806	8.97555 8.97690		35
1		8.97629	9 99804	8.97824.		34
	7/3	8.97761	9.99803	8.97958	£ , at 3"	331
12	3	8 97894	9.99802	8.98092	11.01907	32
ľ	9	3.98025	9.99800	8.58225	1 / / TI	31
1	-	3.08157	9 99799	8.98357	-	3 C
-	-	Cofine.	Sine.	Cotang.	Tangent.	2
1	5)5 .			84 Degree.	5

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ſ	Min	5 Degre	es.		17	4
l	7	Sine.	Cosine.	Tangent.	Cotang.	_
I	30	8.98157	9.99799	8.08357	11.01642	310
Ì	31	8.98288	9.99798	8.98489	11.01510	29
Ì	32	8.98418	9.99797	8.98621	11.01378	28
I	33	8.98549	9.99795	8.98753	11.01246.	26
١	34	8.98678	9.99794	8.98884	11.001115	25
1	35		9.99793	8.99145	11.00854	24
ı	36 37	8.98937	9.99792	8.99275	11.00724	23
ı	38	8.99194	9.99789	8.99404	11.00595	22
	39	8.99322	9.99788	8.99533	11.00466	21
ı	40	8.99449	9.99787	8.99652	11.00337	2.0
ı	41	8.99576	9.99785	8.99790	11.00209	1.9
	12	8.99703	9.99784		11.00081	1.8
	43	8.99829	9.99783	9.00046	10.99953	17
	14	0.00081	9.99782	9.00173	10.99609	15
,	15	-			10.99572	14
	₄₆	9.00266	9.99779		10.99446	13
	47 48	9.00456			10.99320	12
	49	9.00580	9.99775	19.00804	10.99195	II
	50			9.00929	10.99070	10
	51	9.00827	9.99773	9.01054		9
	5 2				10.98820	7
	53					6
	54	1 -		9.01426		5
	55		الاستسال			4
	56	9.01439	9.99766			
	57		9.99764		1 00	2
	59			9.02040	10.97959	
	60				10.97837	0
	1	Cofine.	Sine.	Cotang.	I Tangent.	2
	1				84 Deg	rees.

-1	3 6 Deg	rees.		The state of the s	73- 1			
	E Sine.	1 Cofine.	Tangent.	Cotang.	1_			
	0,9.1.23	9 00.761	9.02162	110.07837	00			
1	1 9.02043	9.99760	9.02283	10.97710	15%			
ı	29.02163	9.99758		10.97595	58			
	3 9.02282	9.99757	9.02525		57			
	49.02401	9.99756			5			
I	59.02520	-	9.02-6;	10 97234	15			
	69 02038	9.99753	9.02885	10.57114	54			
	7,9.02756 8,9.02874	9.99752	9.03004	10.96995	53			
	9,9.02991	9.99749	9.03242	10.96757	52 51			
ı	10,0.03108	9.99747	9 03360	10.96639	50			
ı	11903225	9.99746	9.03479	10.96520	49			
ı	129.03342	9 99745	9.03596	10.96403	48			
I	139.03458	9.99743	9.03714	10.96285	47			
1	149.03574	9'99742	9.03831	10.96168	46			
1	15 9.03689	9.99741	9.03948	10.96051	45			
1	16 9.03804	9.99739	9.04065	10.95934	44			
	179.03919	9.99738	9.04181	10.95818	43			
	18 9.04034	9.99736	9.04297	10.95702	42			
	2019.04262	9.99735	9.04412	10.95587	41			
1	9.04376				40			
	22 9.04489	9.99731	9.04643	10.95356	39 38			
	39.04602	9.99731	9.04872	10.95127	37			
2	49.04715	9.99728	9.04986	10.95013	36			
2		9.99727	9.05100	10.04899	35			
2		9.99725	9.05214	10.94785	34			
2	79.05051	9.99724	9 05327	10.94672	33			
		9.99722	9.05440	10.94559	32			
	-1	9.99721	9.05553	10.94446	31			
13	-	0.00719	9.05665	10.94334	30			
-	Cofine.	Sine.	Cotang.	Targent.	N.			
4	96 - 83 Degrees.							

1	6 Deg	rees.		1	73
	Sine.	Cosine.	1 Tangent		1
3	09.05385	9.9971	9.0566	10.9433	1 30
	1 9.05490	9.99718	3,9.05778		
	2 9.05607	9.99717	1		
_	3 9.05717	9.99715		10.93998	
_	5 9.05936	9.99714	1	10.93887	
-	6 9.06046	9.99711		10.93665	24
13	1 '	9.99709	9.06445	10.93554	1 . 1
3		9.99708	9.96555	10.93444	22
39	, ,	9.99706	9.06665	10.93334	21
4		9.99705	9.06775	10.93224	20
4	8 2	9.99703	9.06884	10.93.115	18
4:	1 (0'	9.99702	9.06993	10.93006	17
4.	, ,	9.99700	9.07211	10.92788	16
4		9.99697	9.07319	10.92680	15
46	9.07124	9.99696	9.07427	10.92572	14
47	7.07230	9.99694	9.07535	10.92464	13
	9.07335	9.99693	9.07643	10.92356	12
49		9.99691	9.07750	10.92249	10
50		9.99690	9.07857	10.92142	
51	9.07653	9.99588	9.07904	10.92035	9 8
52		9.99685	908177	10.91822	
	3.07967	9.99684	9.08283	1091716	7 6
55		9.99682	0.08389	10.91610	5
56	9.08175	9.99681	9.08494	10.91505	4
57).08279	9.99679	9.08599	10.91400	3
58	7.08383	9.99678	9.08705	10.91294	2
59 6c	3.08486	9.99675	9.08014	10.91190	0
-	Cofine.	Sine. +	Gotang.	Tangent.	7
9			3.1	83 Degree	26
7				2 8	

Z	7 Degree	s.		1	72]
Min.	Sine.	Cosine.	Tangent.	Cotang.	
c	9 08 589	9.99675	9.08914	10.91085	60
1	9.08692	9.99673	9.09018	10.90981	59
2	9.08794	9.99671	9.09122	10.90877	58
3	9.08897	9.99670	9.09226	10.90773	57
5	9.00999	9.99667	9.09433	10.90566	55
1	9.09202	9.99665	9.09536	10.90463	54
	3.09303	9.99664	9.09639	10.90360	53
8	9.09404	9.99562	9.09742	10.90257	52
9	3.09505	9.99660	9.09844	10.90155	51
10	9.09606	9.99659	9 09946	10.90053	50
11	9.09706	9.99657	9.10048	10.89951	49
12	, ,	9.99656	9.10150	10.89849	48
14	, ,,	9.99652	9.10353	10.89646	47 46
115	9.10105	9.99651	9.10454	10.89545	45
16		9.99649	9.10555	10.89445	44
17	9.10303	9.99648	9.10655	10.89344	43
18		9.99646	9.10755	10.89244	42
20	1)	9.99644	9.10856	10.89143	41
	177	9.99643	9.10955	10.89044	10
21	9.10495	9.99640	9.11055	10.88944	39
		9.99638	9.11254	10.88745	38
	9.10990	9.99636	9.11353	10 88646	36
25		9.99635	9.11452	10.88547	35
26	13	6.99633	9.11550	10.88449	34
27	17	9.99631	9.11649	10.88350	33
28	122/1	9.99630	9.11747	10.88252	32
30		9.99628	9.11845	10.88154	31
3	Cofine.	Sine.	Cotang.	Tangent.	3C
1		1 ome.	Gorang.	82 Degr	2
. 8	77	-		Or Degi	663.

-								
137	M	7 Degre	es.			72		
n.	I	Sine.	Cofine.	Langent.	Cotang.	1		
3	0	9.11569	9.99626	9.11942	10.88057	30		
3	I	9.11005	9.99025	9.12040	10.87959	29		
3	2	9.11761	9.99623	9.12137	10.87862	28		
3	3	9.11856	9.99621	9.12234	10.87765	27		
3	4	9.11951	9.99620	9.12331.	10.87668	26		
3		9.12046	9.99618	9.12428	10.87571	25		
3	6	9.12141	9.99016	9.12524	10.87475	24		
3:	7	9.12236	9.99615	9.12621	10.87378	23		
3		9.12330	9.99613	9.127.17	10.87282	22		
3	9	912424	9.99611	9.12813	10.87186	21		
4	0	9.12518	9.99610	9.12908		20		
4	I	9.12012	9.99608	9.13004	10.86995	19		
4	2	9.12706	9.99606	9.13099	10.86900	18		
4:	-	9.12799	9.99604	9.13194	2 6	17		
14		9.12892	9.99603	9.13289	1	16		
4		9 12985	9.99601	9.13383	-	15		
40	6	9.13078	9.99599	9-13478	10.86521	14		
4		9.13170	9.99598	9.13572	10.86427	13		
48	_	9.13262	9.99596	9.13666	10.86333	12		
49		9.13355	9.99594	9.13760	10.86239	111		
50	-	9.13417	9.99592	9.13854		10		
5		9.13538	9.99591	9.13947	10.86052	9		
5	_	9.13630	9.99589	9.14040	10.85959	8		
53	_	9.13721	9.99587	9.14134	10.85866	7		
54		9.12812	9.99585	9.14226	10.85773			
5		9.13903	9.99584	9.14319	-	5		
. 50		9.13994	9.99582	9.14412	10.85587	4		
5	/	9.14085	9.99580	9.14504	10.85495	3		
58		9.14175	9.99578	9.14596	10.85403	1		
50		9.14265	9.99577	9.14780	10.85219	C		
-	-	9.14355	9.99575	CONTRACTOR OF THE PARTY OF THE		Z		
1		1 fine.	Sine.	Cotang.	Tangent.	\geq		
1.0	82 Degrees.							

151	8 Degree	· ·		17	T I			
Min	Vine.	Cofine.	langent.	Cotang.				
0	1.14355	9 99575	9.14780	10.85219	60			
1	J.14445	9.99573	9.14871	10 85128	59			
2	9.14534	9.99571	9.14963	10.85036	58			
3	9.14624	9.99569	9.15054	10.84945	57			
4	9.14713	9.99568	9.15145	10.84854	56			
5	7.14802	9.90566	9.15236	10.84763	5.5			
6	9.14891	9.99564	9.15326	10.84673	54			
1 7 8	9.14980	9.99562	9.15417	10.84582	53			
9	1 - ,	9.99559	9.15597	10.84402	51			
10		9.99557	9.15687.		50			
II	1.15333	9.99555	9-15777	10.84222	49			
12	7.15420	9 99553	9.15867	10.84132	48			
13	9.15508	9.99551	9.15956	10.84043	47			
I	1.15595	9.99550	9.16045	10.83954	46			
IS	915682	9.99548	9.16134	10.83865	45			
16	13.00/10	9.99546	9.16223	10.83776	44			
17	9.15856	9.99544	19.16312	10.83687	43			
Iç	17. 2777	9.99542	9.16400	10.83599	42 41			
20		9.99539	9.16577	10.83422	40			
21	9.16202	9.99537	9.16665	10.83334	39			
22		9.99535	9.16753	10.83246	38			
23	9.16374	9.99533	9.16840	10.83159	37			
24	9.16459	9.99531	9.16928	10.83071	3£			
25		9.99529	9.17015	10.82984	35			
	9.16630	9.99527	9.17102	10.82897	34			
127		9.99525	9.17189	10.82810	33			
	9.16800	9.99524	9.17276	10.82723	32			
30		9.99522	9.17363	10.82636	31			
1	Cofine.	Sine.	Cotang.	- Charleston - and	30			
-		oine.	country.	Tangent.	12			
10	98 81 Degrees.							

N	8 Degi	rees.		171	-1			
1111	Sine.	Cofine:	Tangent.	Cotang.				
30	9.16970	9.99520	9.17449	10.82550	3.C			
3 1	9.17054	9.99518	9.17530	10.82463	29			
	9 17138	9.99516	9 17622	10.82377	28			
33	9.17223	9.99514	9.17708	10.82291	27			
34	9.17306	9.99512	9.17794	10.82120	25			
-	9.17390	9.99510			-			
	9-17474	9.99508	9.17905	10.82034	24			
	9.17557	9.99507	9.18136	10.81863	22			
	9.17641	9.99503	9.18221	10.81776	21			
10	9.17807	9.99501	9.18305	10.81694	20			
- Children	9.17890	9.99499	9.18390	10.81009	19			
	9.17972	9.99497	9.18475	10.81524	18			
	9.18055	9.99495	9.18559	10.81440	17			
44	9.18137	9.99493	9.18643	10.81356	16			
45		9.99491	9.18728	10.81271	15			
-	9.18301	9.99489	9.18811	10.81188	14			
	9.18383	9.99487	9.18895	10.81104	13			
18	9.18465	9.99485	9.18979	10.81020	I Z			
19	9.18546	9.99483	9.19062	10.80937	LI			
50	9.18628	9.99481	9.19146	10.80853	10			
51		9.99479	9.19229	10.80770	2			
	9.18790	9-99477	9.19312	10.80687	8			
53	9.18871	9.99475	9.19395	10.80521	7			
148	9.18951	9.99473	9.19560	10.80439	5			
55		9.99471		10.80356	-2			
	9.19112	9.99469	9.19543	10.80350	3			
57		9.99407	9.19807	10.80192	2			
	9.19273	9.99463	9.19889	10.80110	1			
	9.19433	9.99461	9.19971	10.80028	0			
-	Cofine.	Sine.	Cotang.	Tangent.	M			
-	98			81 Degrees.				
	9							

102	9 Deg	rees.		170				
in.	Sine.	Cofine.	Tangent.	Cotang.				
0	9.19433	9.99.101	9.19971	10.80028 00				
1	9.19512	9.99459	0.20052	10.79947 59				
2	9.19592	9-99457	9.20134	10.79865 58				
	9.19671	9.99455	9.20215	10.79784 57				
5	9.19751	9.99453	9.20297	10.79702 56				
16		9.99451	9.20378	10.79621 55				
7	9.19909	9.99449	9.20459	10.79540 54				
8	9.19987	9.99447	9.20540	10.79459 53				
9	9.20145	9.99443	9.20701	10.79298 51				
10	9.20223	9.99441	9.20781	10.79218 50				
11	9.20301	9.99439	9.20801	10.79138 49				
12	9.20379	9.99437	9.20942	10.79057 48				
113	19.20457	9.99435	9.21022	10.78978 47				
14	9.20535	9.99433	9.21101	10.78898 46				
15	9.20613	9-99431	9.21181	10.78818 45				
	9.20690	9.99429	9.21261	10.78738 44				
18	9.20767	9.99427	9.21340	10.78659 43				
	9.20845	9.99425	9.21419	10.78580 42				
20	9.20999	9.99421	9.21577	10.78501 41				
21	9.21075	9.99419	9.21656					
22	9.21152	9.99417	9.21735	10.78343 39				
23	9.21229	9.99414	9.21814	10.78185 37				
24	9.21305	9.99412	9.21892	10.78107 36				
25	3.21381	9.99410	9.21970	10.78029 35				
26	1.21457	9.99408	9.22049	10.77950 34				
27	4.21533	9.99406	9.22127	10.77872 33				
2¢	7.21609	9.99404	9.22205	10.77794 32				
30	9.21685	9.99402	9.22282	10.77717 31				
-		9.99400 Sine.	9.22360	10.77639 30				
!	Coline.	oine.	Cotang	Tangent. \S				
_	99 . 80 Degrees,							

N	9 Degi	rees.		170	. 1
in.	Sine.	Cofine.	Tangent.	Cotang.	2
30	9.21700	9.99400	9.22300	10.77639	30
	9.21836	9.99398	9.22438	10.77561	29
	9.21911	9 99396	9.22515	10.77484	28
	9 21986	9.99393	9.22592	10.77407	27
35	9.22136	9.99391	9.22747	10.77329	25
سنا ا	9.22211	9.99387	9.22823	10.77176	24
37	9.22286	9.99385	9.22900	10.77099	23
38	9.22360	9.99383	9.22977	10.77022	
	9.22434	9.99381	9.23053	10.76946	2.15
-	9.22583		9.23130	10.76869	
	9.22557	9.99376	9.23206	10.76793	18
	9.22731	9.99372	9.23358	10.76641	17
	9.22804	9.99370	9.23434	10.76565	16
45	-	9.99368	9.23510	10.76489	15
	9.22951	9.99365	9.23585	10.76414	14
	9.23025	9.99363	9.23661	10.76338	13
	9.23171	9.99359	9.23812	10.76187	12
	9.23244	9.99357	9.23887	10.76112	10
	9.23317	9.99355	9.23962	10.76037	- 9
52	9.23389	7.99352	9.24037	10.75952	8
	9.23462	3.99350	9.24111	10.75888	7
	9.23534	9.99348	9.24186	10.75813	6
-	9.23679	9.99344	9.24335	10.75654	5
10	9.23751	9.99341	9.24409	10.75590	3
58	9.23823	9.99339	9.24483	10.75516	2
	9.23895	9.99337	9.24557	10.75442	1
-	0.23967	9.99335	9.24631	10.75368	
-	Cofine.	Sine.	Cotang.		≅
-	99			Bo Degrees.	_

15	10/	egrees.		16	9			
1177	Sine.	Cosine.	Tangent.	Cotang.	1			
10	9.234.67	0.99435	0.24631	10.75368	60			
	19.24038	-	10.24705	10.75294	59			
	2,9.24110	, , , , , ,	9.24779	10.75220	58			
	9.24181	9.99328	9.24852	10.75147	57			
1	9.24252	9.99326	9.24926	10.75073	56			
1	0.24323	9.90323	9.24999	-	55			
1	9.24394	9.99321	9.25073	10.74920	54			
8	9.24536	9.99317	9.25219	10.74780	52			
	9.246:6	9.99314	9.25292	10.74708	51			
110	9.24677	9.99312	7.25364	10.74635	50			
11	17-17/17/	9.99310	9.25437	10.74562	49			
	9.24818	9.99308	9.25509	10.74490	48			
8 ~	9.24888	9.99303	9.25582	10.74417	47 46			
135		9.99301	9.25726	10.74273	45			
16	· · · · · · · · · · · · · · · · · · ·	9.99299	9.25799	10.74200	44			
17	9.25167	9.99296	9.25870	10.74129	43			
18	9.25237	9.99294	9.25942	10.74057	42			
19	, ,,	9.99292	9.26014	10.73985	41			
20	9.25376	0.90289	9.26086	10.73913	40			
21	9.25445	9.99287	9.26157	10.73842	39			
23	9.25514	9.99285	9.26229	10.73770	38			
24	1.25652	9.99280	9.26371	10.73628	36			
25).25721	9.09278	9.26442	10.73557	35			
2(1.25789	9.99275	9 26513	10.73486	34			
2	1.25858	9.99273	9.26584	10.734:5	33			
2 (7.25926	9.99271	9.26655	10.73344	32			
30	3.25995 1.26063	9.99268	9.26726	10.73273	31			
-	Coline.	9.99266 Sine.		10.73203	5			
		oine.	Cotang.	Tangent.	2			
1 1	100							

	10 1)	egreis.		160	1
W.L.	Sine.	Cofine.	Tangent.	Cot xng.	
30	-	9.99-6	1720790	10.7320	30
3	-	9.902	1.20867	10.73132	29
3:	1 , ,	9.99261	1.26937	10.73012	20
33	1 / 5"	9 99250	3.27007	10.72992	27
134		9 99257	1.2707;	10.72922	26
33	9.26102	9.09254	9.2714	10.728;2	5
36		9.99252).27217	10.72782	4
37		9.99250).27287	10.72712	23
38	1	9.99217	1.27357	10.72642	22
39		9.99245	3.27426	10 72573	115
40		9 9924	1.27496	10.72;03	20
41		9.99240	9.27505	10.72434	19
42		9.99238	9.27635	10.72364	19
43	1 ' '	9.99235	9.27773	10 72226	17
45	9.27073	9.99231	7.27812	10.72157	15
46		9.97228	9.27911	10.72088	-4
47	9.27206	9.99226	9.27980	10.72019	14
48	9.27272	9 99223	9.28048	10.71951	12
49	9.27338	9.99221	9.28117	10.71882	11
50	9.27404	9.99219	9.28185	10.71814	10
51	9-27470	9.99216	9.28254	10.71745	9
52	9.27536	9.99214	9.28322	10.71677	8
53	9 27602	9.99211	9.28390	10.71609	7
54	9.27668	9.99209	9.28458	10.71541	6
55	9.27733	9.99206	9.28526	10.71473	. 5
56	9.27799	9.99204	9.28594	10.71405	4
57	9.27864	9.99202	9.28662 9.2873C	10.71337	3
58	9.27929	9.99199	9 2873C 9 28797	10.71202	2
59	9.27994	9.99197	9.28865	10.71134	C
		Sine:	Cotang.	Tangent.	
-	Cofine.	Oinc. 1	70	D	\mathbf{z}
I	00			8	-

11	Deg	rees.		168				
3 Sin	ie.	Cofine.	Tangent.	Cotang.				
0 9.28	059	9.99194	9.28865	10.71134	00			
1 9.28	124	9.99192	9.28932	10.71067	59			
29.28		9.99189	9.28999	10.71000	58			
3,9 28		9 99187	9.29067	10.70932	57			
49.28		9.99184	9.29134	10.70865	56			
5 9.28		9.99182	9.29201	10:70798	55			
6 9.28		9.99179	9.29208	10.70731	54			
7 9.28	512	9.99177	9.29335	10:70665	53			
17.20	570	9.99174	9.29401	10.70598	52			
99.28		9.99172	9.29468	10.70465	51			
11 9.28	-	9.99107	9.29501	10.70398				
12 9.28	822	9.99107	9.29667	10.70390	49			
13 9.28		9 99162	9.29733	10.70266	47			
149 28	950	9.99159	9.29800	10.70199	46			
15 9.29		9.99157	9.29866	10.70132	45			
16 9.20	087	9.99154	9.29932	10.70007	44			
179.20		9-99152	9.29998	10.70001	43			
180 20	213	9 99149	9.30063	10.69936	42			
199.29	276	9.99147	9.30129	10.69870	41			
20.9.20		9.99144	9.30195	10.69804	40			
21 9.29	402	9.99142	9.30260	10.69739	39			
	465	9.99139	9.30326	10.69673	38			
23 9 20	528	9.99137	9.30391	10.69608	37			
24 9.29	600	9.99134	9.30456	10.69543	36 35			
			9.30521	The Person of th	- Comments			
26 9.29	7710	9.99126	9.30586	10.69413	34			
28,9.29	841	9.99120	9.30051	10.69348	32			
29 9.29	1003	9.99121	9.30781	10.69218	31			
30 9.20	1965	9.99119	9.30846	10.69153	30			
Towns of the last of	ine.	-	Cotang.	Tongent.	N.			
101					_ 3			
-	101 78 Degrees.							

N	1 11 De	grees.		16	8
in.	Sine.	Cofine.	Tangent.	Cotang.	1_
30	9.29965	9.99119	9.30840	10.69153	30
31		9.99116	9.30910	10.69089	
32		9.99114	9.30975	10.69024	_
33	9.30151	9 99111	9.31039	10.68960	
_	9.30213	9.99108	9.31168	10.68831	25
35		The second second second	9.31232	10.08767	24
	9 30336	9.99103	9.31296	10.68-703	23
	9.30397	9.99101	9.31360	10.68639	1 01
-	9.30520	9.99095	9.31424	10.68575	21
	9.30581	9 99093	9.31488	10.68511	20
-	9.30643	9.99090	9.31552	10.68447	19
	9.30704	9.99088	9.31615	10.68384	18
43	9.30765	9.99085	9.31679	10.68320	17
44	9.30825	9.99082	9.31742	10.68257	16
-	9 30886	9.99080	9.31806	-	15
46	9.309+7	9.99077	9.31869	10.68067	14
47	9 31007	9.99075	9.31932	10.68003	12
40	9.31128	9.99069	9.32059	10.67940	EZ
149	9.31189	9.99067	9.32122	10.67877	10
-	9.31249	9.99064	9.32185	10.67814	9
52	9-31309	9.99061	9.32247	10.67752	
53	9.31369	9.99059	9.32310	10.67689	76
54	9.31429	9.99056	9.32373	10.67626	
55		9-99053	9.32435	10.67564	5
56	9.31549	9.99051	9.32498	10.07501	4
57	9 31609	9.99048	9.32560	10.67439	3
58	9.31668	9.99045	9.32623	10.67314	I
	9.31728	9.99043	9.32747	10.67252	0
-	Cofine.	Sine.	Cotang.	Tangent.	2
	101			78 Degrees.	

-	350	To the other states			man g
11.7	12 Deg		the son to	161	_
-	Sine.	Coline	Tangent.	Cotang.	
0	3.31787	9.99040	9-32747	10.67252	60
I).31847	9.59037	9.32809		59
2	9.31906	9.99035	9.32871	10.67128	5
3	9.31965	9.99032	9.32933	10.67066	57
4	1/0	9.99229	9.32995	10.67004	5t
5		0.99726	0.33057	10.66942	55
6	12.2	9.59724	9.33118	10.66881	54
7 8	9.32201	9.59021	9.33180	10.66819	53
1	19.3	9.99018	9.33241	10.63758	52
10	9.32319	9.99016	9.33303	10.66696	51
		9.59013	9.33364	Contracting and the second	50
	9.32436	9.99010	9.33425	10.66574	49
	9.32495	19.59007	9.33487	10.66512	48
	39.32553	9.99005	9.33548	10.66451	47
11	9.32611	9.99002	9.33609	10.66329	46
1 (9.98699	-	10.66268	45
	17.30/20	9.98595	9-33731	10.66208	44
		9.98991	9.33791	10.66147	43 42
1	13.20044			10.66086	4.1
2	1 3 /		9.33973	10.66026	40
2	19.33017				39
2	2 9.33075	9.98980	9.34094		38
	39.33132	9.98977	9.34155	10.65844	37
	49.33190			10.65784	36
	5 9.33247	9.98972	9.34275		35
	9.33305	9.98960	9-34335		
	7 9.33362	9.98966		10.65604	33
	9.33410				
	9 9.3347				
1	9-3353	-		THE R. LEWIS CO., LANSING, MICH.	
1	Cofine.	1 Sine.	Cotang		Z
1	102			77 Degrees	5.

12	12 Degrees167						
in.	Sine.	Cosine.	Tangent.	Cotang.			
30	9.33533	9.98958	9-34575	10 55121	10		
31	9.33590	9.98955	9.34035	10.65304	29		
32	9 3 3 6 4 7	9.98952	9.34694	10.65305	28		
33	9 33704	9.98949	9.34754	10.65245	27 26		
35		9.98940	9.34873	10.65126	25		
36		9.98911	9.34932	10.65007	24		
37		9.98938	9.34992	10.65007	23		
38		9.98935	9.35051	10.64948	22		
39		9.98932	9.35110	10.64889	21		
40		9.98929	9.35169	10.64830	20		
41	1/21 22	9.98927	9.35228	10.64771	18		
42		9.98924	9.35287	10.64712	17		
43	1, 2,	9.98921	9 35346	10.64594	16		
4:		9.98915	9.35464	10.64535	15		
40		9.98912	9.35522	10.64477	14		
4	17 21127	9.98909	9.35581	10.64418	13		
48		9.9897	9.35639	10.64360	12		
49		9.98904	9.35698	10.64301	II		
50	-	9.98901	9.35756	10.64243	10		
5		9.98898	9.35814	10.64185	9 8		
5		9.98895	9.35873	10.64126	7		
5.		9.98892		10.64010	6		
5		1 200%	9.36047	10.63952	15		
-	6 9.34939	9.98884	9.36105	10.63894	4		
5		9.98881	9.36163	10.63836	3		
5	8 9.35099	9.98878	9.36221	10.63779			
	9,9.35154	9.98875	9.36278	10.63721	0		
6	0 9 3 5 2 0 8	9.98872		10.63653	-		
1_	Cosine.	Sine.	Cotang.	Tangent.	Z		
T	102 77 Degrecs.						

1					66:
No demanded	Degrees				00.
Sin	ie. Co	sine. 1	angent.	Cotang.	
09.35	208 9.9	8872 9	.36330	10.6366	3 60
1 9.35		8869 9	.36394	10.6360	59
29.35	01-0		.36451	10.63548	
39.35			.36509		57
49.354		386c 9	.36566	10.63433	
59.354	181 9.98	3857 9	.36623	10.63376	55
69.35	535 9.98	3854 9	36681	10.63319	54
79.359			36738	10.63261	153
89.356	544 9.98	3848 9.	30795	10.63204	52
99.350		3845 9.	36852	10.63147	51
109.357			36909	10.63090	50
119.358	306 9.98	840 9.	36966	10.63033	49
129.358	60 9.98		37023	10.62976	48
139.359	14 9.98		37079	10.62920	47
14,9.359	67 9.98		37136	10.62863	46
159.360		828 9.	37193	10.62806	45
16,9.360			37249	10.62750	44
179.361	28 9.98		37306	10.62693	43
189.361	82 9.98		37362	10.62637	42
199.362		_	37419	10.62580	41
20 9.362	-	The state of the last of the l	37475	10.62524	40
21 9.363.	42 9.98	810 9.	37531	10.62468	39
22 9.363			37588	10.62411	38.
23 9.364		, ,		10.62355	37
24 9 3650	9.98		7700	10.62299	36
25 9.365		-	-	10.62243	35
26 9 3660	1 90 0 . 0			10.62187	34
25 9.3666 28 0.3671				10.62131	33
12.2.1				10.62076	31
30 9.3681		782 9.3		10.61964	30
			-		-
Cosine	. Sin	e. Co	tang.	Tangent.	3
103			9	76 Degrees	1

N	13 Deg	rees.		166			
n.	Sine.	Cosine.	Tangent.	Cotang.			
30	9.36818	9.98783	9.38035	10.61964	30		
31	9.36871	9.98780	9.38091	10.61909	29		
32	9.36923	9.98777	9.38146	10.61853	28		
33	9.36976	9.98774	9.38202	10.61797	26		
34	9.37080	9.98770	9.38257	10.61687	25		
36	9.37133	9.98767	9.38368	10.61631	24		
37	9.37185	9.98761	9.38423	10.61576	23		
38	9.37237	9.98758	9.38478	10.61521	22		
39	9.37289	9.98755	9.38533	10.61466	20		
40	3.37341	9.98752	9.38588	10.61411			
41	9.37393	9.98749	9.38643	10.61356	19		
42	9.37445	9.98746	9.38698	10.61301	17		
43	9.37496	9.98743	9.38753	10.61191	16		
44	9.37548	9.98740	9.38863	10.61136	15		
46	9.37651	9.98734	9.38917	10.61082	14		
47	9.37703	9.98731	9.38972	10.61027	13		
48	9-37754	9.98727	9.39027	10.60973	12		
49	9.37806	9.98724	9.39081	10.60918	10		
50	9.37857	9.98721	9-39135		-		
51	9.37908	9.98718	9.39190	10.60809	98		
52	9:37960	9.98715	9-39244	10.60701	7		
53	9.38011 9.38c 6 2	9.98712	9.39353	10.60646	6		
55	9.38.113	9.98706	9.39407	10.60592	_5		
56	9.38164	9.98702	9.39461	10.60538	4		
57	9.38215	9.98699	9.39515	10.60484	3		
58	9.38266	9.98696	9:39569	10.60430	1		
	9.38316	9.98693	9.39623	10.60376	C		
60	9.38367	9.98690	9.39677		1.1		
1	Cofine.	Sine.	Cotang.	Tangent.	=		
	103 . 76 Degrees.						

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13 14 D	grees.		16	5	
3 Sine.	(io/ine.	Tangent.	Cotang.	1_	
0'9.38367	9.98190	9.39677	110.60322	60	
19.38418	9.98687	9.39730	10.00269		
2 9.38468	9.98684	9.39784	10.60215		
39.38519	9.98680	9.29838	10.60161		
49.38569	9.98677	9.39891	10.60054		
09.38070	9.98071	9.35958	10.00001	-	
79.38720	9.98668	9.40052	10.59947		
8 9.38770	9.98665	9.40105	10.59894		
99.38821	9.98661	9.40159	10.59840		
100 38871	0.98658	9.40212	10.59787	-	
1119.38921	9.98655	9.40205	10.59734	49	
129.38971	9.98652	9.40318	10.59681		
139.39020	9.98645	9.40371	10.59628		
15,9.39120	0.08642	9.40477	10.59522		
109.39170	9.98039	9.40530	10.59469	_	
17 9.39219	9.98636	9.40583	10.59416		
189.39269	9.98633	9.40636	10.59363		
199.39319	9.98629	9.40689	10.59310	41	
20 9.29368	9.98626	9.40741	10.59258		
21 9.39417	9.98623	9:40794	10.59205	39	
22 9.39467	9.98616	9.40847	10.59152		
249 39565	9.98613	9.40952	10.59047		
25 9.39 514	9.98610	9.41004	10 58995		
20 9.39564	9.98607	9.41056	10.58943	34	
27 9.39713	9.98603	9.41109	10.58890	331	
28 9.39762	9.98600	9 41 161	10.58838		
299.39811	9.98597	9.41213	10.58786		
30 9.39859	9.98594	9.41265	Supplementary of the last of t	2	
Cosine.	Sine.	Cotang.	Tangent.	2	
104 75 Degrees.					

13	31 14 D	grees.		1 : 16¢	-
Tana.	Sine.	Coline.	Tangent		-
30	0 9.39850	9.98594		-	30
3	1,000			7 10.580822	
3.	:- 07731				
3:	1	1 / / 3 1			7
3	. 1) !	1 - 1 - 1	9.41525		
136	9.40152				- 4
137		9.98571	19.41629	10.583702	
38	1- "			10 583192	
39	1 , , ,	9.98564	1	1 / / 1	- 4
+1	-		9.41784	-	4
12	1 . 233	9.98557	9,41835	10.58104 10	
+3		9.98551	9.41938	10.5806117	
44		9.98548	9.41990	10.5800016	
15	-	9.98544	9.42041	10.5795815	
+6	1	9.98541	9.42092	10.57907 14	- 2
47		9.98538	9 42143	10.57856 13	
19	,	9.98531	9.42195	10.57804 12	33
150		9.08728	9 42297	10.57702 10	6
51	9.40873	9.98;24	9.42348		
52	9.40920	9.98521	9.42399	10.57600 8	20
53	9.40968	9.98517	9 42450	10.57549 7	
54	9.41015	9.98514	9 42501		T. Carlo
56	9.41110		9 42551	10.57448 5	
57	9.41157	9.9850-	9 42602	10.57397 4	
58	9.41205	9.98501	9.42704	10.57295 2	
59	9.41252	9.98497	9.42754	10.57245 1	
60	9-41299	9.98494	9 42805	10.57194 0	
	Cofine.	Sine. 1	Cotung.	langene. Z	}
-	104		7	5 Dogrees.	

13	1 15 Dig	recs.		164	1		
in.	Sine.	Cofine.	Tangent.	Cotung.			
0	9.41299	9.98494	9.42805	10.57194	60		
I	9.41346	9.98490	9.42855	10.57144	59		
	9.41393	9.98487	9-12906	10.57093	58		
	9.41440	9.98484	9.42956	10.57043	57		
5	9.41487	9.98480	9.43006	10.56993	56		
	9.41581	9.98474	9.43107	10.56892	54		
7	9.41628	9.98470	9.43157	10.56842	53		
	9.41675	9.98467	9.43207	10.56792	52		
9	9.41721	9.98463	9.43257	10.56742	51		
10	9.41768	9.98460	9.43308	10.56691	50		
11	9.41814	9.98456	9.43358	10.56641	49		
	9.41861	9.98453	9.43408	10.56592	48		
	9.41907	9.98446	9.43457	10.56492	47		
	9.42000	9.98443	9.43557	10.56442	45		
16	9.42047	9.98439	9.43607	10.56392	44		
17	9.42093	9.98436	9.43657	10.56342	43		
18	9.42139	9.98432	9.43706	10.56293	42		
	9.42185	9.98429	9.43756	10.56243	41		
	9.42231	9.98425	9.43805	10.56194	40		
21	9.42277	9.98422	9.43855	10.56144	39		
3	9.42323	9.98415	9.43904	10.56045	38		
	9.42415	9.98412	9.44003	10.55996	36		
25	9.42461	9.98408	9.44052	10.55947	35		
21	9.42507	9.98405	9.44102	10.55897	34		
27	19.42552	9.98401	9.44151	10.55848	33		
28	17.エーフラー	9.98398	9.44200	10.55799	32		
30	9.42644	9.98394	9.44249	.10.55750	31		
1-	9.42689 Cosine.	9.98391 Sine.	9.44298	10.55701	30		
-		oine.	Cotang.	Tangent.	2		
1 1	105 74 Degree						

5-

	El 15 Degrees. 164					
Sine.	Cosine.	Tangent.	Cotang.			
30 9.42689	9 9 3 3 9 1	9.41298	10.55701	30		
31,9-42735	9.98387	9.44347	10.55652	20		
32 9.42780	9.98384	9.44396	10.55603	28		
33 9.42826	9.98380	9.44445	10.55554	27		
34 9.42871	9.98377	9.44494	10.55505	26		
35 9.42917	9.98373	9.44543	10.55456	25		
36 9.42962	9.98369	9.44592	10.55407	24		
37 9.43007	9.98366	9.44641	10.55358	23		
38 9.43052	9.98362	9.44689	10.55310	22		
39 9.43097	9.98359	9.44738	10.5526!	21		
40 9.43 142	The second name of the local division in which the local division is not a second name of the local division in the local division is not a second name of the local division in the local division is not a second name of the local division i	1				
41 9.43187	9.98352	9.44835	10.55164	18		
42 9.43232 43 9.43277	9.98345	9.44932	10.55067	17		
44 9.43322	9.98341	9.44981	10.55018	16		
4: 9.43367	9.98338	9 45029	10.51970	15		
46 9.43412	9.98334	9 45 - 77	10.54922	14		
47 9.43456	9.98330	9.45126	10.54873	13		
48.9.43501	9.98327	9.45174	10.54825	12		
45 9.43546	9.98322	9-45222	10.54777	11		
50 9.43 590	9.08120	9.45200	10.54729	10		
51 9.43035	9.98316	9-45318	10.54681	0,00		
52 9.43679	9.98313	9.45366	10.54633	8		
53 9.43724	9.98309	9.45414	10.54585	7		
549.43768	9.98305	9.45462	10.545 7	6		
55 9.43812	9.98302	9 45 (10)	10.54489	_5		
55 9.43857	9.98293	9 45558	10.54441	4		
57 9.43901	9.98295	9.45000	10.54393	3		
58 9.43945	9.98291	9.45654	10.54298	2		
599.43989 609.440°3	9.98284	9.45739	10.54250	0		
	Sine.	Cotang	Canotat.	N		
Cofine.	othe.	· anung		durant [
105 74.Digress.						

3 16 Degr	ces.		1 1 1	63
Sine.	Cofine.	Tangent.		
0 9.41033	9.98284	9.45749	10.54250	60
1 9.44077	9.98280	9.45797	10.54202	59
2 9.44121	9.98276	9.45844	10.54155	58
39.44165	9.98273	9.45892	10.54107	57
59.44253	9.98266	9.45987	10.54012	55
69.44297	9.98262	9.46034	10.53965	-
79.44341	9.98258	9.46082	10.53917	53
89.44384	9.98255	9.46129	10.53870	52
99.44428	9.98251	9.46176	10.53823	51
109.44471	9.98247	9.46224	10.53775	50
119.44515	9.98244	9.46271	10.53728	49
139.44502	9.98236	9.46365	10.53681	47
149.44645	9.98233	9.46412	10.53587	46
15 9.44689	9.98229	9.46459	10.53540	45
16 9.44732	9.98225	9.46506	10.53493	44
179.44775	9.98222	9.46553	10.53446	43
189.44819	9.98218	9.46600	10.53399	42
199.44862	9.98214	9.46647	10.53352	41 40
21 9.44948	9.98207	9.46741	The second secon	39
22 9.44991	9.98203	9.46788	10.53258	38
23 9.45034	9.98199	9.46834	10.53165	37
249.45077	9.98196	9.46881	10.53118	36
25 9.45120	9.98192	9.46928	10.53071	35
26 9.45 163	9.98188	9.46974	10.53025	34
27 9.45 206 28 9.45 248	9.98184	9.47021	10.52978	33
29 9.45 291	9.98181	9.47067	10,52932	32
309.45331	9.98173	9.47160	10.52839	30
Cofine.	Sine.	Cotang.	Tangent.	Z
106			73 Degre	265.

M	16 Deg	rees.		1	63.
11.	Sin.	Cofine.	Tangent.	Colang.	
30	9.45334	9.98173	9.17160	10.52839	30
31		9.98165	9.47206	10.52793	29
	9.45419	9.9816t	9-47253	10.52746	28
	9.45461	9.98162	9.47299	10.52700	27
	9.45504	9.98158	9.47345	10.52608	25
all transfer	9.45589	9.98151	9.47438	10.52501	24
37	9.45631	9.98147	9.47484	10.52515	23
138	9.45673	9.98143	9.47530	10.52469	22
39	9.45710	9.98139	2.47576	10.52423	21
	9.45755	9.98136	9.47622	10.52377	20
	9.4580C	9.98132	9.47668	10.52331	18
	9.45842	9.98128	9.47714	10.52285	17
	9.45926	9.98120	9.47805	10.52194	16
45	9.45968	9.98117	9.47851	10.52148	15
	9.46010	9.98113	9.47897	10.52102	14
47	9.46052	9.98109	9.47943	10.52056	13
	9.46094	9.98105	9 47988	10.52011	12
	9.46136	9.98101	9.48034	10.51965	II
	9.46178	9.98008		10.51919	
51	9.46219	9.98094	9.48125	10.51828	9
52	9.46303	9.98086	9.48216	10.51783	1
54	9.46344	9.98082	9 48262	10.51737	7 6
55	9.46386	9.98078	9.48307	10 5 1 6 9 2	5
56	9.46427	9.98075	9.48352	10.51647	4
157	9.46469	9.98071	9.48398	10.51601	3
	9.46510	9.98067	9.48443	10.51556	2
	9.46552	9.98063	9.48533	10.51466	0
-	Cosine.	Sine.	Cotang.	Tangent.	Z
-	106		0	73 Degrees	

in. 0	Sine.				
		1 Cosine.	Tangent.	Cetang.	
-).40703	9.98059	9.48532	10.51406	UC
1	1.46634	9.98055	9.48579	10.51420	59
	9.46676	9.98051	9.48624	10.51375	58
	9.46717	9.98048	9 48 69	10.51310	57
32	9.46758	9.98044	9.407.4	10.51240	55
6	-	9.98036	9.48504	10.51195	54
7	9.46881	9.98032	9.48849	10.51150	53
	9.46922	9.98028	9.48894	10.51105	52
	9.46963	9.98024	9.48938	10.51061	51
8	9.47004	9 98020	9.48983	10.51016	50
11	9.47045	9.98010	9.49028	10.50971	49
	9.47127	9.98009	9.49073	10.50881	48
14		9.98005	9.49162	10.50837	46
15	0.47208	9 98001	9.49207	10.50792	45
16	9.47249	9.97997	9.49251	10.50748	44
17	9.47289	9.97993	9.49256	10.50703	43
18 1¢:	11133-	9.97989	9.49340	10.50659	42
20	3.47370 3.47411	9.97985	9.49385	10.50514	41
-	9.47451	9.97977	9.49474	10.50525	39
22	9.47492	9.97977	9 49518	10.50481	38
23	9.47532	9.97969	9.49562	10.50437	37
24	3.47573	9.97955	9.49607	10.50392	36
25).47613	9.07961	9.406;1	10.50348	35
26).47653	9.97957	9.49095	10.50304	34
18).47 ⁶ 93).47 ⁷ 33	9.97953 9.97949	9.49739	10.50260	33
25	3.47774	9.97949	9.49828	10.50171	31
30	1.47814	9.97941	0.49872	10.50+27	3
	Cosine.	Sinc.	Cotung.	Tangent.	N
1	107			72 Degrees	

N	17 Deg	rees.		· 162	_1
4.	Sine	Cosine.	Tangent.	Cotang.	
30	9.47814	7.97941	9.49872	10.50127	31
-	9.47854	9 97937	5.19916	10.50083	29
	9.47894	9.97933	9.49960	10.50039	28
173	0.47934	9.97929	9.50004	10.49995	27
	9 47974	9 97925	9.50048	10.49951	25
-	9.43014	3 97921	0.50092		24
156		9.57917	9.50135	10.49864	23
	9.48093	9.97913).50223	10.49776	22
	19.48133	9.97905	9.50267	10 49732	21
	9.48212	2.97901	9.50310	10.49689	20
	9.48252		9.50354	10.49645	1.9
	9.48292	9.97893	9.50398	10.49601	18
43	19 48331	9.97889	9.50441	10.49558	17
144	19.48371	19.97885	9.50485	10.49514	16
45	9.48410	9.97881	9.50528	10.49471	15
4.6	9.48450	9.97877	9.50572	10.49427	14
	9.48489		9.50615	10.49384	
48	3 9.48528	9.97869	9.50659		1 1
49	9.48568	9.97865	9.50746	10.49253	1 10
-	9.48607		9.50789		
5	9.48646	9.97857			9
5					
5:			9.50919	10.49080	
5	00	9.97841		10.49037	
5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5			9.51005	10.4899	1 4
5		1 9.97832	9.51048	3 10.4895	1 3
5	8 9.48920	9.97828	3 9.51091	10.4890	8 2
5	919.48959	9.97824	1 19.51134	10.4886	5 1
6	0 9.4899	8 9.97820			
1	Cofine.	Sine.	Cotang	72 Degr	The same of the sa
1	:07			72 10087	C. C. C.

199,49730 9.97741 9.51988 10.48011 41 200,40768 9.97737 9.52030 10.47969 40 219,40806 9.97733 9.52072 10.47927 39 229,49844 9.97729 9.52115 10.47884 38 259,49882 9.67725 9.52157 10.47842 37 249,49920 9.97720 9.52196 10.47800 36	N	18 Deg	rees.		161	_
1	171.	Sine.	Cofine.	Tangent.	Cotang.	
1	C	.48998	9.97820	9.51177	10.48822	60
3 9.49114 9.97808 9.5130b 10.48650 56 4 9.49153 9.97804 9.51349 10.48650 56 5 9.20102 9.97800 9.51392 10.48607 55 ().49230 9.97795 9.51434 10.48505 54 7 9.49269 9.97791 9.51477 10.48522 53 10.49346 9.97783 9.51563 10.48479 52 6 9.49346 9.97783 9.51563 10.48436 51 10 9.49423 9.97775 9.51605 10.48304 50 11 9.49423 9.97775 9.51648 10.48351 49 12 9.496462 9.97771 9.51690 10.48309 48 13 9.49500 9.97760 9.51733 10.48266 47 14 9.49538 9.97762 9.51770 10.48223 46 15 9.49615 9.97754 9.51818 10.48181 45 17 9.49653 9.97750 9.51961 10.48138 44 17 9.49653 9.97754 9.51861 10.48138 44 17 9.49691 9.97746 9.51945 10.48064 43 18 9.49691 9.97740 9.51945 10.48064 43 19 9.49691 9.97740 9.51945 10.48064 43 19 9.49691 9.97737 9.52030 10.47969 40 20 9.49730 9.97741 9.52030 10.47969 40 21 9.40806 9.97737 9.52195 10.47969 40 22 9.49844 9.97729 9.52115 10.47884 38 24 9.49820 9.97720 9.52195 10.47884 38 25 9.49882 9.97725 9.52157 10.47884 38	1	9.49037	9.97816			59
4 9.49153 9.97804 9.51349 10.48656 56 56 5.20102 9.97800 9.51392 10.48607 55 10.49230 9.97795 9.51477 10.48505 54 10.49230 9.97787 9.51520 10.48479 52 10.49346 9.97783 9.51563 10.48479 52 10.49345 9.97779 9.51605 10.48304 50 11 9.49423 9.97775 9.51605 10.48304 50 11 9.49423 9.97775 9.51606 10.48309 48 12 9.49500 9.97766 9.51733 10.48266 47 12 9.49538 9.97762 9.51733 10.48266 47 10.48573 9.97754 9.51818 10.48181 45 10.48011 41 10.49653 9.97754 9.51818 10.48138 44 17 1.49653 9.97754 9.51965 10.48096 43 10.4			1		. , ,	2 1
5 3.20102 9.97800 9.51392 10.48607 5.5 ().49230 9.97795 9.51434 10.48505 54 7 3.49269 9.97791 9.51477 10.48522 53 3.49308 9.97787 9.51520 10.48479 52 9.49346 9.97783 9.51563 10.48436 51 10 492×5 9.97779 9.51605 10.48304 50 11 9.49423 9.97775 9.51648 10.48351 49 12 9.49462 9.97771 9.51690 10.48309 48 13 9.49500 9.97766 9.51733 10.48266 47 14 9.49538 9.97762 9.51733 10.48266 47 15 9.49657 9.97758 9.51818 10.48181 45 17 9.49653 9.97759 9.51818 10.48181 45 17 9.49653 9.97750 9.51993 10.48096 43 16 9.49601 9.97740 9.51945 10.48091 41 16 9.49015 9.97754 9.51988 10.48011 41 17 9.49653 9.97754 9.51988 10.48011 41 19 9.49730 9.97741 9.51988 10.48011 41 20 0.40768 9.97737 9.52030 10.47969 40 21 9.40806 9.97733 9.52072 10.47969 40 21 9.40806 9.97729 9.52115 10.47884 38 25 9.49882 9.97725 9.52157 10.47884 38 26 9.49882 9.97729 9.52195 10.47884 38 26 9.49882 9.97729 9.52195 10.47884 38						
().49230	1	1 2 2 -			01	- 1
7 3.49269 9.97791 9.51477 10.48522 53 3.49308 9.97787 9.51520 10.48479 52 5.249346 9.97783 9.51563 10.48436 51 10.949423 9.97775 9.51668 10.48394 50 11.949423 9.97775 9.51690 10.48394 48 12.949462 9.97771 9.51690 10.48399 48 13.949500 9.97766 9.51733 10.48266 47 14.949538 9.97762 9.51770 10.48223 46 15.949677 9.07758 9.51818 10.48181 45 16.949615 9.97754 9.51861 10.48181 45 17.249653 9.97750 9.51963 10.48096 43 18.949601 9.97746 9.51945 10.48064 43 18.949601 9.97746 9.51945 10.48064 43 19.49648 9.97737 9.52030 10.47969 40 20.40768 9.97737 9.52030 10.47969 40 21.940806 9.97733 9.52072 10.47969 40 22.949844 9.9729 9.52115 10.47884 38 23.949882 9.57725 9.52157 10.47884 38 24.949920 9.97720 9.52196 10.47800 36			-	THE RESIDENCE AND ADDRESS OF THE PARTY NAMED IN		men,
\$\begin{array}{c}						
\$\begin{array}{c}						1
11 9.49423 9.97775 9.51648 10.48351 49 12 9.49462 9.97771 9.51690 10.48309 48 13 9.49500 9.97766 9.51733 10.48266 47 14 9.49538 9.97762 9.51770 10.48223 46 15 9.49577 9.07758 9.51818 10.48181 45 16 9.49615 9.97754 9.51861 10.48138 44 17 9.49653 9.97750 9.51963 10.48096 43 18 9.49691 9.97746 9.51945 10.48054 42 19 9.4963 9.97737 9.52030 10.47969 40 21 9.40806 9.97737 9.52030 10.47969 40 21 9.40806 9.97737 9.52195 10.47884 38 22 9.49844 9.97729 9.52115 10.47884 38 23 9.49882 9.57725 9.52157 10.47884 38 24 9.49920 9.97720 9.52195 10.47800 36		2.49346			, , , ,	
12 9.49462 9.97771 9.51690 10.48309 48 13 9.49500 9.97766 9.51733 10.48266 47 14 9.49538 9.97762 9.51776 10.48223 46 15 9.40577 9.97754 9.51818 10.48181 45 16 9.49615 9.97754 9.51961 10.48086 43 18 9.49691 9.97740 9.51945 10.48064 42 19 9.49730 9.97741 9.51988 10.48014 41 2c 0.40768 9.97737 9.52030 10.47969 40 21 9.40806 9.97733 9.52115 10.47884 38 22 9.49844 9.97729 9.52157 10.47884 38 23 9.49882 9.97725 9.52157 10.47882 37 24 9.49920 9.97720 9.52195 10.47800 36	IC	9 49285	9.97779			50
13 9.49500 9.97766 9.51733 10.48266 47 14 9.49538 9.97762 9.51770 10.48223 46 15 9.49577 9.07758 9.51818 10.48181 45 16 9.49615 9.97754 9.51861 10.48138 44 17 9.49653 9.97750 9.51903 10.48096 43 18 9.49691 9.97746 9.51945 10.48054 42 19 9.49730 9.97741 9.51988 10.48011 41 2c 0.40768 9.97737 9.52030 10.47969 40 21 9.42806 9.97737 9.52030 10.47969 40 21 9.42806 9.97739 9.52115 10.47884 38 22 9.49844 9.97729 9.52115 10.47884 38 23 9.49882 9.57725 9.52157 10.47880 36				9.51648	10.48351	
149.49538 9.97762 9.51770 10.48223 46 159.49577 9.07758 9.51818 10.48181 45 169.49615 9.97754 9.51861 10.48188 44 179.49653 9.97750 9.51903 10.48096 43 189.49691 9.97746 9.51945 10.48054 42 199.49730 9.97741 9.51988 10.48011 41 2c 0.40768 9.97737 9.52030 10.47969 40 219.40806 9.97733 9.52072 10.47927 39 229.49844 9.97729 9.52115 10.47884 38 259.49882 9.97725 9.52157 10.47842 37 249.49820 9.97720 9.52196 10.47800 36			9.97771	9.51090		
15 9.49517 9.97758 9.51818 10.48181 45 16 9.49615 9.97754 9.51861 10.48138 44 17 9.49653 9.97750 9.51903 10.48096 43 18 9.49691 9.97746 9.51945 10.48054 42 19 9.49730 9.97741 9.51988 10.48011 41 2c 0.40768 9.97737 9.52030 10.47969 40 21 9.40806 9.97733 9.52072 10.47927 39 22 9.49844 9.97729 9.52115 10.47884 38 25 9.49882 9.57725 9.52157 10.47884 38 24 9.49920 9.97720 9.52195 10.47800 36	1 -	9.49500		9.51733		
16 9.49615 9.97754 9.51861 10.48138 44 17 9.49653 9.97750 9.51903 10.48096 43 18 9.49691 9.97746 9.51945 10.48054 42 19 9.49730 9.97741 9.51988 10.48011 41 2c 0.40768 9.97737 9.52030 10.47969 40 21 9.40806 9.97733 9.52072 10.47927 39 22 9.49844 9.97729 9.52115 10.47884 38 25 9.49882 9.97725 9.52157 10.47842 37 24 9.49920 9.97720 9.52195 10.47800 36				9.51818		2 1
17	-		-			
18 9.49691 9.97746 9.51945 10.48054 42 19 9.49730 9.97741 9.51988 10.48011 41 2c 0.40768 9.97737 9.52030 10.47969 40 21 9.40806 9.97733 9.52072 10.47927 39 22 9.49844 9.97729 9.52115 10.47884 38 23 9.49882 9.97725 9.52157 10.47882 37 24 9.49920 9.97720 9.52195 10.47800 36	17	7.49653				
2c 0.40768 9.97737 9.52030 10.47969 40 21 9.40806 9.97733 9.52072 10.47927, 39 22 9.49844 9.97729 9.52115 10.47884 38 25 9.49882 9.57725 9.52157 10.47842 37 24 9.49920 9.97720 9.52195 10.47800 36	IS	19.49591				42
219.40806 9 97733 9.52072 10.47927 39 22 9.49844 9 97729 9.52115 10.47884 38 25 9.49882 9.57725 9.52157 10.47842 37 24 9 49920 9.97720 9.52195 10.47800 36						
22 9.49844 9 97729 9.52115 10.47884 38 25 9.49882 9.57725 9.52157 10.47842 37 24 9 45920 9.97720 9.52195 10.47800 36	-	-		-		40
23 9.49882 9.97725 9.52157 10.47842 37 24 9 49920 9.97720 9.52199 10.47800 36						39
24 9 49920 9.97720 9.52199 10.47800 36						-
					10.47800	1
	25	9.49958	9.97716	9.52241	10.77758	35
				The Person Name and Address of		34
2. 9.50034 19.97708 9.52325 10.47674 33		9.50034			10.47674	33
28 9.50072 9.97704 9.52367 10.47632 32		9.50072	1 1	1	10.47632	32
	29	9.50109		1		31
	30		1	SECTION SERVICES		30
Cofine. Sine. Cotang. Tangent. 2	1_		Sine.	Cotang.		_

Z	18 D.g	rrees.		10	1
in.	Sin .	Cofin	Tangent.	Cotang.	_
30	9.50147	9.97695	9.52451	19.47548	30
	9.50185	9.97691	9.52493	10.47506	29
32	9.50223	9 97687	9.52535	10.47464	28
33	9.50260	9.97682	9.52577	10.47422	27
34	9.50298	9.97678	9.52661	10.47338	2.5
35	9.50335	9.97670	9.52703	10.47296	24
30	9.50373	9.97070	1.52745	10.47254	23
38	9.50448	9.97661	9.52786	10.47213	22
39	9.50485	9 97657	9.52828	10.47171	21
40	9.50523	9.97653	9 52870	10.47129	20
41	9.50560	9.97648	9.52911	10.47088	19
42	9.50598	9.97644	9.52953	10.47046	18
43	9.50635		9.52995	10.47004	17
44	9.50672	9.97631	9.53036	10.46921	15
1	9.50709			10.46880	14
40	9.50747	9.97627	9.53119	10.46838	13
	9.50821	9.97618	9.53202	10.46797	12
10	9.50858	9.97614	9.53243	10.46756	11
50	9.50895	9.97610	9.53285	10.46714	10
	9.50932	9.97605	9.53326	10.46673	9
52	9.50959	9.97601	9.53367	10.46632	8
53	9.51005	9.97597	9.53409	10.46590	7 6
54	9.51043	9 97593	9.53450	10.46549	5
	9.51080	9.97588	9.53491	10.46467	(Barro
	9.51117	9.97584	9.53532 9.5 35 73	10.46426	4 3
57	9.51153	9.97580			2
50	9.51227	9.97571	9.53656	10.46343	I
60	9.51264		9.5 697		0
1	Cofine.	Sine.	Cotang.	Tangeut.	X
	108		on the majories	71 Degrei	s.

N	19 Deg	rees.		160
11.	Sine.	Cosine.	Tangent.	Cotang.
0	9.51264	9.97567	9.53697	10.40302 60
	9.51300	9.97562	9.53738	10.46261 59
	9.51337	9.97558	9.53779	10.46220 58
	9.51374	9.97553	9.53820	10.46179 57
	9.51447	9.97545	9.53902	10.46098 55
-	9.51483	9.97540	9.53942	10.46057 54
7	9.51520	9.97536	9.53983	10.46016 53
	9.51556	9:97532	9.54024	10.45975 52
	9.51593	9.97527	9.54065	10.45934 51
<u>-</u> 11	9.51665	9.97518	9.54146	20 4 70 7 7
8	9.51701	9.97514	9.54187	10.45812 48
	9.51738	9.97510	9.54228	10.45771 47
14	9.51774	9.97505	9.54268	10 45731 46
	9.518:0	9.97501	9.54309	10 45690 45
1 -	9.51846 9.51882	9.97496	9.54349	10 17600 77
IS	9.51919	9.97488	9.54431	10.45569 43
	9.51955	9.97483	6.54471	10.45528 11
20	9.51991	9.97479	9.54511	10.45488 40
	9.52027	9.97474	9.54552	10.45447 39
	9.52063	9.97470	9.54592	10.45407 38
	9.52134	9.97461	9.54673	10.45326 37
	9.52170	9.97456	9 54713	10.45286 35
25	9.52206	9.97452	9.54754	10.45245
27	9.52242	9.97448	9.54794	10.45205 22
	9.52278	9.97443	9·54834 9·5 4 874	10.45165 32
	9.52313	9.97434	9.54914	TO AFORE 13"
-	Cofine.	Sine.	Cotang.	Tangent. 30
11	109			70 Degrees.

				160 f	
M	19 Degr				
7.	Sino. 1	Coline.	Tangent.	Cotung.	
30	9.52144	9.97434	9.54911	10.45085 30	
31	9.52,85	9.97430	9.54935	10.45045.29	
32	9.52420	9.97425	9.54975	10.45004 28	
33	9.52456	9.97421	9.55035	10.44904 27	
34	9.52491	9.97416	9.55075	10.44924.26	
35	9.52727	9.97412	9.55115	10.4 1884 25	
30	9 52502	9 97407	9.55155	10.44844 24	
137	19.52598	9.97403	9.55195	10.44804 23	
138	9.52632	9.97398	9.55 35	10.44.764.22	
39	9.52669	9.97394	9 55275	10.44724 21	
10	9 52-04	9.97389	9.55214		
41	9 52739	9 97385	9.55354	10.4645 19	
42	19.52775	9 97380	9.55394	1 1	
43	19.52010	9.97376	9.55434	10.44525 16	
144	9 520 +5	9.67371	9.55474	10.44186115	
15	9.52830	9.9736-			
46	19.52,10	9.97302	9-3553	10.44415 14	
147	9.5295.1	9.07358	19.55593	10.44357 12	
48	9.52986	9-97353	9.55672	10.44327111	
49	9.53021	9.97344	9 55712	10.44287:10	
50	9.53056			10.412;8; 9	
151	9.53091	9.97339	19.55751	10.41208 8	
52	9.53125	9.97330	19.55830	10.4+169 7	
53	9.53195	9.97326	9.55870	10.44120 6	
54	9.53190	10.17341	19.55909	10.4:095 5	
-		9.47310	19.55949	10.44050 4	
50	9.53260	9.97312	9.55988	10.44011 3	
57 58	9.53335	9.97307	9.56027	10.43972 2	
59	9.53370	9.97303	9.56067	10.43932 1	
60	9.53405	19.97298	9.56106	10.43893 0	
	C. tone.	Sine.	Cotans.	Ting t. S	
-				70 : egres.	
109					

N	20 Degrees. 159				
in.	Siue.	Cofine	Tangent.	Cotang.	
0	9.53405	9 97298	9.56106	10.43803	60
-	9.53439	9.97293	9.56145	10.43854	55
	9.53474	9.97289	9.56185	10.43814	58
3	9.53509	9.97284	9.56224	10.43775	57
4	9.53543	9.97280	9.56263	10.43736	56
5	9.53578	9.97275	9.56302	10.43697	55
6	9 53612	9 97270	9.56341	10.43658	54
7	17.77.11	9.97266	9.56381	10.43618	53
2	9.53681	9.97261	9.56420	10.43579	52
	9.53716	9.97257	9.56459	10.43540	51
Name of Street	9.53750	9.97252	9.56498	10.43501	50
II	9 53785	9.97247	9.56537	10.43462	49
	9.53819	9 97243	9.56576	10.43423	48
	9.53853	9.97238	9.56615	10.43384	47
	9 53888	9.97233	9.56654	10.43345	46
-	9.53922	9 9-229	9.56693	10.43306	45
	9.53956	9.97224	9.56732	10.43207	44
	19,53990	9.97219	9.56770	10.43229	43
	9.54024	9.97215	9.56809	10.43190	42
	9.54059	9.97210	9.56848	10.43151	41
	9.54003	9.97275	9 56887	10.43112	40
21	1/ / 1 -/	9.97201	9.5692:	10.43073	35
	9.54161	9.97199	9.56964	10.43035	38
	39.54195	9.97191	9.57003	10.42996	37
	19.54229	9.97187	9.57042	10.42957	36
-	9.54263	9.97182	9.57080	10.42010	35
	9.54297	9.97177	9.57119	10.42880	34
	79.54331	9.97172	9.57158	10.42841	33
	9.54364	9.97168	9.57196	10.42803	32
	9.54398	9.9716;	9.57235	10.42764	31
2	-	-	1		30
1_	Cosine.	1. Sine.	Cotang.	Tangent.	$\overline{\Sigma}$
1.10 · 69 Degrees.					

Min	20 Deg	rees.		1(0)
77	Sine.	Coline.	Tangent.	Cotang.
130	9.54432	9.97158	9-57273	10.42726 30
3,1	9.54466	9.97154	9.57312	10.42687 29
32	9.54500	9.97149	9-57350	10.42649:28
33	9 54533.	9.97144	9.57389	10.42610 27
34	9.54567	9.97139	9.57427	10.42572 25
35	9.54601	9.97135	9.57466	10.42533 25
36	9.54634	9.97130	9.57504	10.42495 24
37	9.54668	9.97125	9.57542	10.42457 23
39	9.54735	9.97116	9.57619	10.42418 22
40	9.54768	9.97111	9.57657	10.42342 20
41	9.54802	9.97106	9.57695	10.42304 19
12	9.54835	9.97101	9.57734	10.42265 .18
43	9.54869	9.97097	9.57772	10.42227 17
44	9.54902	9.97092	9.57810	10.42189 16
45	9,54936	9.97087	9.57848	10.42151 15
46	9.54969	9.97082	1	10.42113 14
47	9.55002	9-97077	9.57924	10.42075 13
48	9.55035	9.97073	9.57962	10.42037 12
49	9.55069	9.97068	9.58000	10.41999 11
	9.55102	9.97063		
51	9.55135	9.97058	9 58076	10.41923 9
53	9.55168	9.97053	9.58152	10.41885 8
54	9.55234	9.97044	9.58190	10.41809 6
:55	9.55268	9.97039	9.58228	10.41771 5
56	9.55301	9.97034	9.58266	10.41733 4
57	9.55334	9.97029	9.58304	10.41695 3
58	9.55367	9.97024	9.58342	10.41657 2
59	9.55399	9.97020	9,58379	10.41620 1
60	9.55432	9.97015	9.58417	10.41582
	Cofine.	Sine.	Cotang.	. Tangent. \
1 1	10		6	9 Degrees.

Min	21 Degr	ees.	· Kingin	1	58 [
ui	Sine.	Cofine.	lie.	Cotung.	
C	1.55432	9.97015	9.58417	10.41582	60
]	7.55465	9.97010	9.58455	10.41544	59
	9 55498	9.97005	9 58493	10.41506	58
3	9 55531	9.97000	9.58530	10.41469	57
4 5).55564	9.96995	9.58568	10.41431	56
-	9.55597	-		10.41393	55
1	1.55629	9.91 986	9.58643	10.41356	54
7 8	3.55662	9.96981	9.58681	10.4.1318	53 52
C	7.55095	9.96971	9.58756	10.41243	51
IC	9.557(0	9.96966	9.58794	10.41205	50
II).55793	9.46901	9.58831	10.41168	42
,	9.55825	9 95956	9.58869	10.41130	48
	9.55853	9.96951	9.58906	10.41003	47
I	9.55890	9.95946	9.58944	10 41055	46
15	9.55923	0.96041	9 58081	10.41018	45
	9.55955	9.96937	9.59018	10.40981	44
17	9.55988	9.96932	9.59056	10.40943	43
	9.56020	9 96927	9.59093	10.40905	42
20	9.56085	9.95922	9.59130	10.40869	41
-		9.96917	9.59168	10.40831	40
21	9.56117	2.96912	9.59205	10.40794	39
23	9.56150	9.96907	9.59242	10.40757	38
-	9.56214	9.96902	9.59279	10.40720	37 36
	9.56246	9.96892	9.59354	10.40645	35
-	9.56279	9.96887	9.59301	10.40008	
1	9.56311	9.96882	9.59428	10.40571	34 33
	9.56343	9.96877	9.59465	10.40534	32
20	9.56375	9.96872	9.59502	10.40497	31
13°	9.56407	9.96867	9.59539	10.40450	30
	Coline.	Sine.	Cyline.	Tangent.	N
11	t I			68 Degree	. ~~ .

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13	21 Dr	arrees		C - C - 15	0
lin.	Sine.	Cofine.	Tangent.	Cotang.	1
30	9.56407	9.96807	9-59539	10.40400	30
Described	9.56439	9.90862	9.59576	10.40423	-
	9.56471	9.96857	9.59570	10.40386	29
		9.96852	9.59650	10.40349	27
34	9.56535	9.96847	9.59687	10.40312	26
	9.56567	9.96842	9.59724	10.40275	25
	9.56599	9.96837	9.59761	10.40238	24
	9.56.631	9.96832	9.59798	10.40201	23
	9.56663	9.96827	9.598-35	10 40164	22
10	9.56595	9.96822	9.59872	10.40127	21
	9.56758	9.96812	Projection of Designation of the	10.40000	20
12	9.56790	9.96807	9.59945	10.40054	19
43	9.56822	9.96802	9.60019	10.39980	17
.14	9.56853	9.95797	9.60056	10.39943	16
45	9.56885	9.06792	9.60002	10.39907	15
.16	9.56917	9.96787	9.60129	10.39570	14
	9.56948	9.96782	9.60166	10.39833	13
48	9.56980	9.95777	9.60202	10.39797	12
	9.57012	9.95772	9.60239	10.39760	11
	9.57043		9.60276	10.39723	10
	9.57075	9.96752	9.60312	10.39087	9
52	9.57138	9.96752	9.60349	10.39650	_
54	9.57169	9.95747	9.60422	10.39577	. 6
	9.57200	9.96742	9.60458	10.39541	5
56	9-57232	9.96736	9.60495	10.39504	4
157	9.57263	9.96731	9.60531	10.39468	3
	9.57294	9.96725	9.60568	10.39431	2
	9.57326	9.96721	9.60604	10.39395	I
1	9-57357	9.96716	9.60640	10.30359	-
-	Cosine.	Sine.	Cotang.	Tangent.	Z
I	11		-	68 Degre	25.

Min	22 Degr	ees.		1	7
101	Sine.	Cosine.	langent.	Cotang.	
C	1.57357	9.95716	9.00040	10.30359	60
1).57388	9.90711	9.60677	10.39322	59
2	3 57420	9.96706	9.60713	10.39286	58
3	9.57451	9.96701	9.60749	10.39250	57
4	9.57482	9.96696	9.60786	10.39213	56
5	1.57513	9.96691	9.50822	10.39177	<u>55</u>
(9.57544	9.96685	9.60858	10.39141	54
1 8	7.57575	9.96680	9.60895	10.39104	53 52
ξ	7.57637	9.96670	9.60967	10.39032	51
1C	9.57668	9.96665	9 61003	10.38996	50
II).57699	9.96560	9.61039	10.38960	49
12	9.57730	9 96655	9.61075	10.38924	48
13	9.57761	9.96649	9.61111	10.38888	47
14		9.96644	9.61148	10.38851	46
15	7 57823	9.06630	0.61184	10.38815	45
16	9.57854	9.96634	9 01220	10.38779	44
17	9.57885	9.96629	9.61256	10.38743	43
	9.57916	9.96524	9.61292	10.38707	42
1 g	9.57946	9.96618	9.61328	10.38671	41
-	9.57977	9.96613	9.61364	10 38635	40
21	7.58008	9.96008	9.01400	10.38000	39
22	9.58039	9.96603	9.61435	10.38564	38
24	9.58100	9.96598	9.61471	10.38528	3.
	0.58131	9.96587	9.61543	10.38456	35
	9.58161	9.96582	9.61579	10.38420	34
) 1	9.58192	9.96577	961615	10.38384	33
	9.58222	9.96571	9.616;0	10.38349	32
29	9.58253	9.96566	9.61686	10.38313	31
30	9.58283	9.96561	9.61722	10.38277	30
	(ofine.	Sine.	Cotang. 1	'l'angent.	S
L	12			67 Degree	5.

12	22 D	greis.			5.7
Min.	Sine.	Cosine.	Tangent.	, Crang.	*/
30	9.58283	9.90501	9.61722	10.3827	730
	9.58314	9.90556	9.01758	-	
	9 58344	9 95551	9 61 793	10. 820	
33	9.58375	9.96545	9.61829	10.3817	
	9.58405	9.95540	9.61865	10.4813	-
- Continue	9.58436	9.96535	9.6100)	10.3809	1 1
3t-	9.58400	9.95530	9.61936	10.3800	
3/	9.58496	9.96524	9.61972	10.3802	
30	9.58557	9.96514	9.62043	10.3795	
40	9.58:87	9.96508	9.62078	10.3792	
	9.58617	9.96503	9.62114	10.3788	5 19
42	9.58648	9.96498	9.62149	10.3785	018
13	9.58678	9.96493	9.62185	10.3781	
44	9.58708	9.96487	9.62220	10.3777	
	9.58738			10.3774	-
40	9.58768	9.90477	9.62291	10.3770	
48	9.58828	9.96466	9.62362	10.3763	
49	9.58858	9.96461	9.62397	10.3760	
50	9.58888	9.96456	9.62432	10.3756	710
	9.58918	9.96450	9.62468	10.3753	1 9
	9.58948	9.96445	9.62503	10.37496	
	9.58978	9.96440	9.62538	10.3746	
	9.59008	9.96434	9.62574	10.37429	
	9.59038	-	9.02044	10.3735	1
7	9.59068	9.96424	9.62679	10.37320	
	9.59128	9.96413	9.62714	10.3728	
	9.59158	9.96407	9.62750	10.37249	I
	9.59187	9.96402	9.62785	10.3721	0
	Cofine.	Sine.	Cotung.	Tangent.	
L	112		(67 Degree.	5.

112	23 Dig	rees.		156	
11.	Sine.	Cofine.	Tangent.	Cotano.	
C	9.59187	9.96402	9.62785	10.37213	20
1	9.59217	9.96397	9.02820	10.37179	50
2	1 21 10 1	9.96391	9.62855	10.37144	58
3	1	9 95385	9.62925	10.37109	57
4	1 , , , ,	9.663-5	0.52960	10.37034	3
1-		9 96370	9.62995	10.37001	51
-	9.59395	9.56364	9.63030	10.36969	5.3
1	9.59425	9.95359	9.63065	10.36934	5-
	9.59454	9.96354	9.63100	10.36 97	5.
10		9.66348	903:35	10.0004	5
	9.59513	9.90343	9.63170	10 36829	49
3	9.59543	9.95337	9.63205	10.36794	4
1	9.59572	9.96332	9.63240	10.36724	45
	9.59631	9.96321	9.63309	10.36690	45
-	9.59660		9.63344	10.36655	44
I	79.59690	9.96310	9.63379	10.36620	43
	9.59719		9.63414	10.36585	42
	99.59748		9.63449	10.36550	41
2	- 1 3 / / /	9.96294	9.63483	10.36516	40
2	11 27 1	9.96289			39
2	² 9.59836 3 9.59866			10.36446	38
2				10.36377	37
2					35
2	9.59953	9.95201	9.63691	10.30308	3.
2	1.59982	9.96256	9.63726	10.36273	33
2	1.	9.96250	9.63761	10.36238	32
	9 : .60040	1 / / "		10.36204	31
12	0.6006		-		30
L	Cofine.	Sine.	Gotang.	Tangent.	Z
1	113			66 Degrees	in I

M:	23 De.			156.	-
77.	Sine.	Cofine.	Tangent.	Chang.	
30	9.60069	9.96239	9.63830	10.36169.30	
	9.60099	9.90234	9.6386+	10.36135 20	
	9 60128	9 95228	9.63899	10.36100 2	
	0.60157	9.96223	9.63933	10.36065 2	/ 2
	9.60186	9.95217	9.63968	10.460312	- 3
-	9.60213				
	9.60272	9.95200	9.64037	10.359022	
38	9.60301	9.90201	9.64105	10.358942	
139	9.60330	9.96190	9.64140	10.358592	Part .
40	9.60359	9.96184	9.64174	10.35825 2	
41	9.60388	9.95179	9.04209	10.3579011	9
12	9.60416	9.96173	9.64243	10.357561	
1431	9 60445	9.95168	9.64277	10:357221	
44	9.60474	9.96162	9.64312	10.35687 10	- 4
-	9 60503	9.96156	9.64346	10,356531	-3
40	9.60531	9.96151	9.64380	10.356191	41
4/	9.60560	9.96145	9.64414	10:355501	- E
	9.60617	9.96134	9.64483		ī
	9.60646	9.96129	9.64517	10.35482 10	
	9.60675	9.96123	9.64551		9
	9.60703	9.96117	9.64585	10.35414	8
53	9.60732	9.96112	9.64619	10.35380	7
	9.607.60	9.96106	9.64654	2221	- 1
	9.60789	9.96101	9.64688		5
56	9.60817	9.90095	9.04722		4
57	9 60846	9.96089	9.64756		3
150	9.00874	9.96084	9.64790	77	
	9.60902	9.96073	9.64858		0
	Cosine.	Sine.	Gotang.	Tangent.	1
	LI3	, 01710,		66 Degrees.	

2	24 D g	rees.		155
177.	Sine.		Tangent.	Cotang.
C	9 60931	9.95073	9 64858	10.35141 60
1	9 00959	9.90007	9.04892	10.35107 59
2	3.60988	9.96061	9.64926	10.3507358
5		9.96056	9.64960	10.3503957
4	1.61044	9.96050	9.65028	19.3497155
6		9.96039	9.65061	10.3493854
	1'	9.96033	9.65095	10.34904.53
7	1.61157	9.96027	9.65129	10:3487052
1 9	9 61185	9.90022	9.651113	10.3483651
1	9.61213	9.96016	9.65197	10.34802,50
	1.01242	9.96010	9.65231	10.34768 49
	9.61270		9.65265	10.34734 47
11	19.61320	9.95993	9.65332	10.34667 46
	5).61354		9.65366	10.3463345
I	9.01382	9.95982	9.05400	10.34599 44
	, 9.61410	19.95976	9.65433	10.3456643
1	1/		9.65467	10.3453242
	9.61466 9.61494			10.34498 41
	19.61523	-		
	29.61550			10.34397 38
	3 9.61578			
2	49.61609	9.95936	9.65669	10 34330 36
2	5 9.61632	1		
	0 9.61661			
	79.61680		9.65769	10.3423033
	89.61717			10.34196,32
	c 9.6177			
	Coline.	Sine.	Gotang.	Tangent. Z
1	114			65 Digrees.

M	24 De	rees.		155	1
n.	Sine.	Cosine.	Tangent.	Cotang.	
30	9.61772	9.95902	9.65870	10.34129	30
31	9.61800	9.95895	9.65903	10.34095	29
32	9.61828	9.9;890	9.65937	21	28
33	9.61855	9.95885	9.65970	- 1	27
34	9.61883	9.95879	9.66004	222777	26
-	/	9.95873	9.66037		25
30	9 61938	9.95867	9.66104	337 /	24
38	9.61993	9.95856	9.66137		23
39	9.62021	9.95850	9.65171		21
40	9.62048	9.95844	9.66201		20
41	9.622;6	9.95838	9.65237		19
42	9.62103	9.95832	9.66270	10.33729	18
43	9 62131	9.95827	9.66304	10.33695	17
	9.62158	9.95821	9.66337	1	16
45	9 92186	9.95815	9.66370	10.33629	15
4t		9 95809	9.66403	10.33596	14
47	9.62240	9.95803	9.66437	10 33502	13
48	' /	9.9579	9.66470	10.33529	· 1
50		9.95785	9.65536	10.33493	10
51	9.02350	9.95780	9.66;69	10.33430	9
52	1	9.95774	9.65602	10.33367	9
53	9.6240+	9.95768	9.66635	10.33364	7
54		9.95762	9.66569	10.33330	6
55	9.62459	9.95756	9.66702	10.33297	5
156	9.02486	9.95751	9.66735	10.33264	4
	9.62513	19.95745	9.66768	10.33231	3
58	1 ,	9.95739	9.66801	10.33198	. 2
59	9.62567	9-95733	9.66834	10.33165	
-		9.95727		10.33132	7.
-	Cofine.	Sine.	* Cotung.	Tangent.	2
1 1	1 114 65 Degrees				

三	25 De	grees.		154	1		
177	Sine.	Cofine.	Tangent.	Cotang.	1		
0	9.02594	9.95727	9.66867	10.33132 60			
	9.62621	9.95721	9.66900	10.33099 59			
1 4	9 62648	9.95715	9.66933	10.33066 58			
	9.62676	9.95709	9.66966	10.33033 57			
	9.62730	9.95/03	9.67031	10.32968 5	- 1		
1 0-	9.62757	9.95692	9.67064	10.32935 54	3)		
7	9.62783	9.95685	9.67097	10.32902 5			
8	9.62810	9.95680	9.67130	10.32869 52	2		
	9.62837	9.95674	9.67163	10.32836 51			
No. Com	9.62864	9.95568	9.67196	10.32803 50	-]		
III	9.62891	9.95602	9.67229	10.32770 40			
	9.62945	9.95656	9.67294	10.32738 48	- 1		
14	9.62972	9.95644	9 67327	10.32672 46			
15	9 62598	9.95628	9.67360	10.32639	- 1		
16	9.63025	9 95632	9.67392	10.32607 4	- }		
17	9.63052	9.9562t	9.674.25	10 32574 4	31		
18	9.63079	9.95620	9.67458	10.32541 4	-1		
19	9.63105	9.9;51:	9.67523	10.32508 4	- 5		
-	9.03139	9.9;602	9.67556	10.32476	- }		
	9.63185	9.95596	9.67589	10.32410 3			
	9.63212	9.95590	9.67621	10.32378 3	- 1		
	9.63239	9.95584	9.67654	10.32345 3			
	9.63265	9.95578	9.67686	10.32313 3	5		
	9.63292	9.95572	9.67719	10.32280 3.			
	9.63318	9.95566	9.67752	10.32247 3	~ 1		
20	9.63345	9.95560	9.67784	10.32215 3			
30	3 63398	9.95548	9 67849	10.32150 3	-		
1-1	Coline.	Sine.	Cotang.	Tangent			
1	115 64 Degrees.						

25 Degrees. 154					
Sine.	Cofine.	Langent.	Cotang.	2 -	
30 9.63398	9.95548	9.0-849	10.32150	30	
31 9.63424	9.95542	9.67882	10.32117	29	
32 9.63451	9.95536	9.67914	10.32085	28	
33 9.63477	9.95530	9.67947	10.32052	27	
35 9.63530	9.95518	9.68011	10.32020	25	
130 9.63556	9.95512	9.68044	10.31955	24	
37 9.63583	9.95506	9.68076	10.31923	23	
38 9.63609	9.95500	9.68109	10.31890	22	
39 9 63636	9.95494	9.68141	10.31858	21	
-	9.95488	9.68173	10.31826	20	
41 9.03688	9.95482	9.68206	10.31793	19	
43 9.63741	9.95470	9.68270	10.31761	18	
44 9.6 3 7 6 7	9.95464	9.68303	10.31696	16	
45 9.63703	19.95457	9.68335	10.31664	15	
46 9.63819	9.95451	9.68367	10.31632	14	
47 9.63845	9.95445	9.68400	10.31599	13	
48 9.63871	9.95439	9.68432	10.31567	12	
49 9.63898	9.95433	9.68464	10.31535	II	
	9.95427	9.68496	10.21503	10	
51 9.03950	9.95421	9.68529	10.31470	9	
153 9.64002	9.95409	9.68593	10.31406	- 1	
54 9.64028	9.95402	9.68625	10.31374	7	
55 9.64054	9.95396	9.68657	10.31342	5	
56 9.04080	9.95390	9.68689	10.31310	4	
57 9.64106	9.95384	9.68721	10.31278	3	
58 9.64132	9.95378	9.68754	10.31245	2	
599.64158	9.95372	9.68786 9.68818	10.31213	C	
Gofine.	Sine.	Coline.		1	
	June.	Caspille.	64 Degrees	2	
1 115			of Digites	-	

Z' 26 Degrees. 153					
B Sine:	Lofine.	Langent.	Cotang.		
0,9.64184	9.95306	9.68818	10.31181 60		
19.64210	9.95359	9.68850	10.31149 59		
29.64235	9.95353	9.68882	10.31117 58		
3 9.64261	9.95347	9.68914	10.31085 57		
49.64287	9.95341	9.68946	10.31053 56		
5 9.64313	9.95335	-			
69.64339	9.95328	9.69010	10.30989 54		
7 9.64365	9.95322	9.69074	122		
89.64390	9.95316	9.69106	10.30925 52		
109.64442	9.95304	9.69138	10.30861 50		
11 9.64467	9.95297	9.69170	10.30830 49		
129.64493	9.95291	9.69201	10.30798 48		
13,9.64519	9.95285	9.69233	10.30766 47		
149.64544	9.95279	9.69265	10.30734 46		
15 9.64570	9 95273	9.69297	10.30702 45		
16 9.64596	9.95206	9.09329	10.30670 44		
17964621	9 95 260	9.69361	10.30638 43		
189.64647	9.95254	9.69392	10.30607 42		
20 9.64672	9.95248	9.69424	10.30575 41		
	-	9.69488			
21 9.64723	9.95235	9.69520	10.30511 39		
23 9.64774	9.95229	9.69551	10.30479 38		
24 .64800	9.95216	9.69583	10.30416 36		
25 9.64825	9.95210	9.65615	10 30384 35		
269.64851	9.95204	9.69046	10.30353 34		
27 9 64876	9.95197	9.69678	10 30321 33		
28 9.64902	9.95191	9 69710	10.30289 32		
299.64927	9.95185	9.69741	10.30258 31		
30 9.64952	9.95179	9.69773	10.30226 30		
Cosine.	Sine.	Cotang.	Tangent. \S		
116	116 63 Degrees.				

13 26 Dezi	e(\$.		- 11	ria.
Sine.		1 Tangent.	Cotang.	3.3
30 9.6 195.2	9.95179	19 09773	-	30
31'9.04978	9.95172		10.30194	20
32 9.65003	9.95166			28
339.65028	9.95160	9.69368		25
35 9.65079	19.95147	9.6991	10.30099	25
30,9.65104	9.95141	9.0993	10.30036	24
379.65129	9.95134	9.69974		23
38 9.65154	9.95128	9.70026	10.29973	22
39 9.65 180	9.95122	9.70057	10.29912	21
41 9.65230	9.95109	9.70120	10:29879	19
42,9.65255	9.95103	9.70152	10.29847	18
43 9.65280	9.95096	9.70183	10.29816	17
44'9.65305	9.95090	9.70215	10.29784	16
45 9.65 330	9 93084	9.70246	10.29753	15
46 9.65355	9.95071	9.70278	10.29721	14
48 9.65405	9.95055	9.70340	10.29659	12
49,9.65430	9.95058	9.70372	10.29627	1
50 9.65.155	9.95052	9.70403	10.29596	IO
51 9.65480	9.95045	9.70434.	10.29565	9
52 9.65505	9.95039	9.70466	10.29533	7
549.65555	9.95026	9.70528	10.29471	6
55 9.65580	9.95020	9.70560	10.29439	5
56 9.05605	9.95013	9.70591	10.29408	4
57 9.65630	9.95007	9.70622	10.29377	3
58 9.65655	9.95000	9.70685	10.29345	7
60 9.65704	9.04788	9.70716	10.29283	0
Cofine.	Sine.	Cotang.	Tangent.	7
116		-	63 Degrees.	-

1 50	10 11	1885.		15	1
in.	221.6.	Lujin .	Targini.	C.tang.	_
(9.6-110	9.94593	9. 2567	10.27.432	60
	9.57184	9.94586	9.72597	10.27402	59
	9.67208	9.94580	9.72628	10.27371	58
	9.67232	9.94573	9.72658	10.27341	57
	9.67279	9.94559	9.72719	10.27280	55
	9.67303	9.94553	9.72750	10.27249	54
7	9.67326	9.94546	9.72780	10.27219	53
	9.67350	9.94539	9.72810	10.27189	52
	9.67374	9.94532	9.72841	10.27158	5 I 50
	9.67421	9.94526	9.72901	10.27098	49
12	9.67444	9.94519	9.72931	10.27067	48
13	9.67468	9.94505	9.72962	10.27037	47
	9.67491	9.94498	9.72992	10.27007	46
	9.67515	9.9.4492	9.73023	10.26976	45
10	9.67538	9.94485	9.73053	10.26946	
18	9.07585	9.94478	9.73083	10.26916	43
19	9.67609	9.94465	9.73144	10.26855	41
20	9.67632	9.94458	9.73174	10.26825	40
21	9.47650	9.94451	9.73204	10.26795	39
22	9.6-6-9	9 94444	9.73235	10.26764	38
24	9.67703	9.94437	9.73265	10.26734	371
25	9.67749	9.94424	.9.73325	.10.26674	35
26	9.67773	9.94417	9.73355	10.26644	
12.7	9.67796	9.94410	9.73386	10.26613	33
23	9.67819	9.94403	9,73416	10.26583	32
30	9.67843	9.94396	9,73446	10.265 \$3	31
-	Copine.	Sine.	9,73476 Cotang.	Tangent.	M.10
1-	118	otne,	Gorang.	61 Degree.	
1 -			171	01 20 18166	- 1

N	28 D	Tiees.		151	-1
in.	Sine.	Coline.	Tangent.	Carano.	-
30	9.67866	9.94389	9.73475	-0.26523	30
31	9.67889	9.94382	9.73500	10.20493	29
32	9.67912	9.94376	9.73536	10.26463	28
33	9.67936	9.94369	9.73566	10.26433	27 26
35	9.67959	9.94362	9.73596	10.26373	25
30	-	9.94348	9.73650	10.20343	24
137	9.68028	9.94341	9.73687	10.26312	23
38	9.68051	9.94334	9.73717	10.26282	22
39	11	9.94327	9.73747	10.26252	21
40	9 68098	9.94321	9.73777	10.25222	20
41	9.68121	9.94314	9.73807	10.26102	19
12	9.68144	9.94307	9.73837	10.26162	18
44	9.68190	9.94293	9.73897	10.26102	16
	9.68213	9.94286	9.73.927	10.26072	15
-	9.68236	9.94279	9-73957	10.26042	14
47	9.68259	9.94272	9.73986	10.26013	13
	9.68282	9.94265	9.74016	10.25983	12
	9.68305	9.94258	9.74046	10.25953	II
	9.68328	9.94251	9.74076	10.25923	10
51	9.68351	9.94244	9.74106	10.25893	9
	9.68374	9.94237	9 74166	10.25833	7
	9.68420	9.91223	9.74196	10.25803	6
55		9.94216	9 74226	10.25773	5
156	9.68465	9.94209	9 74255	10.25744	4
57	9.68488	9.94202	9.74285	10.25714	31
58	7	9.94195	9.74315	10.25684	2
159	9.68534	9.94188	9.74345	10.25654	I
-	9.68557	Sine.	9.74375 Cotang.	Tangent.	=
-	Cofine.	oine.	- 3	61 Degrees.	4
_	118			or Degrees.	-

M	29 Deg	rees.		150	
n.	Sine.	1 Cofine.	Tangent.	Cotang.	
0	9.68:57	9.94181	9.74375	10.25624	60
I	9.68579	9.94174	9.74404	10.25595	59
2	9.68602	9.94167	9.74434	10.25565	58
3	9.68625	9.94160	9.74464	10.25535	57
4	9.68648	9.94153	9.74494	10.25505	56
5	9.68693		9.74524		55
7	9.68716	9.94139	9.74553	10.25446	54
8	9.68738	9.94125	9.74613	10.253.86	53
9	9.68761	9.94118	9.74642	10.25357	51
10	9.68784	9.94111	9.74672	10.25327	50
II	9 68806	9.94104	9.74702	10.25297	49
12	9.68829	9 94097	9.74731	10.25268	48
13	9.68852	9.94090	9.74761	10.26238	47
14	9.68874	9.94083	9.74791	10.25208	46
15	9.68897	9.94076	9.74820	10.25179	45
17	9.68919	9.94069	9.74850	10.25149	1-1
18	9.68942	9.94062	9.74880	10.25119	43
19	9.68987	9.94048	9.74939	10.25060	42 41
20	9.69009	9.94040	9.74968	10.25031	40
21	9.69032	9.94033	9.74998	10.25001	39
22	9.69054	9.94026	9.75028	10.24971	38
23	9.69077	9.94019	9.75057	10.24942	37
24	9.69099	9.94012	9.75087	10.24912	36
25	9.69122	9.94005	9.75116	10.24883	35
26	9.69144	9.93998	9.75146	10.24853	34
27	9.69166	9.93991	9.75175	10.24824	33
29	9.69189	9.93983	9.75205	10.24794	32 31
30	9.69233	9.93969	9.75264	10.24735	30
	Cofine.	Sine.	Cotang.	Tangent.	AL'S
1		E all agents or to the	8.	60 Degrees	
119 60 Degrees.					

N	20 Degr	ees.		150	*		
7	Sinc.	Cosine.	langent.	Cotang.	1		
30	9.69233	9:93959	9.75264	10.24735 30			
	9.69256	9.93,62	9.75293	10.24706 20	4		
	9.69278	9.93955	9.75323	10.24676 28			
	9.69300	9.93948	9.75352	10.24647 27			
	9.69345	9.93941	9.75382	10.24617 26			
	9.69367	9.93920	9.75440	10.24559 24			
	9.69389	9.93920	9.75470	10.2452923			
	9.69412	9.93912	9.75499	10.24500 22			
	9.69434	9.93905	9.75529	10.24470 21	ı		
	9.69456	9.93897	9.75558	10.24441 20	1		
	9.69478	9.93890	9.75587	10.24412 19	48		
42	9.69500	9 93883	9.75617	10.24382 18			
	9.69522	9.93876	9.75646	10.24353 17			
	9.69567	9.93869	9.75705	10.24324 16			
	9.69589	9.93854	9.75734	10.24265 14	- (
	9.69611	9.93847	9.75763	10.24236 13	-		
	9.69633	9.93840	9.75793	10.24206 12	1		
	9.69655	9.93833	9.75822	10.2417711	1		
50	9.69677	9.93825	9.75851	10.24148 10			
	9.69699	9.93818	9.25880	10.24119			
	9.69721	9.93811	9.45910		•		
	9 69743	9.93804	9.45939	10.24060	1		
55	9.69787	9.93789	9.75900	10.24002	•		
±6	9 69809	9.93782	9.76027	10.23972 4			
57	9.69831	9.93774	9.76056	10.23943			
58	9.69853	9.93767	9.76085	10.23914 2	2		
59	9.69875	9.93760	9.76114	10.23885	1		
6c		9.93753	9.76143	10.23856			
1:	Cosine.	Sine.	Cotan.	Tangent.			
I	119 60 Degrees.						

3	30 Digi	recs.		149	
\$77.	Sine.	Cofine.	Tangent,	Cor. ng	
0	9.69897	9.1.3 52	9.76143	10.23036	00
I	9.65918	9.93745	9.76173		59
2	9.69940	9.93738	9.76202		58
3	9 69962	9.93731	9.76231		57
4	9.69984	9.93723	9.76289	0,00	55
-6	9.70028	9.93709	9.76318		54
7	9.70049	9.93701	9.76347		53
8		9.93694	9.76377	10.23622	52
9	9.70093	9.93687	9.76400	0-1-	51
1 C	9.70115	9.93679	9.76435		50
11	9.70130	9.93672	9.76404		49
12	9.70158	9.93665	9.76,493	1	48 47
14	9.70180	9 93650	9.76551		46
IC	0.70222	9.93643	9.76580		45
11	9.70245	9.93635	9.76500	-	44
I.	9.70266	9.93628	9.76638	207	+3
18	17.1-0-0	9.93620	9.76667	222	42
119	1 , 2	9.93613	9.76696		41
20	11/232	9.93606	9.76725	-	40
21	9-70353	9.93598	9.76754	10.23245	38
2:	17.1.21.4	9.93591	9.76783		37
2	11137	9.93576	9.76841		36
2:	1	9.53569	9.76870	10.23129	35
26	9.70460	9.93561	9.76899	10.23100	34
27	9.70482	9.93554	9.76928	10.23071	33
28	12.4.2.2	9.93546	9.76957	10.23042	32
30	1 1 1 1	9.93539	9.76985	10.23014	31
13	-	9.93532	9.77014	10.22985	30
1-	Cofine.	Sine.	Cotang.	Tangent.	Z
-	120			59 Degrees.	

1	ISI 30 Degrees.					40
I	in.	Sine.	Coline.	Tangent.	Cotang.	49
	30	9.7054	9.93532	9.77014	10,2298;	120
	31	9 70508	9.93524	9.77043	-	30
		9.70589	9.93517	9.77072	10.22950	29
		9.70011	9.93509	9.77101	10.22898	27
	34	9.70632	7.93502	9.77130	10.2281.9	26
	35	9.70653	9.93494	9.77159	10.22840	25
	3:	9.70075	9.93487	9.7-188	10.22811	2.1
		9.70690	9.93479	9.77216	10.22783	23
		9.70718	9.93472	9.77245	10.22754	22
		9 70739	9.93464	9.77274	10.22725	21
		9.70760	9.93457	9.77303	10.22696	20
		9.70781	9.93449	9.77332	10.22667	19
		9.70824	9.93442	9.77360	10.22639	18
		9.70845	9.93427	9.77418	10.22510	17
		9.708	9.93419	9.77447	10.22552	15
	41		9.93412	9.77475	10.22524	-
		9.70909	9.93404	9.77504	10.22495	14
		9.70930	9.93397	9.77533	10.22466	12
	49	9.70951	9.93389	9.77562	10.22437	II
	50	9.70972	9.93382	9.77590	10.22409	10
i		9.70994	9.43574	9.77019	10.22380	0
i		9.71015	9.93367	9.77648	10.22351	9
ı		9.71036	9 93359	9.77676	10.22323	7
ı	-	9.71057	9.93352	1.77705	10.22294	6
	55	9.71078	9.933.14	9.77734	10 22265	5
		9.71099	9 93 53	9.77762	10.22237	4
	6	9.71120	9.93329	9.77791	10.22208	3
	-	9.71162	9.93314	9.77848	10.22179	2
		9.71183	9.933.4	9.77877	10.22122	
		Colline.		Cotang.	Tangent.	E
		120	-/	0	59 Degrees	
	_				3	- f

M	31 Deg	rees.		14	8 }
n.	Sine.	Cosine	Tangent.	Cotang.	
0	9.71183	9.93306	9.77877	10.22122	60
	9.71204	9:93298	9.77.905	10.22094	59
	9.71225	9.93291	9.77934	10.22065	58
	9.71246	9.93283	9.77963	10.22036	57
4		9.93276	9.77991	10.22008	50
5	-	9.93268	9.78020	10.21979	55
	9.71309	9.93250	9.78048	10.21951	54
7 8	9.71330	9.93253	9.78106	10.21922	53
	9-71372	9.93238	9.78134	10.21865	51
10		9.93230	9.78163	10.21836	50
11	9.71414	9.93222	9.78191	10.21808	49
1 2	9.71435	9.93215	9.78220	10.21779	48
13	39.71456		9.78248	10.21751	47
	9.71476	9.93199	9.78277	10.217.22	46
	9.71497	9.93192	9.78305	10.21694	45
	9.71518			10.21665	44
17		9.93176		10.21637	43
	99.71560		9.78391	10.21608	42
20		9.93153	9.78447	10.21552	40
21			9.78476		
2:	1 '	1110 -	9.78504	10.21523	39
2				10.21466	37
2.	11 1 1 2	12 / 0	9.78561	10.21438	36
2	9.71705	9.93115	9.78590	10.21409	35
2).71725			10.21381	34
2	9.71746			10.21353	33
28	13.1.1.1			10.21324	32
120	1 1 1 1			10.21.296	31
1,	7.71808	-		10.21268	30
-	10 hne	Sine.	· Cotang.	Tangent.	12
-	121	The Arthres becomes up	- Antonio de la constituira de	58 Degn	ees.

M	31 Deg	reis.		148	=1
11	Sine.	Cosine.	Tangent.	Cotang.	
30	9.71808	9 93076	9.78731	10.21268	30
31	1.71824	9.93068	9.77700	10.21239	29
	9.71849	9.93061	9.78788		28.
	9.71870	9.93053	9.78816		27
_	9.71890	9.93045	9.78845 9.78873	10.21154	25
35	9.71911	9.93037			24
	9.71931	9.93030	9.78901	10 21093	23
-/-	9.71952	9.93014	9.78958	10.21041	22
39	9.71993	9.93006	9.78986	10.21013	21
40	9.72013	9.92998	0.79015	10.20.984	20
41	9.72034	9.92991	9.79043	10.20956	19
42	9.72054	9.92983	9.79071	10.20928	18
43	9.72075	9.92975	9.79099	10.20900	17
44		9.92967	9.79128	10.20871	16
45	9.72116	9.92959	9.79156	10.20843	15
46	1.72136	9.92952	9 79184	10.20815	14
47		9.92944	9.79212	10.20758	12
	9.72177	9.92936	9.79269	10.20730	1.1
49	9.72197	9.92920	9.79297	10.20702	10
-		9.92912	9.79325	10:20674	9
51	9.72258	9.92905	9.79353	10.20646	8
	9.72279		9.79381	10.20618	7
	9.72299	. 9.92889	9.79410	10.20589	6
55	9.72319	9.92881	9.79438	10.20561	_5
56	9.72340	9.928.73	19.79400	10.20533	4
57	9.72360	9.92865	9.79494	10.20505	3
	9.72380		9.79522		2
	9.72400		9.79550	10.20421	0
00	9 72420	Sine.	Cota g.	? angent.	5
-	Cojine.) Other,	8.	58 Degrees	5.
-	IZI			-	

N	32 Deg	grees.		14	7
77	Sini.	Cofine	Tangent.	Cotang.	
0	9.72420	9.4,23.12	9.79578	10.20421	60
I	// 11	9.92834	9 79607	10.20392	59
	9.72461	9.92826	9.79635	10.20364	58
	7.72481	19.92818	9.79563	10.20336	57
	9.72501	9.92810	9.79719	10.20360	55
-	9.72542		9.79747	10.20252	54
	9.72562	9.92794	9.79747	10.20224	53
8	9.72582	9.92778	9.79803	10.20196	52
	7.72502	9 927-0	9.79831	10.20168	51
10	4.72622	9.927.12	99859	10.20140	50
11	1.72042	9.92754	9.79837	10.20112	49
1.2	1.72062	9.92746	9.79)15	10.20084	48
13	1.72682	9.92738	9-79943	10.20056	47
11	2.72702	9.92731	9.79971	10.20028	46
	7 7 3 7 2 2	9.92723	9.79999		45
).72742	9.92715	9.80027	10.19972	44
17	9.72782	9.92707	9.80055	10.19944	43
19	3.72822	9.92691	9.80111	10.19888	41
1 1	9.72822	9.92083	9.80139	10.19850	40
21	9.72 42	9.92675	9.80157	10.19832	39
22	9.72862	9.92667	9.80195	10.19804	38
2 3	9.72882	9.92659	9 87223	10.19776	37
	172902	9 926;1	9.80251	10.197.18	36
-	1.72922	0.02013	9.30279	10.19720	35
	1-2942	9.92635	9.80307	10.19092	34
2-	9.72962	0.92627	9.80335	10.19604	33
20	9.72931	9.92619	9.80362	10.19537	-32
30	9.73721	9.92010	9.80390	10.19539	31
×	Cofine.	Sine.	Cotang.	Tangent.	A Jos
	2.2	Oluc	Cottong.	57 Digie	
1	6+ H			3/ 10:8/6	34

M	32 Deg	grees.		147	- 1
n.	Sine	Coline,	Tangent.	Cotang.	
30	3.73021	9 921.02	0.80418	10.19;81	30
31).73041	9.92594	9.80446	10.19553	20
3-	7.73061	9.92586	9.80474	10.19525	28
33	9.73081	9.92578	9.80502	10.19497	27
34	9.73100	9.92570	9.80530	10.19469	26
35	3.73120				25
3	9.73140	9.92554	9.80585	10.19414	24
37 38	9.73160	9.92546	9.80641	10.19358	22
1	1	9.92530	9.80669	10.19330	21
40	9.73219	9.92522	9.8.69	10.19102	20
41	9.73239	9.92514	9.80724	10.19275	19
1.	9.73258	9.92505	9.80752	10.19247	18
43	9.73278	9.92497	9.80780	10.19219	17
	9.73298	9.92489	9.80808	10.19191	16
45	9.73317	9.92481	9.80836	10. 9163	15
4	9.73337	9.92473	9 00803	10.19136	14
47	111000	9.92465	9.80891	10.19108	13
	9.73376	9.92457	9.80919	10.19052	11
1	9.73415	9.92449	9.80974	10.19025	10
51	9.73435	9.94432	9.81002	10.18997	0
52		9.92424	9.81030	10.18969	9
-	9.73474	9.92416	9.81057	10.18942	7
54		9.92408	9.81085	17.18914	6
55	9.73513	9 92400	9.81113	10.18886	5
5	9.73532	9.92391	9.81141	10.18858	4
57	9.73552	9.92383	9.81168	10.18831	3
	9.73571	9.92375	9.81196	10.18775	2
	9.73591	9.92367	9.81251	10.18-18	0
-		9.92339 Sine.	Cotung	'I angent.	E
-	Cojine.	gine.	Jordang 1		-
1	122 57 Degrees.				

MI	33 De	grēes.		14	6 -
in.	Sine.	Cosine.	Tangent.	Cotang.	1
C	9.730 IC	9.92359	9.81251	10.18748	60
1		9.92350	9.81279	10.18720	59
2	9.73649	9.92342	9.81307	10.18692	58
3	9.73669	9.92334	9.81334	10.18665	57
	9.73688	9.92326	9.81362	10.18637	56
	9.73707	9.92318	9.81389	10.18610	55
1.6	9.73727	9.92309	9.81417	10.18582	54
7	9.73746	9.92301	9.81445	10.18554	53
0	9.73766	9.92293	9.81472	10.18527	52
IIC	9.73785	9.92285	9.81500	10.18472	51
	9.73804		-		
112	9.73824	9.92268	9.81555	10.18444	49 48
13	9.73862	9.92252	9.81610	10.18389	47
	9.73882	2.92243	9.81638	10.18361	46
	9.73901	9 92235	9.81665	10.18334	45
116		9.92227	9.81693	10.18306	44
17	9.73939	9.92218	9.81720	10.18279	43
18	9.73959	9.92210	9.81748	10.18251	42
119	9.73978	9.92202	9.81775	10.18224.	41
20	9.72997	9.92194	9.81803	10.18106	40
21	9.74016	9.92:85	9.81830	10.18169	39
22	9.74035	9.92177	9.81858	10.18141	38
23		9.92169	9.81885	10.18114	37
24	9.74074	9.92160	9.81913	10.18086	36
-	9.74093	9.92152	9.81940	10.18059	35
20).74112	9.92144	9 81968	10.18031	34
25	9.74131	9.92135	9.81995	10.18004	33
24).74150).74169	9.92127	9.82050	10.17976	31
30		9.92110	9.82078	10.17021	30
-	Coline.	Sine.	Gotang.	Tanger	Ni J
-	123		8.	56 Degrees	
_		-			- A

N	33 Degi	rees.		174	6	
in.	Sine.	Cosine.	Tangent.	Cotang.		
30	9.74188	9.92110	9.82078	10.17921	30	
-	9.74208	9.92102	9.82105	10.17894	29	
		9.92093	9.82133	10.17866	28	
3.3		.9.92085	9.82160	10.17839	27	
34		9.92077	9.82188	10.17811	25	
	9.74284	9.92068			-	
	9.74303	9.92060	9.82242	10.17757	24	
	9.74322	9.92043	9.82297	10.17702	22	
	99.74360	9.92035	9.82325	10.17674	21	
	9.74379	9.92026	9.82352	10.17647	20	
-	19.74398	9.92018	9.82379	10.17620	19	
	2 9.74417	9.92009	9.82407	10.17592	18	
4	3 9.74436	9.92001	9.82434.	10.17565	17	
4	19.74454	9.91993	9.82461	10.17538	16	
	5 9.74473	9.91984	9.82489	10.17510	15	
	6 9.74492	9.91976	9.82516	10.17483	14	
	7 9.74511	9.91967	9.82543	10.17456	13	
	8 9.74530	9.91959	9.82571	10.17401	II	
4	99.74549	9.91950	9.82625	10.17374	IO	
		-	9.82053	10.17346	9	
5	1 9.74587	9.91933	9.82680	10.17319	8	
2	3 9.74624	9.91916	9.82707	10.17292	7	
5	49.74643	9.91908	9.8:735	10.17264	7 6	
5	5 9.74662	9.91899	9.82762	10.17237	_5	
	6 9.74081	9.91891	9.82789	10.17210	4	
15	79.74699	9.91882	9.82816	10.17183	3	
	8 9.74718	9.91874	9.82844	10.17155	2	
	99.74737		9.82871	10.17128	I	
16	9.74756				1	
1	Cosine.	Sine.	Cotang.	I Tangent.	Z.	
1	1 123 56 Degrees.					

MI	El 34 Degrees. 145				
in.	Sine.	Cosine.	Tangent.	Cotang.	_
10	10.74756	9.91857	9 82898	10.17101	60
-	9.74774	9.91848	9.82925	10.17074	59
	9.74793	9.91840	9.82953	10.17046	53
and .	9.74812	9 91831	9.82980	10.17019	57
	9.74830	9.91823	9.83007	10.16992	5
-	9.74849	9.01814	9 83034	10.16965	55
	19.74808	9.91806	9.83 62	10.16937	54
7	9.74886	9.91797	9.83089	10.16910	53
		9.91789	9.83116	10.16883	52
	9.74924	9.91780	9.83143	10.16856	51
1	9.74942	9.91771	9.83170	10.16829	50
	9.74901	9.91763	9.8,198	10.10801	49
	9.74980	9.91754	9.83225	10.16774	48
	9.74998	9.91746	9.83252	10.16747	47
	9.75017	9.91737	9.83279	10.16693	45
	9.75035	9.91729	9.83306		
10	9.75054	9 91720	9.83333	10.1666	44
	9.75072	9.91711	9.83361	10.16611	43
	9.75091	9.91703	9.83388	10.16584	41
	9.75109	9.91604	9.83412	10.16557	40
P.		-	-		
	9. 5146	9.91677	9.83469	10.16530	39 38
	9.75165	9.91668	9.83496	10.16476	37
	7.75183	9.91651	9.83550	10.16449	36
	75202	0.91642	1.83578	10.164.21	35
21				10.16394	34
16	75239	9.91634	9.83605	10.16307	33
2		9.91625	9.83659	10.16340	32
16	91. 5391	9.91668	9.83 85	10.16313	31
	;312	9.91599	0.83-13	10.16286	3
S TOTAL	Ch.	Silla.	Cotang.	Tangent.	2
1		1 017.4.	Gorang.		,
1	124			55 Degrees	

-	D.			147 4
M.	34 De:		T	Catalan
-	Sine.	C tine.	Tongent.	Crang.
30	9. ,412	9.91:99	9 3-131	10 10286 36
31	9.75331	9.91590	9.83740	10.10259 29
32	9 753+9	9 91582	9.83767	10.16232 28
33	9.75367	9.91573	9.83794	10.16205 27
	9.75386	9.91564	9.83821	10.16178 26
35	9.75404	9.91555	9.83848	
136	9.75422	9.91547	9.83875	10.16124 24
	9.75'441	9.91538	9.83902	10.16097 23
	9.75459	9.91529	9.83929	10.15070 22
	9.75477	9.91521	9.83956	10.16016 20
	9.75496	9.91512	9.83983	
41	17 1 77 18	9.91503	9.24010	10.15962 18
	9.75532	9.91494	9.84037	10.1593517
	9.75550	9.91486	9.84064	10.1590816
	9.75569	9.91477	9.84118	10.1588115
	9 75587	9.91463	9.84145	10.1585414
	9.75605	9.91459	9.84172	10.15827 13
	9.75623	9.91450	9.84199	10.1580012
	9.75659	9.91442	9.84226	10.15773 11
	9.75678	9.91424	9.84253	10.15746 10
-	9.75696	9.91415	9.84280	
	9.75714	9.91415	9.84307	10.15719 9
	3,9.75732	9.91398		10.15605 7
54	9.75750	9.91389	9.84361	10.15638 6
5	9.75768	9.01380		10 15611 5
_	9.75786	9.91371	9.84415	10.15584 4
	79 75804	9.91362	9.84441	10.15558 3
58	3 9.75823	9.91354	9.84168	10.15531 2
59	9.75841	9.91345	9.84495	10.15504
60	9.75841	9.91336	9.84522	10.15477 0
	Cosine.	Sine.	Cotang.	Tangent. Z
1	124		the day they to	55 Degrees.
-	The Real Property lies			

131	35 De	grees.	-	14	4 1	
in.	Sine.	Cosine.	Tangent.	Cotang.		
C	9.75859	9.91336	9.84522	10.15477	60	
	9.75877	9.91327	9.84549	10.15450	59	
2	9.75895	9.91318	9.84576	10.15423	58	
	9.75913	9.91309	9.84603	10.15396	57	
	9.75931	9.91301	9.84630	- 20)	56	
	9.75949	9.91292	9.84683	10.15342	55	
7	9.75967	9.91283	9.84710	10.15316	54	
3 "	9.75903	9.91265	9.84737	10.15262	52	
	9.76021	9.91256	9.84764	10.15235	51	
10	9.76038	9.91247	9.84791	10.15208	50	
	9.76056	9.91238	9.84818	10.15181	49	
	9.76074	9.91229	9.84844	10.15155	48	
2	9.76092	9.91220	9.84871	10.15128	47	
	9.76110	9.91212	9.84898	10.15101	45	
Sales	9.76146	9.91194	9.84952	10.15047	44	
17	9.76140	9.91194	9.84932	10.15021	43	
18	9.76182	9.91176	9.85005	10.14994	42	
119	9.76199	9.91167	9.85032	10.14967	41	
-	9.76217	9.91158	9.85059	10.14940	40	
21		9.91149	9.85086	10.14913	39	
22	9.76253	9.91140	9 85112	10.14887	38	
	9.76271	9.91131	9.85139	10.14860	37 36	
	9.76:06	9.91113	9.85193	10.14806	35	
	9.70324	9.91104	9.85219	10.14780	34	
127	79.76342	9.91095	9.85246	10.14753	33	
25	9.76259	19.91086	9.85273	10.14726	32	
. 20	79.76377	9.91.077	9.85300			
130	6205	9.91068		10.146-73	30	
1	1 Cujine.	Sine.	Cotang.	Jung Citi	Z	
1	125 54 Degrees.					

M	35 Deg	rrees.		14	4	
in.	Sine.	Cosine.	Tangent.	Cotang.		
30	9.76395	9.91068	9.85326	10.14673	30	
	9.76413	9.91059	9.85353	10.14646	29	
	9.76430	9.91050	9.85380	10.14619	28	
	9.76448	9.91041	9.85406	10.14593	27	
	9.76466	9.91032	9.85433	10.14566	26	
	9.76501	9.91014	9.85487	10.14512	24	
27	9.76519	9.91005	9.85513	10.14486	23	
	9.76536	9.90996	9.85540	10.14459	22	
39	19.76554	9-90987	9.85567	10.14432	21	
	9.76571	9.90978	9.85593	10.14406	20	
41	9.76589	9.90969	9.85620	10.14379	19	
42	9.76607	9.90960	9.85647	10.14352	18	
43	9.76624	9.90950	9.85673	10.14326	17	
144	9.76659	9.90941	9.85700	10.14272	1.5	
	9.76677	9.90923	9.85753	10.14246	14	
	9.76694	9.90914	9.85786	10.14219	13	
	9.76712	9.90905	9.85806	10.14193	12	
	9.76729	9.90896	9.85833	10.14166	11	
	9.76747	9.90887	7 85860	10.14139	10	
51	9.76764	9.90878	9.85885	10.14113	98	
52	9.76782	9.90869	9.85913	10.14086		
53	9.76799	9.90859	9.85940	10.14033	7	
55	9.76834	9.90841	9.85993	10.14006	5	
	9.70852	9.90832	9.86019	10.13980	4	
157	9.76869	9.90823	9.85046	10.13953	3	
58	9.76887	9.90814	1.85072	10.13927	2	
159	9.76904	9.90804	7.85099	10:13900	E	
	9.76921	9.90795	9 85;26	10.13873	-	
-	Cosine.	Sine.	Jotang'.	Tungent.	\geq	
I	125 54 Degrees.					

17.	36 Deg	rees.	-	143
113	Jc 1	Cosine.	Tangent.	C'ong.
	0921	9.90795	9.85126	10.136;3 60
I	70339	9.90786	9 86152	10.13847 59
į.	7.76956	9.90777	9.86179	10.13820 58
3).76973	9.90768	9.85205	10.13794 57
4		9.90759	9.86232	10.13737 55
1-5	-	9.90749	9.86258	10.12741 55
6	17.11.	9.90740	9.86285	10.13638 53
1	9.77043	9.90731	9.86311	10.13068 53
6	9.77060	9.90722	9.86338 9.8636 5	10.13635 51
10		9.90712	9.86391	10.13608 50
11		9.90694	9.86418	10.13581 49
1	9.77129	9.90655	9.86444	10.13555 48
	9.77147	9.90675	9.85471	10.13528 47
	9.77164	9.90656	9.86497	10 13502 46
15	9.77181	9.90.57	9.86524	10.13475 45
	9.77198	9.90648	9.80550	10.13449 44
	9.77215	9.90638	9.86577	10.13422 43
	9.77233	9.90629	9.86603	10.13396 42
	9.77250	9.90620	9.86629	10.13370 41
		9.90601	9.86682	
2	1, 1, ,	9.90592	9.86709	10.13317 39
	39.77301	9.90583	9.86735	10.13264 37
	4,9.77336	9.90573	9.86762	10.13237 36
	5 9.77353	9.90564	9 86788	10.13211 35
-	6'9.77370	9.90555	9.80815	10.13184 34
	79.77387	9.90545	9.86841	10.13158 33
	8,9.77404	9.90536	9 86868	
	99.77421	9.90527		
3	09.77438	9.90517	1	10.13079 30
1	Cosine.	Sine.	Cotang.	Tangent. \S
1	126			53 Degrees.

1 5	35 D.s	rrripi.			
lin	Sine:		1.7	14	3
-	-	Cosine.	Tangens.	Cotang.	
130	9.77438	0.9051-	9.86920	10 1307.9	30
31	9.77455	9.90508	9.85947	10.13052	29
	9.77472	9.90499	9.86973	10.13026	28
133	9.77489	9.90489	9.87000	10,12999	27
	9.77506	9.90480	9.87026	10.12073	26
35	9.77523	9.90471	9.87052	10.12947	.2.5
136	9.77541	9.90401	9.87079	10.12920	24
37	9.77558	9.90452	9.87105	10.12894	23
	9.77575	9.90442	9.87132	10.12867	22
139	9.77591	9.90433	9.87158	10.12841	21
40	9.77608	9.90424	9.87184	10.12815	20
41		9.90414	9.87211	10.12788	10
	9.77642	9.90405	9.87237	10.12762	18
4-3	9.77659	9.90395	9.87253	10.12736	17
	9.77676	9.90386	9.87290	10.12709	16
45		9.90377	9.87316	10.12683	15
146	9.77710	9.90307	9 87343	10 12656	14
47	1	9.90358	9.8.7369	10.12530	13
	9.77744	9.93348	9.87395	10.12604	12
	9.77761	9.90339	9.87422	10.12577	11
5°	9.77778	9.90329	9.87448	10.12551	10
51	9.77795	9.90320	9.87474	10.12525	9
52		9.90310	9.87501	10.12498	8
53		9.90301	9.87527	10.12472	7 6
54	9.77845	9.90291	9.87553	10.12446	
55	9.77862	9.90282	9.87579	10.12420	_5
50	1	9.90272	9.87606	10.12393	4
57		9.90263	9.87632	10.12367	3
_	9.77912	9.90253	9.87658	10.12341	2
1 - /	9.77929	9.90244	9.87685	10.12314	I
00	9.77946	9.90234	9.87711	10.12288	0
1	Cofine.	Sine.	Cotung.	I angent.	2
I	26			53 Degre	es.

37 D	egrees.		14:	2 ,
Sine.	Cofine.	Tangent.	Cotang.	
09.77946	9.90234	9.87711	10.12288	60
1 9.77963	9.90225	9.87737	10.12262	59
29.77979	9.90215	9.87764	10.12236	58
39.77996	9.90206	9.87790	10.12209	57
49.78013	9.90196	9.87816	10.12183	56
5 9.78030	9.90187	9.87842	10.12157	55
6 9.78046	9.90177	9.87869	10.12130	54
79.78063	9.90168	9.87895	10-12164	53
89.78080	9.90158	9.87921	10.12078	52
99.78096	9.90148	9.87947	10.12052	51
100.78113	9.90139	9.87974	10.12025	50
11 9.78130	9.90129	9.88000	10.11999	49
12 9.78145	9.90120	9.88026	10.11973	48
139.78163	9.90110	9.88052	10.11947	47
149.78180	9.90101	9.88079	10.11921	46
15 9.78196	9.90091	9.88105	10.11894	45
169.78213	9.90081	9.88131	10.11868	44
179.78229	9.90072	9.88157	10.11842	43
189.78246	9.90062	9.88183	10.11816	42
19 9.78363	9 90052	9.88210	10.11789	41
20 9.78279	9.90043	9.88236	10.11763	40
219.78296	9.90033	9.88262	10.11737	39
229.78312	9.90024	9.88288	10.11711	38
239.78329	9.90014	9.88314	10.11685	37
24 7.78345	9.90004	9.88341	10.11658	36
25 9.78362	9.89995	9.88367	10.11632	35
26 9.78378	9.89985	9.88393	10.11606	34
27 9.78395	9.89975	9.88419	10.11580	33
28 9.78411	9.89966	9.88445	10.11554	32
29 9.78428	9.89956	9.88471	10.11528	31
30 9.78444	9.89946	9.88498	10.11501	30
Cosine.	Sine.	Cotang.	Tangent.	Z
127			52 Degree.	5.

37 Degre	ees.		14	2
Sine.	Cosine.	Tangent.	Cotang.	
30.9.78444	9.89946	9 88498	10.11501	30
31 9.78461	9.89936	9.88524	10.11475	29
32,9.78477	9.89927	9.88550	10.11449	28
33 9.78494	9.89917	9.88576	10.11423	27
34 9.78510	9.89907	9.88602	10.11397	26
35 9.78526	9.89898	9.88628	10.11371	25
36,9.78543	9.89888	9.88654	10.11345	24
37,9.78559	9.89878	9.88681	10.11318	23
38 9.78576	9.89868	9.88707	10.11266	22
39 9.78592 40 9.78608	9.89859	9.88759	10.11240	20
	-	9.88785	10.11214	10
41,9.78625	9.89839	9.88811	10.11188	18
43 9.78657	9.89820	9.88837	10.11162	17
44 9.78674	9.89810	9.88863	10 11136	16
45 9.78690	9.89800	9.88889	10.11110	15
46 9.78706	9.89790	9.88916	10.11083	14
47,9.78723	9.89781	9.88942	10,11057	13
48 9.78739	9.89771	9.88968	10.11031	12
49,9.78755	9.89761	9.88994	10.11005	11
50 9.78772	9.89751	9.89020	10.10979	10
51 9.78788	9.89741	19.89040	10.10953	9
529.78804	9.89731	9.89072	10.10927	8
53 9.78820	9.89722	9.89098		7 6
54 9.78837	9.89712			1 1
55 9.78853	9.89702		-	5
56 9.78869	9.89692	9.8917t	10.10797	4 3
57 9 78885	9.89682			2
58 9.78901	9.89672		1	I
609. 8934	19.89653			0
Cofine.	Sine.	Cotang.	Tangent.	M.
	1 vine.	Corang.		-
1 127			52 Digree	3.

38 De	grees.	******	Idi
Sine.	Cosine.	Tangert.	Cotting.
C9.750'4	9.80053	9.89280	10.10719 60
1,9.78950	9.89543	9.89307	10.10(92 59
29.78960	9.89533	9.89333	10.10606 58
39.78982	9.89323	9.89359	10.10640 57
49.78998	9.89613	9.89411	10.10588 55
6,9.79331	9.89593	0.89437	10.10502 54
7.9.79047	9.89583	9.89453	10.10536 53
89.79063	9.89574	9.89489	10.10510 52
99.79079	9.89564	9.89515	10.10484 51
10,9.79095	9.89554	9.89541	10.10458 50
11/9.79111	9.89544	9.89567	10.10432 49
12/9.79127	9.89534	9.89593	10.10466-48
149.79159	9.89514	9 89645	10.10354 46
1519.79175	9.89504	9.89671	10.10328 45
16,9.79191	9 89494	9.89697	10.10302 44
179.79207	9.89484	9.89723	10.10276 43
189.79223	9.89474	9.89749	10.10250 42
199.79239	9.89464	9.89775	10.10224 41
2019.70255	9.89454		10.10198 40
21 9.79271 22 9.79287	9.89444	9.89827	10.10173 39
239.79303	9.89424	9.89878	10.10121 37
249.79319	9.89414	9.89904	10.10095 36
25 9.79335	9.89404	9.89930	10.10069 35
26 9.79351	9.89394	9.89956	10.10043 34
27 9.79367	9.89384	9.89982	10.10017 33
28 9.79383	9.89374	9.90008	10.10991 32
30 9.79399	9.89364	9.90034	10.10965 31
Cofine.	Sine.	Cotang.	Tangent. Z
1 28	Othe.	Governg.	51 Degrees.
120			3. 2.8

17.	38 Deg	rees.		141	-	
	Sine.	Coline.	Tangent.	Cotang.	ı	
30	9.79414	9.89354	9.90060	10.09039 30	l	
31	9.79430	9.89344	9.90086	10.09913 29	l	
32	9.79446	9.89334	9.90112	10.09887 28	ı	
33	9.79462	9.89324	9.90138	10.09861 27	ı	
35	9.79478	9.89314	9.90164	10.09835 26	l	
30	9.79510	9.89294	9.90216	The Personal Control of the Pe	i	
37	9.79525	9.89294	9.90241	10.0978 224	I	
38	9.79541	9.89273	9.90267	10.09732 22	ì	
39	9.79557	9.89263	9.90293	10.0970621	-	
40	9.79573	9.89253	9.90319	10.09580 20	-	
4T	9.79589	9.89243	9.90345	10 09054 19	-	
42	9.79004	9.89233	9.90371	10.09628 18	ı	
	9.79620	9 3-1223	9.90397	10.09602 17	я.	
15	9.79536	9 89213	9.90423	10.0957616		
from		9.89203	9.90449	10.09550 15	н	
10	9.79507	9.89192	9.90474	10 09525 14	и.	
18	9.79099	9.89102	9.90526	10.0949913	н	
4	9.79715	9.89162	9.90552	10.09473112	u	
10		9.89152	9.90578	10 0)421 10	ŧ	
51	9.79746	9.89142	9.90004	10.09395	à	
52	9.79762	9.89131	9.90630	10.09369 8		
53	12.1 71 11	9.89121	9.90656	10.09343 7	-	
	9.79793	9.89111	9.90681	10.09318	ч	
55	17/7	7.89101	9.90707	10.09292	-	
155	17.17 - T	9.89091	9.90733	10.09266 4		
15	9.79840	9.39080	9.90759	10.09240	1	
350	9.79855	9.89070	9.90785	10.09214	1	
66		9 89050	19.90836	10.00163		
-	Cofine.	Sine.	Corang.	Tangent.		
organi	128		0	51 Degrees.	-	
128 51 Degrees.						

M	39 Deg	rees.		14	0		
in.	Sine.	Cofine.	Tangent.	Cotang.			
0	9.79887	9.89050	9 90836	10.09103	60		
	9.79902	9.89040	9.90262	10.09137	59		
	9.79918	9.89029	9.90888	10.09111	58		
1	9.79933	9.89019	9.90914	10.09085	57		
	9.79949	9.89009	9.90940	10.09059	5(
-	9.79965	9.88999	9.90966	10.09033	55		
	9.79980	9.88988	9.90991	10.09008	54		
7	9.79996	9.88978	9.91017	10.08982	53		
	9.80011	9.88968	9.91043	10.08930	52 51		
	9.80027	9.88957	9.91005	10.08904	50		
(I	9.80042		9.91120	10.08879	49		
	9.80073	9.88937	9.91126	10.08853	48		
	9.80089	9.88916	9.91172	10.08827	47		
	9.80104	9.88906	9.91198	10.08801	46		
S 1	1.80120	9.88896	9.91224	10.08775	45		
16	9.80135	9.88885	9.91249	10.08750	44		
	9.80151	9.88875	9.91275	10.08724	43		
	9.80166	9.88865	9.91301	10.08698	42		
19	9.80181	9.88854	9.91327	10.08672	41		
20	9.80197	9.88844	9.91352	10.08647	40		
21	9.80212	9.88834	9.91378	10.08021	35		
_	9.80228	9.88823	9.91404	10.08595	38		
	9.80243	9.88813	9.91430	10.08569	37		
	9.80258	9.88802	9.91455	10.08544	36		
-	9.80274	9.88792	9.91481	10.08518	35		
20	7.80289	9.88782	9.91507	10.08492	34		
20	9.80305	9.88771	9.91533	10.08466	33		
20	9.80320 9 80335	9.88761	19.91558	10.08441	32		
30	3.80351	9.88751	9.91584		3		
-	Coline.	Sine.	Cotang.	Tangent.	2-1		
-	-	J bine.	Juning.		12		
1_	129 50 Degrees.						

39 D. grees. 140					
in.	Sine.	Cofine.	Tangent 1	Cotang.	
30	9.80351	9.88740	9.91610	10.08389 30	
31	3.80366	9.88730	9.91636	10.08363 20	
32	/ /	9.88719	9.91661	10.08338 28	
	9.80396	9.88709	9.91687	10.08312 2-	
	9.80412	9.88698	9.91713	10.08286 26	
-	9.80427	9.88683	9.91739	10.08260 25	
	9.80442	9.88678	9.91764	10.08235 24	
37		9.88667	9.91790	10.08209 23	
38		9.88657	9.91816	10.08183 22	
39		9.88646	9.91841	10.08158 21	
40		9.88636	9.91867	10.08132 20	
41	9.80519	9.88625	9.91893	10.08105 19	
42		9.88615	9.91919	10.08080,18	
43	1 2 1 1 1	9.88604	9.91944	10.08055 17	
	9.80564	9.88594	9.91970	10.08029:16	
45	3.80579	-		10.08003 15	
46	0 7 7 7	9.58573	9.92021	10.07978,14	
47		9.88562	9.92047	10.07952 13	
	9.80625	9.88552	9.92073	10.07926 12	
149	9.80640	9.88541	9.92098	10.07901 11	
-	0	-			
51	9.80170	9.88520	9.92150	10.07849 8	
152	9.80686	9.88510	9.92176		
53	9.80701	9.88488	9.92227	10.07798 7	
55	9.80731	9.88478	9.92253	10.07746 5	
		9.88407			
	9.80746	9.88457	9.92278	1 1	
57	9.80776	9.88446	9.92330	10.07669 2	
	9.80791	9.88435	9.92355	10.07644 1	
	9.80800	9.88425	9.92381	10.07618	
-	Cofine.	Sine.	Cotung	Tangent, 2	
1	129			50 Degrees.	

1 50	40 Deg	rees.		139	1		
Tin.	Sine.	Cosine.	Tangent:		ı		
-0	9.80806	9.88425	9.92381	10.07618 60			
-	9.80821	9.88414	9.92407	10.07592 59			
2	9.80836	9.88404	9.92432	10.07567 58	- 6		
. 3	9.80851	9.88393	9.92458	10.07541 57			
4	9.80865	9.88382	9.92483	10.07490 55			
	9.80881	9.88372	9.92509	10.07464 54	н		
	9.80896	9.88361	9.92535	10.07439 53			
	9.80911	9.88340	9.92586	10.07431 52			
	9.80920	9.88329	9.92612	10.07387 51			
	9.80956	9.88319	9.92637	10.07362 50	1		
	9.80971	9.88308	9.92663	10.07336 49	ŒΕ		
	9.80986	9.88297	9.92689	10.07310 48	п		
	9.81001	9.88287	9.92714	10.07285 47			
	9.81016	9.88276	9.92,40	10.07234 45	1		
-	9.81031	9.88254	9.92791	10.07208 44			
	9.81046	9.88244	9.92817	10.07182 43			
	9.81076	9.88233	9.92842	10 07157 42	-1		
	9.81091	9.88222	9.92868	10.07131 41	-		
20	9.81106	9.88212	9.92893	100/100	-		
	9.81120	9.88201	9.92919	10.07080 39	ш		
	9.81135	9.88190	9.92945	10.07054 3			
	9.81150	9.88179	9.92970	10.07003 3			
	9.81165	9.88158	9.92990	10.06978 3	5		
-	9.81195	9.88147	9.93047	10.06952 3	-		
	9.81210	9.88136	9.93073	10.06926 3			
	9.81224	9.88126	9.93098	10.06901 3			
	9.81239	9.88115	9.93124	10.06875 3			
39	9.81254	9.88104	9.93149		1 1		
1	Cofine.	\ Sine.	1 Cotang.	Langent.	92.0		
1	130 49 Degrees.						

1	40 Deg	rees		139	-	
lin.	Sine.	Cofine.	Tangent.	Cotang.		
130	9 81254	9.88104	9.93149	10.06850	30	
	9.81269	9.88093	9.93175	10.06824	20	
32	9.81284	9.88082	9.93201	10.06798	28	
133	9.81298	9:88072	9.93226	10.06773	27	
	9.81313	9.88061	9.93252	10.06747	25	
-	981328	9.88050	9 93277		-	
	7.81343	9.88039	9.93303	10.06690	24	
137	9.81357	9 88028	9:93328	10.05645	22	
		9.88018	9.93354	10.06619	21	
	9.81387	9.88007	9.93380	10.06504	20	
-	1	and the same of th	-	10.00508	10	
	9.81416	9.87985	9.93451	10.05543	18	
	9 81431	9.87963	9 93482	10.06517	17	
	9.81460	9.87952	9.93507	10.06492	10	
	9.81475	9.87941	9 93533	10.06466	15	
	9.81489	9.87931	9.93558	10.06441	14	
	9.81504	9.87920	9.93584	10.06415	13	
	9.81519	9.87909	9.93609	10.06390	12	
4.0	9.81533	9.87898	9.93635	10.06364	1 1	
50	9.81548	9.87887	9 93661	10.05338	10	
51	9.81563	9.87876	9.93686	10.06313	9 8	
52	9.81577	9.87865	9.93712	10.06287		
	9.81592	9.87854		10.06262	7	
	19.81606	9.87843	9.93763	10.06236	5	
1	9.81621	9.87832	9.93788	10.06211		
	9.81636	9.87821	19.93814	10.06185	4	
	9.81650	9.87810	9.93839	10.06160	3	
	9 81665	9 87799	9.93805	10.06134	1	
	9 8 1 6 7 9	9.87788	9.93090	10.00109	C	
-		Sine.	Cotang.		13	
-	Cofine.	June.	Corang.	I Tungent.	=	
1 150 49 Degrees.						

M.n	41 Deg	rees.		13	8	
77.	Sine.	Coline.	Tangent.	Cotang.		
0	1.81591	9.87777	9.93916	10.06083	60	
1	9.81708	9.87767	9.93941	10.06058	59	
2	1 1 3	9.87756	9.93967	10.06032	58	
	9.81737	9.87745	9.93992	10.06007	57	
4	11 . 1 3	9.87734	9.94018	10.05981	56	
5		THE PERSON NAMED IN	9.94043		55	
	9.81781	9.87711	9.94069	10.05930	54	
7 8	7.81795	9.87689	9.94120	10.05879	53	
	9.81824	9.87578	9.94145	10.02854	51	
	2.81839	9.87567	9.94171	10.05828	50	
11	3.81853	9.87556	9.94.196	10.05803	49	
12		9.87645	9.94222	10.95777	48	
13	/	9.87634	9.94247	10.05752	47	
14	2/	9.87623	9.94273	10.05726	46	
-).81911	9.87612	9.94298	10.05701	45	
).81925	9.17601	9.94324	10.05675	44	
	9.81940	9.87590	9.94349	10.05650	43	
110	9.81968	9.87579	9.94400	10.05599	42	
20	9.81983	9.87557	9.94426	10.05573	40	
2 1	9.81997	9.87545	9.94451	10.05548	39	
22	9.82011	9.87534	9.94477	10.05522	38	
23	9.82026	9.87523	9.94502	10.05497	37	
	9.82040	9.87512	9.94528	10.05471	36	
-	9.82054	9.87501	9.94553	10.05446	35	
125	9.82069	9.87490	9.94579	10.05421	34	
27	9.82083	9.87479	9.94604	10.05395	33	
	9.82097	9.87467	9.94629	10.05370	32	
30	9.82126	9.87445	9.94055	10.05344	30	
-	Cosine.	Sine.	· Cotang.	Tangent	MIS	
131 48 Degree						

					1001
Mi	41 Deg				38
77.	Sine.	Cofine.	Tangent.	Cotang.	1-
3C	9.82126	9.87445	9.94680	10 05319	3C
31	9.82140	9.87434	9.94700	10.05293	29
132	9.82155	9.87423	9.94731	10.05268	28
133	9.82169	9.87412	9.94757	10.05242	
34	19.82183	9.87400	9.94782	10.05217	
13	9.82197	9.87389	9 94808	10.05191	25
130	5 9.82211	9.87378	9 94833	10.05160	
3	79.82226	9.87367	9.94858	10.05141	
	8 9.82240		9.94884	10.05115	2 1
3	9 9 82254	9.87344	9.94909	10.05090	
4	09.82268			10.05064	
	1 9.82283		9 949 00	10.05039	19
4	29.82297	9.87311	9.94986	10.0501	7
4	3 9.82311	19.87299		10.04988	
	19.82325			10.0496	
4	5 9.82330		9.95062		
	16 9.8235		9.95087	10.0491	2 14
4	17 9.8236	8 9.87254	9.95113	10.0488	5 13
1	18 9.8238	2 9.8724	3 9.95138	10.0486	
4	49 9.8239	6 9.8723	2 9.95164	10.0481	
	50 9.8241				
	51 9.8242				
	52 9.8243			10.0475	
- 1	53 9.8245	2 9.8718		1	
1	54 9.8246	6 9.8717			
	55 9.8248			-	
	50 9.8249				32 3
	57 9.8250	08 9.8714			07. 2
	58 9.825		9.9539 8 9.9541		81 1
	59 9.825				
	60 9.825		_		
	Cosine	Sine.	Cotang	48 Digi	
	131			40 118	

974	42 Deg	71.668.		143	1		
1 112	J. 726.	Conne.	Tangent.	Co'ang.			
(9.82551	9.87107	9 95443	10.04556	60		
1	9.82505	9 87095	9.954.9	10.04530	59		
	9.82579	9.87084	9.95494		58		
	9.82593	9.87073	9.95519		57		
4	9.82607	9.87051	9.95545	- 1	56		
-6	-	9.87636	9.95570	-			
1	9.82649	9.87027	9.95595		54		
1 2	9.82663	9.87016	9.95646	,	52		
C		9.87004	9.95672		51		
10	9 82690	9.85993	9.95697		50		
1:	9.82704	9.86981	9.95723		49		
	7.82718	9 86970	9.95748		48		
	9.82732	9.86958	9.95773		+7		
	9.82746	9.86947	9.95799		46		
1	-	9.80924		Comments of the last of the la	45		
	9.82774	9.86912	9.95850		44		
	9.82802	9.86901	9.95900		42		
	9.82816	9.86890	9.95926		41		
20	9.82830	9.85878	9.95951	10.04048	40		
21	9.82843	9.86867	9.95976	10.04023	39		
	9.82857	9.86855	9.95002		38		
	9.82871	9.86843	9.96027		37		
	9 82885	9.86820	9.96053	1	36		
-	-	Street Constitution of the last	-		35		
	9.82913	9.86869	9.90103	0 1	34		
	9.82940	9.86,86	9.96154		32		
	9.82954	9.86774	9.95179	1 , , ,	31		
	0.820(-8	9 86763	9.06205		30		
1	(10/:1.8.	Sine.	Citung.	Tangest.	2		
T	132. 47 Digrecs.						

31 9	Sine .82958	9.86763	Tangent.	Cotang.	- 1
31 9		0.86=621			1 1
	0 - 0 -	9.00/03	9.96205	10.03794	30
32 0	.82982	98751	9.96230	10.03769	29
	.82995	9.86739	9.96255	10.03744	28
	.83009	9.86728	9.96281	10.03718	27
3419	.83023	9 85716	9.96306	10.03693	26
	.83037	9 86705			25
30 9	.83050	9.80.693	9.96357	10.03642	24
3719	.83064	9.86681	9.95408	10.03591	23
300	.83092	9.86658	9.96433	10.03566	21
100	.83105	9.86646	9.96458	10.03541	20
	.83119	9.86635	9.96484	10.03515	19
	.83133	9.85623	9.96509	10.03490	18
	83140	9.86612	9.96534	10.03465	17
	.83160	9 85600	9.96560	10.03439	16
45:9	.83174	9.86588	9 96585	10.03414	15
45:9	83187	9.80577	9.96610	10.03389	14
47,9	0.83201	9.85565	9.96636	10.03363	I 3
18,9	9.83215	9.86553	9.96661	10.03338	12
	9.83228	9.86530	9.96686	10.03313	11
	0.83242			10.03262	
51 19	9.83256	9.86518	9.95737	10.03237	9,62
	9.83283	9.85495	9.95788	10.03211	
	9.83295	9.86483	9.95813	10.03186	6
5510	2.83310	9.86471	9.96838	-10.03161	5
Street Co.	0.83324	9.86459	9.96864	10.03135	4
	9.83337	9.85448	9.96889	10.03110	
58	9.83351	9.85436	9.96914	10.03085	
	9.83364		9.96940	10.03059	
	9.83378	-	9.96965	10.03034	
1 1	Cofine.	Sine.	Cotang.	1 Tangent.	

121 44 De	grees.		13	5								
Sine.	Copine.	Tangent.	Cotung.									
0 9.84177	9.85693	9.98483	10.01516	60								
19.84190	9.85681	9.98509	10.01491	59								
2 9.84203	9.85669	9.98534	10.01465	58.								
39.84216	9.85656	9.98559	10.01440	57								
49.84229	9.85644	9.98584	10.01415	56								
5 9.84212	9.85632	9.98610	10.01389	55								
09.84255	9.85020	9.98635	10.01364	54								
79.84268	9.85607	9.98660	10.01339	53								
99.84294	9.85583	9.98711	10.01288	52 51								
109.84307	9.85571	9.98736	10.01263	50								
11 9.84320	9.85558	9.98761	10.01238	49								
129.84333	,9.8554t	9.98787	10.01212	48								
113 9.84346	9.85534	9.98812	10.01187	47								
149.84359	9.85521	9.98837	10.01162	46								
15 9.84372	9.85509	9.98862	10.01137	45								
16 9.84385	9.85497	9 98888	10.01111	44								
179.84398	9.85484	9.98913	10.01086	43								
199.84424	9.85472	9.98963	10.01026	42								
2019.81437	9.85447	9.98989	10.01010	41								
21 9.84450	9 85435	9.99014	10.00985	-								
22 9.84463	9.85423	9.99039	10.00060	39								
23 3.84476	9.85410	9.99065	10.00034	37								
24 9.84488	9.85398	9.99090	10.00909	36								
25 3.84501	9.85386	9 99115	10.00884	35								
20).84514	9.85373	9.99140	10.00859	3+1								
27 9.84527	9.85361	9.99166	10.00833	33								
28 9.84540	9.85349	9.99191	10.00808	32								
25, 9.84553 30, 9.84566	9.85336	9.99216	10.00783	3 1								
Cofine.	Sine.	9.99241	10.00758	30								
2	ome.	Cotang.	Tangent.	2								
1 134			45 Degrees	134 45 Degrees.								

M	44 Degr			13	5
72.	Sine.	Cofine.	Tangent.	Cotang.	f
30	9.84566	19.85324	9.99241	10.00758	30
31	9.84579		9.99267	10.00732	29
32	9.84591	9.85.299	9.99292	10.00707	28
33	9.84604	9.85286	9.99317	10,00682	27
34	9.84017	9.85274	9-99343	10.00656	26
35	-	9.85262	9,99368	The second second	25
:36	9.84643	9.85249	9.99393	10,00000	24
37	9.84655	9.85237	9.99418	10.00581	23
38	9.84668	9.85224	9.99444	10.00530	22
39	9.84694	9.85212	9.99469	10.00505	20
1	9.84707	9.85187	-	10,00480	19
41	9.84719	9.85174	9.99519	10.00454	18
43	9.84732	9.85162	9 99545	10.00429	17
44	9.84745	9.85149	9.99595	10 00404	16
145	9.84758	9.85137	9.99621	10.00379	15
46	9.84770	9.85124	9.99646	10.00353	14
47	9 84783	9.85112	9.99671	10.00328	13
48	9.847.96	9.85099	9 99696	10:00303	12
49	9.84809	9.85087	9.99722	10.00277	1 1
50	9.84821	9 85074.	9-99747	10.00252	IC
51	9.84834	9.85061	9.99772	10.00227	9
5:2	9.84847	9.85049	9.99797	10.00202	. 8
	9.84859	9.85036	9.99823	10.00176	7 6
154	9.84872	9.85024	9.99848	10.00151	
55	9.84885	9.85011	9.99873	District Control of the last o	_5
56	9.84897	9.84998	9.99898	10.00101	4
57	9 84910	9.84986	9.99924	10.00050	3
	9.84923	9.84973	9.99949	10.00025	1
159	9.84948	9.84948	9.99974	10,00000	0
	Cofine.	Sine.	Cotang.	Tangent.	N.
1	134			45 Degree	

TABLE

OFTHE

LOGARITHMS

O F

NUMBERS from 1 to 2000.

To find the Logarithm of a given Number, and the contrary.

RULE

Find the Number in the Column Num. and against it is its Logarithm, in the Column Logar. I ikewise, if the Log. be given, seek the nearest in the Table, and against it is the correspondent Number.

Thus, the Log. of 45 is 1.65321; and the Log. of 1857 is 3.26881.

And, if the Log. be 2.92648, the nearest Log in the Table is 2.92634, whose Number is 844.

Num	Logarith,		Num	Logariti	1	Num	Logarith
I	0.00000		34	1.53147		67	1.82607
2	0.30103		35	1.54400	-	68	1.83250
3	0.47712		36	1.55630		69	1.83884
4	0.60201		37	1.56820		70	1.84509
5	0.6980~		38	1.579-8		71	1.85125
6	0.77815		39	1.59106		72	1.85733
7	0.84509		40	1.60206		73	1.86332
8	0.90309		41	1.61278		74	1.86923
9	0.95424		42	1.62324		75	1.87506
10	0000001		43	1.6334		76	1.88081
II	1.04139		44	1.04345	1	77	1.88049
12	1.07918	1	45	1.65321		78	1.89209
13	1.11394		46	1.66275		79	1.89752
14	1.14612		47	1.67209		80	1.90309
15	1.1-609		48	1.68124		81	1.90848
10	1.20412		49	1.09019		82	1.91381
17	1.23044		50	1.69897		83	1.91907
18	1.25527		51	1.70757		84	1.92427
19	1.27875		52	1.71600		85	1.929+1
20	1.30103		53	1.72427		86	1.93449
21	1.32221		54	1.73239		87	1.93951
22	1.34242		55	1.74036		88	1.94448
23	1.36172	ı	56	1.74818		89	1.94939
24	1.38021		57	1.75587		90	1.95424
25	1-39794		58		1	91	1.95904
26	1.41497		59	1.77085		92	1.95378
27 28	1.43136		61	1.77815		93	1.96848
29	1.44715	I	62	1.78532		94	1.97312
30	1.40239		63	1.79239		95 96	1.97772
			-		-		
3.1	1.49136		64	1.80618		97	1.98677
32	1.50515		661	1.81291		98	1.99122
33	1.51851	1		1.82607	-	99	2. 0000
34	33.4/	-	/-	1.0200/1		.100	2. 0000)

	I	00			-	0	-	
1	Num	Logarith		Nun	Logarith		Num	Logarith
	101	2.00+32		134	2.12710		167	2.22271
1	102	2.00860	1	135	2.13033		168	2.22530
1	103	2.01283	П	136	2.13353		169	2.22788
1	104	2.01703		137	2.13672		170	2.23044
1	105	2.02118		128	2.13987	П	171	2.23299
	10:	2.02530		139	2 14301		172	2.23552
1	107	2.02938		140	2.14612		173	2.23804
	108	2.03342		141	2.14921		174	2.24054
1	109	2.03742		142	2.15228		175	2.24303
1	110	2.24139		143	2.15533		176	2.24551
1	111	2.04532		144	2.15836		177	2.24797
1	112	2.04921		145	2.16136		178	2.25042
1	113	2.05307		146	2.16435		179	2.25285
1	114	2.05690		147	2.16731		180	2.25527
-1	115	2.06069		148	2.17026		181	2.25767
ı	116	2.00445		149	2.17318		182	2.2000-
-	117	2.06818		150	2.17609		183	2.26245
-	118	2.07188		151	2.17897		184	2.26481
1	119	2.07554		152	2.18184		185	2.26717
	120	2.07918		153	2.18469	1	186	2.26951
-	121	2.08278		154	2.18752	1	187	2.2718+
- Andrew	122	2.0863=		155	2.19033	-	188.	2 27.1.15
	123	2.08990		156	2.19312		189	2 2-646
1	124	2.09342	ı	157	2.19589	,	190	2.27875
Ì.	125	2 09691		158	2.19865	1	101	2.28:03
	126	2.10037		150	2 20139		192	12 28330
1	127	2.10300		160	2.20412	4	193	2 28 5 5 5
1	128	2.10721		161	2 20682		194	2.28-80
-	129	2.11058		162	2 209;1		195	2.29003
-	130	2.11391		163	2.21218		190	2.202.25
1	131	2.11727		104	2 21484		197	2.29.146
-	132	2.12057		164	2.2174		198	2.20(66)
1	133	2.12385		166	2.22010		199	2 29885
1	134	2.12710	1	167	2.22271		200	2.30103
								The same of the sa

200						
Num Lo	garith	Num	Logarith	1	Num	Logarith
201 2.	30319	234	2.36921		267	2.42051
	30535	235	2.37106		258	2 42813
203 2.	30749	236	2.37291		269	2.42975
204 2.	30953	237	2.37474	ш	270	
205 2.	31175	238	2.37657		271	2.43296
206 2.	31386	239	2.37839		272	2.43456
207-2.		240	2.38021		273	2.43616
208 2.		241	2.38201		274	2.43775
209 2.		242	2.38381		275	2.43933
210 2.		243	2.38560		276	2.44090
211 2,	32428	244	2.38738		277	2.44247
212 2.		245	2.38916		278	2 44404
213 2.		246	2.30093		279	2.44560
2142.	33041	247	2.39269		280	2.44715
215 2.	33243	248	2.39145		281	2.44870
216 2.	33445	249	2.39019		282	2.45024
217 2.	33645	250	2.39794		283	2.45178
218 2.	33845	251	2.39967		284	2.45.331
219 2.		252	2.40140		285	2.45484
220 2.	34242	253	2.40312		286	2.45636
221 2.	34439	254	2.40483		287	2.45788
222 2.	34635	255	2.40654		288	2.45939
223 2.	34830	256	2.40824		289	2.46089
224 2.	35024	257	2.40993		290	2.46239
225 2.	35218	258	2.41161		291	2.46389
226 2.	35410	259	2.41329		292	2.46538
227 2.	35602	260	2.41497		293	2.46686
228 2.		261	2.41664		294	2.46834
229 2.	35983	262	2.41830		295	2 46982
230 2.		263	2.41995		296	2.47129
231 2.	36351	264			297	2.47275
232 2.	365481	265			298	2.47421
233 2.		266			299	2.47567
1 234 2.	36921	1 267	12.42651	[300	2.47712

5 3	00		-	-		
Num	Logarith	Nun.	Logarith		Num!	Log with
301	2.4785t	334	2.52374	1		2.56:66
302	2.480CC	335	2.52504	1		2.56584
303	2.48144	336	2.52633			2.56702
304	2.48287	337	2.52762		- 1	2.56820
305	2.48426	338	2.52891		371	2.56937
306	2.48572	339	2.53019		372	2.57054
307	2.48713	340	2.53147		373	2.57170
308	2.48855	341	2.53275		374	2.57287
309	2.48995	342	2.53402		375	2.57403
310	2.4913	3+3	2.52529		376	2.5-518
311	2.49276	344	2.53655		377	2.57634
312	2.49415	345	2 53781		378	2.57749
313	2.49554	346	2.53907		379	2.57863
314	2.49692	3.7	2.54032		380	2.57978
315	2. 9831	3 18	2.54157		381	2.58092
316	2.49968	3+9	2.54282		382	2.58206
317	2.50105	350	2.54406		383	2.58319
318	2.50242	351	2.54530		384	2.58433
319	2.50379	352	2.54654		385	2.58546
320	2.50515	353	2.54777		386	2.58658
321	2.50650	354			387	2.58771
322	2.50785	355			388	2.58883
323	2.50920	356	2.55145		389	
324	2.51054	357			390	
325	-	-			391	2.50217
326		359	2.55500	3	392	
327		360 361			393	1 2 ,
	2 2 1		2.55750		394	1 222.
329	1	36:			395	
	1		-	MEDIO	-	-
331		30.			397	2.59879
33:					398	
33:			7 2.5646		399	
-		1 30	, 2:1040	-1	400	2,00200

Service Control	.00	_					
Num	Logarith	1	Num	Logarith.	1	Num	Logarit'
401	2.60314		434	2.63748		467	2.66931
402	2.60422		435	2.63848	3	468	2.67024
403	2.60530		436	2.63948		469	2.67117
404	2.60638		437	2.61048		470	2.67209
405	2.60745	В	438	2.64147		471	2.67302
406	2.60852	Ç-	439	2.64246		472	2.57394
497	2.60959		440	2.64345		473	2.67485
408	2.61056		441	2.64443		474	2.67577
409	2.61172		442	2.64542		475	2.67669
410	2.61278		443	2.64640		475	2.67760
411	2.61384		444	2.64738		477	2.67851
412	2.61489		445	2.64836		478	2.67942
413	2.61595		446	2.64933		479	2.68033
	2.61700	1	447	2.65030		480	2.68124
-	2.61804		448	2.65127		481	2.68214
	2.61909		449	2.65224		482	2.68304
417	2.62013	-1	450	2.65321		483	2.68394
418	2.62117		451	2.65417		484	2.68484
419	2.62221	-	452	2.65513		485	2.68574
-	2.62324	-1	453	2.65609		486	2.68663
	2.62428		454	2.65705		487	2.68752
	2.62531		455	2.65801		488	2.68841
	2.62634		456	2.65896		489	2.68930
424	2.62736	-	457	2.65991 2.65086		490	2.69019
			458			-	2.69108
	2.62940		459	2.65181	1		2.69196
	2.63042		460	2.66275		493	2.69284
428 2	2.63144	1	461	2.66370			2.69372
429 2	2.63245		462	2.66464	-	495	2.69460
					-		
	.63447	1	464	2.06651			2.0963
	2.63548		465	2.66745			2.69722
	2.63648	1	466	2.66838			2.6981c
434 2	2.63748		4071	2.00931	1	5001	2.090971

Num Logarith Num Logarith 501 2.69983 534 2.72754 567 2.75358 502 2.70070 535 2.72835 568 2.75434 503 2.70156 535 2.72916 569 2.75511 504 2.70243 537 2.72997 570 2.75587 505 2.70415 539 2.73078 571 2.75663 507 2.70500 546 2.73236 573 2.75815 507 2.70586 541 2.73316 574 2.75891 509 2.70671 542 2.73319 575 2.75966 509 2.70671 542 2.73319 572 2.75815 509 2.70671 542 2.73399 575 2.75966 511 2.76842 544 2.73559 577 2.76117 512 2.76842 544 2.73579 578 2.76192 514 2.712
502 2.70070 535 2.72835 568 2.75434 503 2.70156 535 2.72916 569 2.75511 504 2.70243 537 2.72997 570 2.75587 505 2.70415 536 2.73158 572 2.75739 507 2.70500 546 2.73396 573 2.75815 508 2.70586 541 2.73316 574 2.75891 509 2.70671 542 2.73396 575 2.75966 510 2.70-671 542 2.73396 575 2.75966 511 2.76842 544 2.73556 577 2.76042 512 2.76842 545 2.73536 577 2.76192 513 2.71611 546 2.73586 580 2.76342 514 2.71696 547 2.73886 581 2.76417 516 2.71204 549 2.73957 582 2.76492
503 2.70156 536 2.72916 569 2.75511 504 2.70243 537 2.72997 570 2.75587 505 2.70415 530 2.73158 572 2.75663 507 2.70500 546 2.73236 573 2.75815 508 2.70586 541 2.73316 574 2.75891 509 2.76671 542 2.73390 575 2.75966 511 2.76842 544 2.73550 577 2.76042 512 2.76842 544 2.73550 578 2.76192 513 2.71611 546 2.73716 579 2.76267 513 2.71611 546 2.73718 580 2.76342 514 2.7186 542 2.73878 581 2.76417 516 2.71204 549 2.73957 582 2.76492 517 2.71349 550 2.74036 583 2.7664 <
504 2.70243 557 2.72997 570 2.75587 505 2.70329 538 2.73078 571 2.75663 506 2.70415 530 2.75158 572 2.75739 507 2.70500 540 2.73237 573 2.75815 508 2.70586 541 2.73319 574 2.75891 509 2.70671 542 2.73390 575 2.75966 511 2.70842 544 2.73539 578 2.76042 512 2.70842 544 2.73539 578 2.76192 512 2.70842 544 2.73539 578 2.76192 513 2.71011 546 2.73710 579 2.76267 513 2.71186 542 2.73878 580 2.76342 516 2.71204 549 2.73957 582 2.70492 518 2.71432 551 2.74115 584 2.7664
505 2.70329 538 2.73078 571 2.75663 506 2.70415 539 2.73188 572 2.75739 507 2.70500 540 2.73231 573 2.75815 508 2.70586 541 2.73319 574 2.75891 509 2.70671 542 2.73399 575 2.75966 510 2.70-6-
505 2.70429 538 2.73072 571 2.75663 506 2.70415 530 2.75158 572 2.75739 507 2.70500 540 2.73234 573 2.75815 508 2.70586 541 2.73319 574 2.75891 509 2.70671 542 2.73390 575 2.75966 510 2.70000 542 2.73400 576 2.76042 511 2.70842 544 2.73554 577 2.76042 512 2.1092 545 2.73510 579 2.76267 513 2.71011 556 2.73710 579 2.76267 514 2.71094 556 2.73710 579 2.76267 516 2.71204 549 2.73857 580 2.76342 517 2.71349 550 2.74036 583 2.76566 518 2.71432 551 2.74115 584 2.76641 519 2.71516 552 2.74193 585 2.76715 520 2.71683 554 2.74350 587 2.76863 521 2.71683 554 2.74350 587 2.76863 587 2.76863 587 2.76863
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510 2.76-2-7 542 2.73.2-0 576 2.76042 511 2.76842 344 2.73539 577 2.76117 512 2.76927 545 2.73539 578 2.76192 513 2.71011 546 2.73710 579 2.76267 514 2.71294 547 2.738-10 580 2.76342 516 2.71294 549 2.73957 582 2.76417 517 2.71349 550 2.74036 583 2.76566 518 2.71432 551 2.74115 584 2.76641 519 2.71516 552 2.74193 585 2.76789 520 2.71683 554 2.74350 587 2.76863
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523 2.71850 556 2.74507 589 2.77011
524 2.71933 557 2.74585 590 2.77085
525 2.72015 5:8 2.74663 591 2.77158
526 2.72068 559 2.74741 592 2.77232
527 2.72181 560 2.74818 593 2.77305
528 2.72263 561 2.74896 594 2.77378
529 2.72345 562 2-74973 595 2.77451
530 2 72427 563 2.75050 596 2.7752
531 2.72500 564 2.75127 597 2.77597
532 2.72591 565 2.75202 598 7.7676
533 2.72672 566 2.75281 599 2.77-4:
534 2.72754 567 2.75358 600 2.7781:

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-	Vum	Logarith		Num	Logariti.	Num	Logariths
ľ	100	2.77887		034	2.80208	667	2.82412
ı	602	2.77959		635	2.80277	668	2.82177
ľ	603	2.78031		630	.2.80345	669	2.82542
I	604	2.78103		637	2.80413	670	2.82607
ı	605.	2.78175		638	2.80482	671	2.82672
I	606	2.78247		639	2.80550	672	2.82736
ľ	607	2.78318		640	2.80018	673	2.82801
ı	608	2.78390		641	2.80685	674	2.82865
ı	609	2.78461		942	2.80753	675	2.82930
į	610	2.78532		643	2.80821	676	2.82994
١	611	2.78004		644	2.80888	677	2.83058
ı	612	2.78675		645	2.80955	678	2.83122
ı	613	2.78746		64t	2.81023	679	2.83180
1	614	2.78816		647	2.81090	680	2.83250
ı	615	2.78887		648	2.81157	681	2.83314
-	616	2.78958		649	2.81224	682	2.83378
I	617	2.79028		650	2.81291	683	2.83442
ĺ	618	2.79098		651	2.81358	684	2.83505
1	619	2 79169	П	652	2.81424	685	2.83569
1	620	2.79239		653	2.81491		2.83632
I	521	2.79309		054	2.81557	687	2.83095
į	622	2 79379		655	2.81624	683	2.83758
I	623	2.79448		650	2.81690	689	2.83821
-	624	2.79518		658	2.81756	690	2.83884
	625	2.79588					
-	626	2.79357		659	2.81888	692	2.84010
1	627	2.79726		660	2.81954. 2.82020	693	2.84073
1	628	2.79795		662	2.820851	694	2.84198
1	629	2.79865		663	2.82151	696	2.84260
I	630	2.79934				697	2.84325
1	631	2.80002		664	2.82216	698	2.84385
-	632	2.80071	-	666	2.82347	699	2.84447
-	633.	2.80140		667	2.82412	700	2.84500
1	624	2.002001		00/	2002432	1-01	, ,

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Num	Logarita	1 Nur	1. Logarit		Num	Logariti
1001	2.84571	73	4 2.8050		767	2.88479
702	2.84633	73			768	2.88531
703	2.84595	73			769	2 88392
704	2.84757	73:			770	2.88049
705	2.84818	73	2.8580;		771	2.88705
706	2.84880	1739	2.86854		772	2.88,61
707	2.84941	749			773	2.8881
708	2.8500:	74	4		774	2.38874
709	2.85064	74			775	2.8893c
710	2.85125	74			776	2.8898t
711	285180	744			777	2.80041
712	2.85248	74			778	2.89097
713	2.85308	74			. 779	2.89153
714	2.85356	74			780	2.89209
715	2.85430	748			781	2.89265
710	2.85491	749			782	2 8932
717	2.85551	750			783	2.89376
718	2.85012	75			784	2.89431
719	2 85672	752			785	2.89486
720	2.85733	75			786	2.89512
721	2.85793	75-			787	2.89597
722	2 8 5 8 5 3	75			788	2.89652
723	2.85913	750			789	2.89707
724	2.85973	757			790	2.857' 2
725	2.86032	7:8			791	2.89817
726	2.8609:	759			792	2.89872
727	2.86153	760			793	2.89927
728	2.86213	76			794	2.89982
729	2.86272	76:	1 /1		795	2.90036
730	2.86332	76:	-	1 1	796	2.90091
731	2.86391	76			797	2.90145
732	2.86451	76			798	2.90200
733	2.86510	76			799	2.90254
734	2.86569	76	7 2.88479		800	2.90306

	700					
,	Logarith .	Num	Logarith	1	Num	Logariti
801	2.90303	834	2.92110	1	807	2.9380
802	2.90417	835	2.92168		863	2 93851
803	2.90471	836	2.92220		869	2 93901
804	2.90525	837	2.92272		870	2.93951
805	2.90579	838	2.92324		871	2.94001
806	2.90033	1 839	2.92376		872	2.94051
807	2.90687	840	2.92427		873	2.94101
808	2.90741	841	2.92479	П	874	2.94151
809	2.90794	842	2.92531		875	2.94200
810	2.90848	843	2.92582		876	2.94250
811	2.90902	844	2.92634		877	2.94299
812	2.90955	845	2.92685		878	2.94349
813	2.91009	846	2.92737		879	2.94398
814	2.91062	847	2.92788		880	2.94448
815	2.91115	848	2.92839		881	2.94497
816	2.91169	849	2.92890		882	2.94546
817	2.91222	850	2.92941		8831	2.94596
818	2.91275	851	2.92992		884	2.94645
819	2.91328	852	2.93043		885	2.94694
820	2.91381	853	2.93091		886	2.94743
821	2.91434	854	2.93145		887	2.94792
822	2.91487	855	2.93196		888	2.94841
823	2.91539	856	2.93247	н	889	2.94890
824	2.91592	857	2.93298		890	2.94939
825	2.91645	858	2.93348		891	2.94987
826	2.91098	859	2.93399		892	2.95036
827	2.91750	860	2.93449		893	2.95085
828	2.91803	861	2.93500		894	2.95183
829	2.91855	862	2.93550		895	2.95182
830	2.91907	863	2.93631		896	2.95230
831	2.91960	864	2.93651		897	2.95279
	2.92012	865	2.93701		898	2.95327
	2.92064	866	2.93751		899	2.95375
	2.92116	1 1	2.93801		900	3.95424
			73-1	- 3	900	3.97424

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Num Logarith	Num Logarith	Num Legariti
1 901 2.95472	934 2.97034	957 2.98542
902 2.95520	935 2.97081	968 2.98587
903 2.95568	936 2.97127	969 2.98632
904 2.95616	937 2 97173	970 2.98677
905 2.95664	938 2.07220	971 2.98721
906 2.95712	939 2.97266	972 2.98706
907 2.95760	940 2.97312	973 2.98811
908 2.95808	941 2.97358	974 2.98855
909 2.95856	942 2.97405	975 2.98900
910 2.95904	943 2.97451	976 2.98944
911 2.95951	941 2.97497	977 2.98980
912 2.95999	945 2.97543	978 2.99533
913 2.96047	94(2.97539	979 2.99078
914 2.96094	947 2.97635	980 2.99122
915 2.90142	948 2 97686	081 2.99166
915 2.96189	949 2.97720	982 2.99211
917 2.96236	950 2.9772	98312.99255
918 2.96284	951 2.97818	984 2.99299
919 2.96331	952 2.97863	985 2.99343
920 2.06278	953 2.97909	986 2.99387
921 2.90425	954 2.97954	98; 2.99431
922 2.96473	955 2.98000	988 2.9947;
923 2.95520	950 2.98045	989-2.99519
924 2.96567	957 2.98091	996 2.99563
925 2.95614	958 2.98136	991 2.0960-
926 2.96661	959 2.98181	992 2.99051
927 2.96707	9(0 2.98227	993 2.99694
928 2.96754	961 2.98272	994 2.99738
929 2.96801	962 2.98317	994 2.99732
930 2.96848	963 2.98362	996 2.99825
931 2.96894	904 2.9840	
932 2.9(9.11	965 2.984;2	997 2.99869 998 2.99913
933 2.96988	966 2.98497	999 2 99556
934 2.97034	967 2.98542	1000 3.00000
	7 7 7 7 7 7 4 2 .	1,200 3,00000

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	Num Logarith	Nu	m	Lozarith		Num	Ligari bi
	1001 3.00043	103		3.01452		1007	3.02010
	1002 3 00086	103		3.01494		1058	3.02857
	1003 3.00130			3 015;5		1069	3.02897
	1004 3 00173	103	7	3.01577		1070	3 02938
		101	- 1	3.01619		1071	3.02978
	1006 3 00259			3.01051		1072	3.03019
	1007 3.00302	104		3.01703		1073	3.03059
	1009 3.00389	101	_	3.01745		1074	3.03100
	1010 3.00432	10.	_	3.01783		1075	3.03140
ı	1011 3.00475	104		3.01870		_	3.03181
ı	1012 3.00518	104	-4	3.01911		1077	3.03221
ı	1013 3.00560	104		3.01953		1078	3.03261
ı	1014 3.00603	104		3.01994		1080	3.03302
	1015 3.00646	104	.8	3.02036		1031	3.03182
ı	1016 3.00689	104		3.02077		1082	3.03422
ı	1017 3.00732	105		3.02118		1083	3 03462
ı	1018 3.00774	105		3.02160		1084	3.03502
	1019 3.00817	105		3.02201		1085	3.03542
ı	1020 3.00860	105		3.02242		1086	3.03582
ı	1021 3.00902	105	4	3.02284		1087	3.03022
ı	1022 3.00945	105		3.02325		1088	3.03662
ı	1023 3.00987	105	-	3.02366		1089	3.03702
ı	1025, 3.01072	105		3.02407		1090	3.03742
ı	1026 3.01114	1		3.02448		1091	3.03782
ı	1027 3.01157	105		3.02489	_	1092	3 0 3 8 2 2
ı	1028 3.01199	106	_	3.02530		1093	3.0386z
ı	1029, 3.01241	106		3.02512		1094	3.03901
	1030 3.01283	106		3.02653		1096	3.03941
	1031 3.01325	106		3.02694		1097	-
	1032 3.01 367	106	5	3.02734		1097	3.04020
I	1033 3.01410	106		3.02775		1099	3.04000
1	1034 3.01452	106	71	3.02816		1100	3.04139
					-		1.39

1100		
Num Lugarith	Num Logareth	Num Log: rith
1101 3 04178	1134 3.95461	1167 3.06707
1102 3.04210	1135 3.05499	1168 3.06744
1103 3.04257	1136 3.05537	1169 3.06781
1104 3.04296	1137 3.05576	1170 3.06818
1105 3.04331	1138 3.05614	1171 3.05855
1105 3.04375	1139 3.05652	1172 3.00692
1107 3.0441-	1140 3.05690	1173 3.06929
1108 3.04453	1141 3.05728	1174 3.06966
1109 3 04493	1142 3.05706	1175 3.07003
1110 3.04532	1143 3.05804	1176 3.07040
1111 3.04571	1144 3.058-2	1177 3.07077
1112 3.04610	1145 3.05880	1178 3.07114
1113 3.04 49	1146 3.05918	1179 3.07151
1114 3.04688	1147 3.05956	1180 3.07188
1115 3.04727	1148 3.05994	1181 3.07224
1116 3.04706	1149 3.00032	1182 3.07201
1117 3.04805	1150 3.06069	1183 3.07298
1118 3.04844	1151 3.06107	1184 3.07335
1119 3.04883	1152 3.05145	1185 3.07371
1120 3.04921	1153 3.06182	1185 3.07408
1121 3.04960	1154 3.06220	1187 3.07445
1122 3.04999		1188 3.07481
1123 3.05037		1189 3.07518
1124 3.05076		1190 3.07554
1125 3.05115	1158 3.06370	1191 3.07591
1125 3.05153	1159 3.06468	1192 3.07627
1127 3.05192	1160 3.06.145	1193 3.07664
1128 3.05230	1161 3.06483	1194 3.07700
1129 3.05269		1195 3.07736
1130 3.05307	1163 3.06557	1196 3.07773
1131 3.05346	1164 3.06595	1197 3.07809
1132 3.05384		1198 3.07845
1133 3.0542	1166 3.06669	11199 3.07881
11124-2.05461	1167 3.06707	11200 3.07918

	-	200						
	Num	Logarith	1	Num	1 ogurito		Niene	Logariti
	1021	3.07954	-	11231	13.09131		1257	3.10:77
	1202	3.07990		1:235	3.09166		1258	3.10311
	1203	3.08025	1	1236	3.09201		1260	3.103 ;6
	1204	3.08062	}	123-	3.09236		1270	
	1200	3 08098		1248	3 07272		1271	3.10414
	1206	3.08134		1239	3.00,07		1272	3.10448
	1207	3.03170		1240	3.09312		1273	3.10:82
	1208	3.08206	i	1241	3.09377		1274	3.10516
	1200	3.08242		1242	3.09412		1275	3.19551
	1210	3.08278		1243	3 00447	5	1276	3.10,85
	1211	3 08314		1244	3.09482		1277	3.10519
	1212	3.08350		1245	3.09516		1278	3.106:3
	1213	3.08386		1246	3.09551		1279	3.10687
	1214	3.08421		1247	3.09586		1280	3.10721
	1215	3.08457		1248	3.07621		1281	3.10754
	1216	3.08493		1249	3.09656		1282	3.10788
	1217	3.08529		1250	3.09691		1283	3.10322
	1218	3.08564		1251	3.09725		1284	3.10856
	1219	3.08600		1252	3 09760		1285	3.10.90
-	1220	3.08635		1253	3.09795		1286	3.10924
	1221	3.08671		1254	3.098291		1287	3.10957
	1222	3.08707		1255	3.09364		1288	3.10991
1	1223	3.08742		1256	3.09898		1289	3.11025
	1224			1257	3.09933		1290	3.11058
	1225	3.08813	-	1258	3.09068		1291	3.11092
	1226	3.08849		1259	3.10002		1292	3.11126
		3.08884		1260	3.10037		1293	3.11159
	1228	3.08919		1261	3 10071	1	1294	3.11193
	1229	3.08955	-	1262	3.10105	1	1295	3.11226
1	1230	3.08940	-	1263	3.10140		1296	3.11260
-	1231	3.09025	-	1204	3.10174		1297	3.11294
-	1232	3.09051		1265	3.10209	,	1298	3.11327
1	1233	3.09091	-	1266	3.10243	1	1299	3.11360
-	1234	3.09131		12671	3.10277	1	1300	3.11394
4			-					

1300		
Num Lagirisi	Num Lagarit	Nun. Logarith
1301 3.1142	1334 3.12515	1367 3.13576
1302 3.1146.	1335 3.12548	1368 3.13608
1303 3.1149	1336 3.12580	1369 3.13640
1304 3.11527	1337 3 12613	1370 3.13672
1305 3.11501	1338 3.12 45	1371 3.13703
1306 3.11:91	1339 3.12678	1372 3.13735
1207 3.116.27	1340 3.12710	1373 3.13767
1:08 3.11660	1341 3-12742	1374 3 13798
1309 3.11693	1342 3.12775	1375 3.13830
1310 3.11727	1343 3.12807	1376 3.13861
1311 3.1170	134413.12859	1377 3.13893
1312 3.11793	13+5 3.12872	1378 3.13924
1313 3.11826	1346 3.12901	1379 3.13956
1314 3.11850	1348 3.12935	1380 3.13987
1315 3.11892		
1310 3.11925	1349-3.13001	1382 3.14050
1317 3.11958	1350 3.13033	1383 3.14082
1318 3.11991	1352.3.13097	1384 3.14113
1	1353 3.13129	1386 3.14176
The Person Name of Street, or other Designation of the Person of the Per		
1321 3.12090	1354 3.13101	1387 3.14207 1388 3.14238
1322 3.12123	1355 3.13193	1388 3.14238 1389 3.14270
1324 3.12188	1357 3.13257	1390 3.14301
1325 3.12221	1358 3.13289	1391 3 14332
1326 3.12254	1359 3.13321	1392 3.14363
1327 3.12287	13'0 3.13353	1393 3.14395
1328 3.12319	1361 3.13385	1394 3.14426
1329 3.12352	1362.3.13417	1395 3.14457
1330 3.12385	1363 3.13449	139 3.14488
133: 3.12417	1364 3.13481	1397 3.14519
1337 3.12450	1365 3.13513	1398 3 14550
133 . 3.12483	1366 3.13545	1399 3.14581
133 3.12515	1367 3.1357	140: 3.14612

	1	400						
	Num	Logarith	ì	Num	Logarith		Num	Logarith
	1401	3.14043		1434	3.15054		1467	3.16643
	1403	3.14074		1435	3.1568;		1468	3.16672
	1403	3.1470		1436	3.15715		1469	3.16702
	1401	3.14736		1437	3.15745		1470	3.16731
	140;	3.14767		1438	3.15775		1471	3.16761
	1400	3,14798		1439	3.15806		1472	3.16790
	1407	3.14829		1440	3.15836		1473	3.16820
	1403	3.14860		1441	3.15866		1474	3.16849
	1409	3.14891		1442	3.15896		1475	3.16879
	1410	3.14921		1443	3.15926		14-6	3.16908
	1411	3.14952		1444	3.15950		1477	3.16938
	1412	3.14983		1445	3.15986		1478	3.16967
	1413	3.15014		1446	3-16016		14-9	3.16996
	1414	3.15044		1447	3.16046		1480	3.17026
	1415	3.15075		1448	3.16076		1481	3.17055
	1410	3.15106		1449	3.10100		1482	3.17084
	1417	3.15136		1450	3.16136		1483	3.17114
	1418	3.15167		1451	3.16166		1481	3.17143
	1419	3.15198		1452	3.16196		1485	3.17172
	1420	3.15228		1453	3.16220		1486	3.17201
	1421	3.15259		1454	3.16256		1487	3.17231
	14.22	3.15289		1455	3 16286		1488	3.17260
	1423	3.15320	- 1	1456	3.16316		1489	3.17289
ı	1424	3.15351		1457	3.16345		1490	3.17318
	1425	3.15381	-	1458	3.15375		1491	3.17347
ı	1426	3.15411	-	1459	3.16405		1492	3.17376
ı	1427	3.15442	-	1460	3.16435	- 1	1493	3.17405
ı	1428	3.15472	į	1461	3.15465	- 1	1494	3.17435
	1429	3.15503		1462	3.16494	- 1	1495	3.17464
	1430	3.15533	- 1	1463	3.16524		1496	3.17493
	1431	3.15503		1404	3.16554		1497	3.17522
-	1432	3.15594		1465	3.16583		1498	3.17551
	1433	3.15624	- 1	1466	3.16613	_	1499	3.17580
	1434	3.15654!		1467	3.16643	1	1,00	3,176091
								The second second

1500		 	
1 . Vani Ligarith	Num: Logarith	Num	Lugarith
1501 3.17638	1,34 3.18582	1567	3.19500
1502 3.17665	1535 3.18610	1568	3.19534
1503 3.17695	1536 3.18639	1569	3.19562
1504 3 17724	1537 3.18607	1570	3.19589
1505 3.17753	1538 3.18605	1571	3.19617
1500 3.17782	1539 3.18/23	1572	3.19645
1507 3.17811	154C 3.18752	1573	3.19672
1508 3.178-0	1541 3.18780	15741	3.19700
1509 3.17868	1542 3.18808	1575	3.19728
1510 3.1-897	1543 3.18836	1576	3.19755
1511 3.17920	1544 3.18864	1577	3.19783
1512 3.17955	1545 3.18892	1578	3.19810
1513 3.17983	1546 3.18920	1579	3.19838
1514 3.18012	1547 3.18949	1580	3.19855
1515 3.18041	1548 3.18977	1581	3.19893
1516 3.18069	1549 3.19005	1582	3.19920
1517 3.18098	1550 3.19033	1583	3.19948
1518 3.1812	1551 3.19061	1584	3.19975
1519 3.18155	1552 3.19080	1585	3 20002
1.520 3.18184	1553 3.19117	1586	3.20030
1521 3-18212	1554 3.19145	1587	3.20057
1522 3.182.1	1555 3.19173	1588	3.20085
1523 3.18269	1556 3.19200	1589	3.20112
1524 3.18298	1557 3.19228	159	3.20139
1525 3.1832	15,8 3 19256	1591	3.30167
1520 3.10355	1559 3.16284	1592	3.20194
1527 3.18333	1560 3.19312	1593	3 20221
1528 3.13412	1561 3.19340	1594	3.20248
1529 3.18440	1562 3.19368	1595	3.20276
	1553 3.10395	1596	3.20303
1571 3.18497	1504 3.19423	1597	3.20330
1532 3.18525	1565 3.19451	1598	3.20357
1533 3.18554	1566 3.19479	1599	3.20384
1534. 3.18582	1567 1.19500	1600	3.20412

Nun	Logarith	Num	Logarith		1 37	. 7
1001	3.20436	1	-	1	Charles and the last of the la	Logarith
1502	3.2040(1634	3.21325		1067	3.22193
1603	3.20493	1636	3.21351		1668	3.22219
11604	3.20520	1637	3.21404		1669	3.22245
1605	3.20547	1638	3.21431		1671	3.22271
160t.	3.20574	1039	5.21457			
160-	3.20501	1640	3.21484		1672	3.22323
1608	3.20628	1641	3.21510		1674	3.22349
1609	3.20655	1642	3.21537		1675	3.22401
1610	3.20682	1643	3.21563		1676	3.22427
1611	3.20,09	1544	3.21590		1077	3.22453
1612	3.20736	1645	3.21616		1678	3.22479
1613	3.20703	1640	3.21642		1679	3.22505
1614	3.20790	1547	3.21669		1580	3.22530
1615	3.20817	1648	3.21695		1681	3.22556
1616	3.20844	1049	3.21722		1682	3.22582
1617	3.20871	1650	3 21748		1583	3.22008
1618	3.20897	1651	3.21774		1684	3.22634
1619	3.20924	1652	3.21801	. +	1685	3-22659
1620	3.20951	16:3	3.21827	1	1586	3.22685
1621	3.20978	1554	3.21853	1	687	3.22711
1622	3.21005		3.21879			3.22737
	3.21031	1656	3.21906	1	689	3.22752
1624	3.21058		3.21932			3.22788
	3.21085		3.21958	I	601	3.22814
	3.21112	16;9	3.21984		692	3.22040
	3.21138	1	3.22010	I		3.22805
1	3.21165	2 - 2 "	3.22036	I		3.22891
	3.21192		3.22003			3.22916
I			3.22089	-		3.22912
	3.21245	664 3	3.22115			3.22968
	3.21272		3.22141			1.22993
	3.21325		3.2216			1.23019
1-4-1	1.21329	0.57). · · Z I Q ·	1	0 3	.23011

	1700							
Num	Logarith.		Num	Logarith		Num	Logarith	
1701	3.23070		1734	3.23904		1707	3.24723	
1702	3.23095		1735	3.23929		17(8	3 24748	
1703	3.23121		1736	3.23954		1769	3.24772	
1704	3.23146		1737	3.23979		1770	3.24797	
1705	3.23172		1738	3.24004		1771	3.24821	
1706	3 23197		1739	3.24029		1772	3 24846	
1707	3.23223		1740	3.24054		1773	3.24370	
1708	3.23248		1741	3.24079		1774	3.24895	
1709	3.23274		1742	3.24104		1775	3.24919	
1710	3.23299		1743	3 24129		1776	3.24944	
1711	3.23325		1744	3.24154		17.7	3.24968	
1712	3.23350		1745	3 24179		1778	3.24993	
1713	3.23375		1746	3 24204		1779	3.25017	
1714	3.23401		1747	3.24229		1780	3.25042	
1715	3.23426		1748	3.24254		1781	3 25066	
1716	3.23451		17+9	3.24278		1782	3.25090	
1717	3.23477		1750	3.24303		1783	3.25115	
1718	3.23502		1751	3.24328		1784	3.25139	
1719	3.23527		1752	3.24353		1785	3.25163	
1720	3.23552		1753	3.2437°		1786	3.25188	
1721	3.23578		1754	3.2440.		1787	3.25212	
1722	3.23603		1755	3.24427		1788	3.25235	
1723	3.23628		1756	3.24452		1789	3.25261	
1724	3.23653		1757	3.24477		1790	3.25281	
1725	3.23678		1758	3.24501		1791	3.25309	
1726	3.23704	t	1759	3.24526		1792	3.25333	
1727	3.23729		1760	3.24551		1793	3.25358	
1728	3.23754		1761	3.24575		1794	3.25382	
1729	3.23779 3.23801		1763	3.24600		1795	3.25406	
1730						1796	3.25430	
1731	3.23829		1764	3.2 1649		1797	3.25454	
1732	3.23854		1765	3.24674		1798	3.25478	
1733	3.23879		1766	3.24699	1	1799	3.25503	
1734	13.23004	ĺ	11,07	3.24723		11900	3 25527	

180	0						
Num L	ogarith	Num	Logorith		Num	Lorarith	
1801 3	.25551	1834	3 25339		1807	3.27114	
	.25575	1835	3.26363		1863	3.27137	
1803 3	.25599	1836	3.26387		1869	3.27160	
	.25623	1837	3.26410		1870	3.27184	
1805 3	.25647	1838	3.26434		1871	3 27 207	
	3.25671	1839	3.20458		1572	3.27230	
1807 3	1.25695	1840	3.26481		1873	3.27253	ı
	3.25719	1841	3.20505		1874	3.2,2-6	
	3.25743	1842	3.26528		1875	3.27300	l
1810	3.25767	1843	3.26552	ŧ	1876	3.2-323	l
1811	3 25791	1844	3.20576		1877	3 27346	
	3.25815	1845	3.26599		1878	3.27369	ı
	3.25839	1846			1879	3.27392	ŀ
1814	3.25863	1347			1880	3.27415	L
1815	3.25887	1348	-	ŧ	1881	3 2-0.38	ı
	3.25911	1849			1882	3.27401	l
	3.25935	1850		1	1383	3.27485	ı
	3.25959		3.26740		185.4	3.27508	t
	3.25983	1852			1885	3.27531	ı
1820	3.26007	1853			1886	3.27554	
1821	3.26030				1887	3.27577	
1822	3.26054				1888	1 -	
1823	3.26078		1		1889		
1824	3.26102				1890		
1825	3.26126				1391	3.27660	
1826	3.26150				1892		
1827	3.26173				1893		
1828	3.25197				1894	3.27738	No. of Lot
1829	3 26221		10		1895		
1830	3.26249			- 1	1896		=11
1831	3.21 268				1897		
1832	3.26292	2 1186) = '		1898	3.27820)
11833	3.26316				1889	3.2785	-
1834	3.26330	9 1186	7 3.2711	4	11900	3.2787	7.3

	1900			· · · · · · · · · · · · · · · · · · ·			
Nun	Logarith		Num	Logarith	Num	Logarith	1
11901	3.27898		1934	3.28645	1967	3.2938c	
1902		-	1935	3.28568	1968	3.29402	l
1903			11930	3.28590	11969	3.29424	l
11904			1937	3.28712	1970	3.29446	ı
100:	3.27989		1938	3 28735	19-1	3 29468	L
1900			1939	3 28757	1972	3.29490	
11907			1940	3.28780	1973	3.29512	l
1908			1941	3.28802	1974	3.29534	
1909			1542	3.28824	1975	3 29556	ı
1010	1 3		1943	3.26 847	1976	3.29578	ı
Byll	3.18126		1944	3.22869	1977	3.29500	ľ
1912			1945	3.20891	1978	3,29622	
. 1913	1 / 1		1946	3.26814	1979	3.29644	
1914			1947	3.28936	1980	3.29666	
:915	3.282.0		1048	3.28958	1981	3.29688	
916			1919	3 28481	1982	3.29710	
1917	3.28262		1950	3.29003	1983	3.29732	
1.918	3.28284		1951	3.29025	1984	3.29754	
1919	3.28307	П	1952	3.29047	1985	3.29776	
1920	3.28330	П	1953	3.29070	1986	3.29797	
1921	3.28352		1954	3.29092	1987	3.29819	
1922	3.28375		1955	3.29114	1988	3.29841	
1923	3.28397		1656	3.29136	1989	3.29863	
1924	3.28420		1957	3.29159	1990	3.29885	
1925				The state of the s	-	3.29907	
1926	3.28465		1959	3.29203	1992	3.29928	
1927	3 28 488		1960	3.29225	1993	3.2995C	
11928	3 28510		1961	3 29247	1994	3.29972	
1925	3.28533		1963	3.292'9	1995	3.25994	
	-			3-29202		3.30016	
1931	3.28578		1964	3.29314	1997	3.30037	
1932	3.28000		1965	3 29336	1998	3.30059	
1933	2.28645		1967	3.29358	2000	3.30101	
	1 . 200	-	190/	1.293	100001	3 30102	-

ERRATA.

b fignifies reckon from the Bottom.

40115	3.295	10月1日 日本自2日公司公司 日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本
Page	Line	Read
3	76	black line (instead of flower-de-luce)
4	16	to the true
15		Calais
		Frith
		Texel Road
		wight was a second of the seco
28		Then the
		Sum 28 12
33	70	25 2 13
44	70	14 56 (under October)
53	13	reckonings outward
68	2	thro' G, H, AL; and the departure is
00	22	The Diff. of Longitude (begins the Break)
77	12	PROP. VIII.
91		PLAIN SAILING.
3		Courfe 3½
93	26	VI. By the Log. Tangents.
95		Fig. 16 (in the Margin)
119		for East India
124	7	NW & NIW.
1 32	56	Current
137		Chiloa I.
143		Malique I.
144		Mayetta I. Lat. 13 10 S.
ITI	0	Serration

TRAVERSE TABLE.

(12 Deg. Dift. 38.) Dep. 7.9 (31 Deg. Dift. 60.) Lat. 51.4 (36 Deg. Dift. 40.) Lat. 32.4 (36 Deg. Dift. 58.) Dep. 34.1 (45 Deg. Dift. 36.) Dep. 25.4

TABLE

ERRAT

TABLE of Meridional Parts.

D. M. Read M. P.

0:3292

8,3394

53 14 3787

24187

4.4558

72 46 6487

76 67235

86 54 12408

TABLE of Sines, &c.

D. M. Read

10 Cot. 12.53627

37 Tan. 8.65992

21 Sine 9.10697 7

22 Sine 9.10795 54 Sine 9.13812 1 Tan. 9.20052

10 1 Tan. 9.24705

12 17 Sine 9.32786

14 3 Tan. 9.39838

18 4 Cot. 10.48650

18 21 Sine 9.49805

18 25 Cot. 10.47758

19 10 Tan. 9.54471

22 34 Cot. 10.38134

23 34 Cot. 10.36031

24 52 Cot. 10.33317

25 35 Cot. 10.31988

26 30 Cot. 10.30226

28 30 Cot. 10.26 523

29 13 Cot. 10.25238

29 51 Tan. 9.7 &c.

35 56 Tan. 9.85

&C.

FINIS.

22.045.002 *

